A Genetic Algorithm based Methodology for Optimizing Multi–Service Convergence in a Metro WDM Network

Hyo–Sik Yang, Martin Maier, Martin Reisslein, and W. Matthew Carlyle

Abstract— We consider the multi-objective optimization of a multi-service AWG-based single-hop metro WDM network with the two conflicting objectives of maximizing throughput while minimizing delay. We develop and evaluate a genetic algorithm based methodology for finding the optimal throughput-delay trade-off curve, the socalled Pareto-optimal frontier. Our methodology provides the network architecture (hardware) and the Medium Access Control (MAC) protocol parameters that achieve the Pareto-optima in a computationally efficient manner. The numerical results obtained with our methodology provide the Pareto-optimal network planning and operation solutions for a wide range of traffic scenarios. The presented methodology is applicable to other networks with a similar throughput-delay trade-off.

Keywords— Arrayed–Waveguide Grating, Genetic Algorithm, Medium Access Control Protocol, Metropolitan Area Network, Multi–Objective Optimization, Pareto–Optimal, Wavelength Division Multiplexing

I. INTRODUCTION

O PTICAL single-hop wavelength division multiplexing (WDM) networks have the potential to provide high throughput and low delay connectivity in metropolitan and local area settings, as demonstrated by recent studies [1] – [9]. The throughput-delay performance of these single-hop WDM networks is typically very sensitive to the setting of the *architecture parameters* (e.g., degree of underlying arrayed-waveguide grating (AWG), degree of employed combiners and splitters) and the medium access control (MAC) *protocol parameters* (e.g., length of frames in timing structure, number of control slots, node back-off probability). For good network performance, these pa-

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Fig. 1. Different types of traffic dominate during different times of the day

rameters must be set properly, which is a challenge due to the large search space of possible parameter combinations and the typically computationally demanding evaluation of a particular parameter combination. Importantly, in single-hop WDM networks, the objectives to maximize the throughput while minimizing the delay are typically conflicting. With certain combinations of parameter settings, the networks achieve a small delay and moderate throughput, which is perfectly suited for *delay-sensitive* traffic with moderate throughput requirements, such as voice traffic. On the other hand, certain combinations of parameter settings achieve a large throughput but introduce some moderate delays, which is perfectly suited for throughput-sensitive traffic that can tolerate some delays, such as Internet (FTP, HTTP, e-mail) and Frame Relay traffic. Typically, these different types of traffic dominate during different times of the day, as illustrated in Figs. 1 a) - c [10]. During office hours, voice traffic dominates the network load. Whereas Internet and Frame Relay traffic play a major role in the evening and at night, respectively. By carrying these heterogeneous traffic types in a single converged network the utilization of the network resources can be significantly increased, as illustrated in Fig. 1 d). The resulting multi-service network enables revenuegenerating services in an efficient and cost-effective way [11] - [13]. This is very important especially in costsensitive metropolitan and local area networks.

The challenge of multi-service convergence lies in (i)providing the different types of small delay – moderate throughput and large throughput – moderate delay service at different times of the day in a given fixed installed network, and (ii) providing these different service types efficiently, e.g., achieving the largest possible throughput in the small delay – moderate throughput regime. Optimizing the parameter setting in single-hop WDM networks for multi-service convergence thus gives rise to a socalled multi-objective optimization problem. This multiobjective optimization problem does not have a single solution; instead, the solution is a Pareto-optimal trade-off curve between throughput and delay. Roughly speaking, this trade-off curve gives the smallest achievable delay as a function of the desired throughput, or conversely, the largest achievable throughput as a function of the tolerable delay. Finding the optimal trade-off curve as well as the combinations of parameter settings that attain this optimal trade-off curve is a challenging problem. This is due to the large search space of parameter combinations and the typically demanding evaluation of an individual parameter combination. The optimal trade-off curve, however, is crucial for (1) the planning and provisioning of new networks, i.e., to determine the best architecture (hardware) parameters, and (2) the efficient operation of installed network hardware. The Pareto-optimal throughput-delay trade-off curve can thus be used in a two-step optimization process as follows. First, we optimize a *new* network by finding the optimal architecture (hardware) parameter values. Second, after fixing the architecture, we optimize the protocol (software) parameters for an *existing* architecture. Specifically, we operate the network at different points of its Paretooptimal throughput-delay trade-off curve according to the traffic type that dominates at a given time of the day. The network protocol parameters are tuned to provide varying degrees of (i) small delay (and moderate throughput) service, or (ii) large throughput (and moderate delay) service as the traffic changes with the time of the day. This tuning requires detailed knowledge of the optimal trade-off curve, which can be pre-computed with our methodology and stored in tables for fast look-up.

In this paper, we develop a genetic algorithm based methodology for solving the multi-objective optimization problem of maximizing throughput and minimizing delay in single-hop WDM networks. We consider the Arrayed-Waveguide Grating (AWG)-based network [5] as an example throughout this paper. Our methodology finds the optimal trade-off curve and the parameter combinations attaining the curve in a computationally efficient manner. Our work enables network planners to select the (hardware) network architecture parameters that give the best performance. In addition, our methodology enables the operators of (fixed) installed network hardware to optimally tune the throughput-delay performance along the optimal trade-off curve by changing the (software) network MAC protocol parameters.

While we focus on the AWG-based network [5] in this work, our methodology applies analogously to networks with a similar throughput–delay trade–off. Our genetic algorithm based approach takes an analytic characterization of the mean throughput and the mean delay of the network as input. This analytic characterization may involve highly non–linear equations (or possibly systems of equations); we only require that the equations can be solved numerically. Our methodology may also be applied to networks that are analytically intractable and require simulations to obtain the (mean) throughput and the (mean) delay. The computational effort required to obtain the optimal throughput-delay trade-off curve for a given traffic load with our approach depends on the effort required to evaluate the throughput and the delay for a particular combination of network parameters and the size of the exhaustive search space. The number of parameter combinations that our approach needs to evaluate to obtain the optimal trade-off curve is usually on the order of thousand times smaller than the exhaustive search space. In typical scenarios, our approach requires less than one day of CPU time on a 933 Mhz PC to find the optimal trade-off curve, whereas the exhaustive search would require several years of CPU time.

This paper is organized as follows. In the following section we review the related work on optimizing optical WDM networks, including works that employ genetic algorithm based approaches. In Section II, we formulate the multi-objective optimization problem of maximizing throughput while minimizing delay. We briefly review the AWG-based single-hop WDM network [5], which is used as an example throughout the paper. We give the two objective functions (throughput and delay), we identify the decision variables in the optimization and discuss the constraints on the decision variables. In Section III, we develop our genetic algorithm based methodology for finding the Pareto-optimal throughput-delay trade-off curve. First, we briefly review the notion of multi-objective optimization and explain why we base our solution methodology on genetic algorithms. We then discuss and evaluate in detail the individual components of our methodology. In Section IV we apply our methodology to the AWG-based single-hop WDM network and study its optimal throughput-delay trade-offs in detail. We summarize our conclusions in Section V.

A. Related Work

We now give a brief overview of the literature on optimization in optical WDM networks, which may be broadly categorized into studies addressing (i) wide–area wavelength–routed mesh WDM networks (typically envisioned as Internet backbone networks), (ii) WDM ring networks, and (iii) WDM networks with a physical star topology (typically employed in the metro/local area with a central passive star coupler (PSC) or AWG). The design and operation of wavelength-routed mesh (wide area) WDM networks have been optimized extensively, including aspects such as the routing and wavelength assignment, as well as the design of optimal logical topologies, see for instance [14] - [29], and references therein. Also, optimality issues in planning and operation of survivable wavelengthrouted WDM networks have been thoroughly investigated, see for instance [30] - [37], and references therein. The optimal placement of wavelength converters in WDM mesh networks is studied in [38], while [39] studies the optimal amplifier placement. The optimal setting of physical parameters in optical networks, such as the power budget and detection thresholds, have also been investigated, e.g., [40] - [42]. General strategies for the optimal planning of optical networks are explored in [43],[44].

WDM ring networks (including SONET/SDH rings) have received a great deal of attention and a wide range of aspects of ring networks, including the placement of add/drop multiplexers, traffic grooming strategies, the provisioning of wavelengths and hardware components to ensure network survivability, as well as MAC protocols and wavelength assignment have been optimized, see for instance, [45] - [57].

WDM networks with a physical star topology are typically studied in the context of single-hop networks [6] or multi-hop networks [58]. For multi-hop networks, much research has gone into the design of optimal virtual topologies (see for instance [59] - [61] or the survey [58]). For single-hop networks most optimization efforts have focused on the optimal scheduling, see for instance [62] - [68]. Our optimization methodology is orthogonal to these studies in that our methodology optimizes the architecture and MAC protocol parameters of the network without assuming any particular scheduling mechanism. (To fix ideas a simple FCFS scheduling policy is used in [69], where the mean throughput and the mean delay of the network considered in this paper are derived.) A unique aspect of our work is that we jointly optimize the network architecture (hardware) and the MAC protocol parameters (software). Generally, the existing works, in isolation optimize either hardware or software parameters. We also note that most of the existing literature on single-hop WDM networks considers networks based on a central PSC, which is a broadcast device and hence does not allow for spatial wavelength reuse. In contrast, we consider a network based on an AWG, which provides wavelength-sensitive routing and thus allows for spatial wavelength reuse. This allows for increased concurrency and as we demonstrate in this paper, makes the AWG based network a promising candidate for efficiently achieving multi-service convergence in metro area networks. (The wavelength routing property of the AWG has recently also been exploited in other networking contexts, e.g., in optical packet switches [70].)

Another distinguishing feature of our work is that we

explicitly consider a multi-objective optimization problem. whereas most of the existing literature focuses on optimizing a single objective function. Optical network optimization with multiple conflicting objectives is considered only by a few studies. In [71] reconfiguration policies to accommodate changing traffic (routing) patterns or the failure of network components in a PSC-based single-hop WDM network are studied. It is found that maximizing the degree of load balancing and minimizing the number of transceiver retunings are conflicting objectives. The problem is formulated in a Markov decision process framework, which is used to evaluate reconfiguration policies. The reconfiguration policy that achieves the desired balance between the two conflicting objectives is determined by selecting proper cost functions and weights for the objectives. In [51] it is noted that minimizing the number of nodes (optical adddrop multiplexers) and minimizing the number of rings in a stack of WDM rings are conflicting objectives; the trade-off is quantified and a heuristic for finding a spectrum of designs is developed. Similarly, in [48], [49] it is observed that the objectives to minimize the number of optical add-drop multiplexers and to minimize the number of wavelengths in a WDM ring network are conflicting and a number of designs that strike different balances between the objectives are proposed. In [72] a multi-objective optimization problem to find the wavelength assignment in a mesh WDM network that minimizes the path lengths while maximizing the fiber utilizations is formulated and solved using genetic algorithms.

A wide range of optimization methods are employed in the reviewed optical network optimization studies. Some use traditional optimization methods that are guaranteed to find the global optimum, such as integer linear programming, employed for instance in [16], [31], [35] - [37]. However, due to the complexity of the problems and the prohibitive computational effort required for solving them with traditional methods, novel algorithms and heuristics are developed (e.g., [29]) and heuristic algorithms, such as Tabu-search (e.g., in [73], [19], [28]), simulated annealing (e.g., in [23], [74]), and genetic algorithms (in [75], [72], [76] - [39]) are applied. We note that the use of evolutionary (genetic) algorithms in the design of general wide area mesh network topologies that minimize the network cost is studied in [79]. Genetic algorithms are compared with simulated annealing for optimizing the topological design of a network in [80] and it is found that genetic algorithms give better performance than simulated annealing. The existing studies employing genetic algorithms for optical network optimization typically optimize a *single* objective, e.g., minimize the number of amplifiers [39], minimize the network cost [77], [78], or maximize the number of connections while satisfying power constraints [75]. In contrast, in this paper we consider a *multi-objective* optimization problem — minimize delay while maximizing throughput.

II. FORMULATING THE MULTI–OBJECTIVE Optimization Problem

In this section we formulate the multi-objective optimization problem of maximizing throughput while minimizing delay in single-hop WDM networks. We first review the AWG-based single-hop WDM network [5], which we use as an example network throughout this paper.

A. Overview of AWG-based Single-Hop WDM Network

The basic architecture of the single-hop WDM network [5] is based on a $D \times D$ AWG, as shown in Fig. 2. At each AWG input port, a wavelength-insensitive $S \times 1$ combiner collects data from S attached nodes. Similarly, at each AWG output port, signals are distributed to S nodes by a wavelength-insensitive $1 \times S$ splitter. (An Erbium Doped Fiber Amplifier (EDFA) is placed at the output of each combiner and the input of each splitter to compensate for the splitting/combining and fiber losses.) Each node is composed of a transmitting part and a receiving part. The transmitting part of a node is attached to one of the combiner ports. The receiving part of the same node is located at the opposite splitter port. The network connects $N = D \cdot S$ nodes. At each AWG input port we exploit R adjacent Free Spectral Ranges (FSRs) of the AWG, each FSR consists of D contiguous wavelengths. The total number of wavelengths at each AWG input port is $\Lambda = D \cdot R$. The network runs an attempt-and-defer type of MAC protocol, i.e., a data packet is only transmitted after the corresponding control packet has been successfully transmitted. In the MAC protocol, time is divided into cycles. Each cycle consists of D frames. Each frame contains F slots. The slot length is equal to the transmission time of a control packet. Each frame is partitioned into the first M, $1 \leq M < F$, slots and the remaining (F - M) slots. In the first M slots, control signals are transmitted based on a modified slotted ALOHA protocol and all nodes must be tuned (locked) to one of the Light Emitting Diode (LED) slices carrying the control information. (This LED slice broadcast mechanism can also be used to quickly update the protocol parameters in all network nodes. By looking up the appropriate parameter settings in a table precomputed with our methodology and broadcasting them to the nodes with the LED slices in one single hop, the network is able to adapt almost instantly to changing traffic conditions and throughput–delay requirements.) In every frame within the cycle, the nodes attached to a different AWG input port send their control packets. Specifically, all nodes attached to AWG input port o, 1 < o < D, (via a common combiner) send their control packets in frame o of the cycle. During the first M slots of frame o, control and data packets can be transmitted simultaneously by the nodes attached to AWG input port o. Transmissions from the other AWG input port cannot be received during this time interval. In the last (F - M) slots of each frame, no control packets are sent. The receivers are unlocked, allowing transmission between any pair of nodes. This allows for spatial wavelength reuse. In the considered traffic scenario, a node that is not backlogged generates a new packet with probability σ at the beginning of its transmission cycle. The generated packet is long (has size F slots) with probability q, and is short (has size K = F - M slots) with probability 1 - q. The parameters of the considered network architecture and MAC protocol, as well as the traffic parameters are summarized in Table I.



Fig. 2. Architecture of AWG based WDM network

B. Objective Functions: Throughput and Delay

The two key performance metrics of single-hop WDM networks, such as the AWG-based network reviewed in the preceding section, are the mean throughput and the mean delay. The typical goal of the optimization of single-hop WDM networks is to maximize the throughput while minimizing the delay. For the reviewed AWG-based network, the mean throughput and the mean delay have been derived in [69] as functions of the parameters summarized in Table I. (The derivation in [69] considered the case M < F, i.e., K > 0. In our optimization, we allow for $M \leq F$, i.e., $K \geq 0$; the objective functions for the special case M = F are derived in the Appendix.) We briefly review here these two objective functions of our optimization.

The average throughput of the network is defined as the average number of transmitting nodes in a slot and is given by:

$$TH = D^2 \cdot \frac{F \cdot E[\mathcal{L}] + K \cdot E[\mathcal{S}]}{F \cdot D}, \qquad (1)$$

where $E[\mathcal{L}]$ is the expected number of successfully scheduled long packets (of size F slots) from a given (fixed) AWG input port to a given (fixed) AWG output port per cycle (of length $F \cdot D$ slots), and E[S] is the expected number of successfully scheduled short packets (of length K = F - Mslots) from a given (fixed) AWG input port to a given (fixed) AWG output port per cycle. (We note that the throughput given by (1) may also be interpreted as the average number of transmitted data packets per frame; for

	Network Architecture (Hardware) Parameters
N	Number of nodes in the network
Λ	Number of usable wavelengths at each AWG port (Tuning range of transceivers)
D	Degree of AWG
R	Number of FSRs $(R = \Lambda/D)$
S	Degree of combiner and splitter $(S = N/D)$
_	Protocol (Software) Parameters
F	Number of slots in a frame
M	Number of reservation slots in a frame
K	Length of short packets in slots $(K = F - M)$
p	Re–transmission probability of control packet in ALOHA contention
	Traffic Parameters
σ	Packet generation probability (for idle node at beginning of cycle)
q	Probability that a given data packet is long (i.e., occupies F slots)
	Performance Metrics (Objective Functions)
TU	Average network throughput in transmitting nodes per glot
тп	Average network throughput in transmitting nodes per slot
	(or equivalently in packets/frame)
Delay	Average packet delay in slots

 TABLE I

 PARAMETERS OF NETWORK ARCHITECTURE AND MAC PROTOCOL

convenience we will use this packets/frame interpretation in our numerical work in Sections III and IV.) $E[\mathcal{L}]$ and $E[\mathcal{S}]$ are evaluated by modeling the control packet contention and the data packet scheduling, and then establishing a set of equilibrium equations for the network. In brief, the arrival rate of control packets to a given control slot is expressed as

$$\beta = \frac{S}{M} [\sigma v + p(1-v)], \qquad (2)$$

where v is the fraction of idle (i.e., not backlogged) nodes in steady state. The number of successful (i.e., not collided) control packets destined to a given AWG output port in a given frame is expressed as

$$P(Z=k) = \binom{M}{k} \left(\frac{\beta e^{-\beta}}{D}\right)^{k} \left(1 - \frac{\beta e^{-\beta}}{D}\right)^{M-k},$$

$$k = 0, 1, \dots, M.$$
(3)

The probability that a given control packet corresponds to a long data packet (either newly generated by an idle node, or retransmitted by a backlogged node) is denoted by \tilde{q} ; note that typically $\tilde{q} > q$ since long data packets are more difficult to schedule and thus typically require more retransmissions than short packets. The analysis of the data packet scheduling results in

$$E[\mathcal{L}] = \tilde{q} \left\{ R - \sum_{k=0}^{\min(R,M)} P(Z=k)(R-k) \right\} := \tilde{q} \cdot \varphi(\beta) \quad (4)$$

and

$$E[\mathcal{S}] = (1 - \tilde{q}) \left[R - \sum_{k=0}^{R} (R - k) \cdot P(Z = k) \right] + \sum_{j=1}^{M-R} \gamma_j \sum_{m=j}^{M-R} \sum_{k=m+R}^{M} \binom{k-R}{m} \cdot (1 - \tilde{q})^m \tilde{q}^{k-R-m} \cdot P(Z = k)$$
$$:= h(\tilde{q}, \beta), \tag{5}$$

where γ_j accounts for the "packing" of the short packets into the schedule and is given by a non–linear function of the network and traffic parameters and \tilde{q} . Finally, in equilibrium, the numbers of serviced long and short packets are equal to the numbers of newly generated long and short packets, which, after some algebraic manipulations, results in the equations

 $\tilde{q} = q \cdot \frac{S\sigma v}{D \cdot \varphi(\beta)} \tag{6}$

and

$$(1-q) \cdot \frac{S\sigma}{D} \cdot v = h(\tilde{q}, \ \beta). \tag{7}$$

Equation (7) is solved numerically and the obtained v is inserted in (2) to obtain β , which in turn is used in (4) to obtain $\varphi(\beta)$. These quantities are in turn used to obtain \tilde{q} from (6), and finally $E[\mathcal{L}]$ from (4) and $E[\mathcal{S}]$ from (5).

The mean packet delay is defined as the average time period in slots from the generation of the control packet corresponding to a data packet until the transmission of the data packet. The average delay in the network in slots is:

$$Delay = \left\{ \frac{S}{D \cdot (E[\mathcal{L}] + E[\mathcal{S}])} - \frac{1 - \sigma}{\sigma} \right\} \cdot D \cdot F.$$
 (8)

C. Decision Variables and Constraints

We now identify the decision variables in our optimization problem and identify the constraints on the decision variables. We select the AWG degree D as the (independent) decision variable for the network (hardware) architecture; we determine the other architecture parameters Rand S (see Table I) as functions of D (and the given N and Λ), as discussed shortly. Generally, the decision variable Dcan take any integer satisfying

$$D \ge 2$$
 and $D \le \Lambda$, (9)

where Λ is the maximum number of wavelength channels accommodated by the fast tunable transceivers employed in the considered network. In other words, Λ is the maximum tuning range of the employed transceivers divided by the channel spacing and is thus very technology dependent. (To use transceivers with a negligible tuning time (and a small tuning range) we set $\Lambda = 8$ in our numerical investigations in Sections III and IV.) We also note that the number of ports of commercially available photonic devices is typically a power of two. We can easily incorporate this constraint by restricting D to the set $\{2, 4, 8, \ldots\}$.

The number of used FSRs R depends on the (independent) decision variable D and the given tuning range Λ of the transceivers. Generally, R must be an integer satisfying $R \cdot D \leq \Lambda$, i.e., $R \leq \Lambda/D$. The larger R, the more parallel channels are available between each input-output port pair of the AWG, and hence the larger the throughput. Therefore, we set R to the largest integer less than or equal to Λ/D , i.e., $R = |\Lambda/D|$. We note that the tuning range Λ and degree D are typically powers of two for commercial components. Hence, Λ/D is a power of two for practical networks, and we may write $R = \Lambda/D$. The combiner/splitter degree S depends on the decision variable Dand the given number of nodes in the network N. In determining the combiner/splitter degree S, it is natural to assume that the nodes are equally distributed among the D AWG input/output ports; i.e., each input/output port serves at least |N/D| nodes. This arrangement minimizes the required combiner/splitter degree S, which in turn minimizes the splitting loss in the combiners/splitters. Hence, we set $S = \lfloor N/D \rfloor$.

We now turn to the protocol (software) parameters; see Table I. We identify three decision variables; these are F, M, and p. Generally, the number of slots per frame Fcan take any positive integer, i.e., $F \ge 1$, while the number of control slots per frame can take any positive integer less than or equal to F, i.e., $1 \le M \le F$. (Note that in case M = F, the length of the short packets degenerates

to zero. In this case only large packets contribute to the throughput; the objective functions for this case are given in the Appendix.) We note that the size of the packets to be transported may impose additional constraints on Fand M. With a given maximum packet size, F must be large enough to accommodate the maximum size packet in a frame. If short packets have a specific size requirement, F-M should be large enough to accommodate that packet size. For our numerical work in Section III and IV we do not impose packet size requirements. Instead, we let the genetic algorithm determine the F and M values that give the optimal throughput-delay performance, subject only to $F \geq 1$ and $1 \leq M \leq F$. The packet re-transmission probability p may take any real number in the interval [0, 1]. To reasonably limit the search space we restrict p to $[0, 0.05, 0.10, 0.15, \ldots, 1.0]$ in our numerical work.

D. Network Cost Considerations

Minimizing the total network cost could be a third objective, in addition to the maximize throughput and minimize delay objectives introduced in Section II-B. We note that the genetic algorithm methodology could accommodate the third objective in a straightforward fashion, it would make the solution space three dimensional. Specifically, we would obtain an optimal throughput-delay trade-off plane for a given (acceptable) cost level. We did not include network cost minimization in our optimization model because we are primarily interested in uncovering the fundamental performance limitations and trade-offs in the metro WDM network. Network cost — while an important consideration — is typically not considered a fundamental performance metric for a network. In addition, network costs tend to be highly variable. The costs of the hardware components in the considered network are expected to drop significantly once they are extensively mass produced.

Even though we did not include cost minimization in our optimization model, we now briefly discuss the impact that the cost minimization objective would have on the problem and its solution. Generally, the total network cost is the sum of capital expenditures (cost of network hardware and installation) and operational expenditures (cost of network management). With the current component pricing structure, the hardware cost of the network increases linearly with the AWG degree D. This is because (i) there is typically a per-port charge for an AWG, and (ii) the number of required EDFAs increases linearly with D. (The cost of the splitters/combiners is typically insignificant. Also, the number of transceivers depends only on the number of network nodes.) The cost of installation is roughly fixed (and independent of the decision variables), as is the network management cost. Thus the total network cost is approximately a linear function of the AWG degree D. Since D is typically a power of two, the genetic algorithm methodology would give optimal throughput-delay planes for each $D = 2, 4, \ldots$ This three dimensional solution gives the

best throughput–delay trade–off for a given acceptable cost level.

III. GENETIC ALGORITHM BASED METHODOLOGY

In this section we discuss the difficulties in optimizing the multiple objectives of maximizing throughput while minimizing delay. We point out why we base our solution methodology on genetic algorithms. We describe our genetic algorithm solution approach to the multi-objective optimization problem formulated in the previous section and evaluate the performance of our approach.

A. Why Evolutionary Algorithm (Genetic Algorithm)?

The familiar notion of an optimal solution becomes somewhat vague when a problem has more than one objective function, as is the case in our metro WDM network optimization. A solution (i.e., set of decision variables D, F, M, and p) that gives very large throughput may also give large delay and thus rate poorly on the minimize delay objective. The best we can do is to find a set of optimal tradeoff solutions, i.e., solutions that give the largest achievable throughput for a given tolerable delay, or equivalently the smallest achievable delay for a required throughput level. After a set of such optimal trade-off solutions is found, a user can then use higher–level considerations, such as the traffic patterns illustrated in Fig. 1, to make a choice. A feasible solution to a multi-objective optimization problem is referred to as efficient point or Pareto-optimal solution [81]. As illustrated in Figs. 3 and 4, we have two objectives — maximizing throughput, and minimizing delay. The region which is shaded in light gray is said to be *dominated* by the point X. All points in the region, e.g., A and Bhave larger delay and smaller throughput than the point X. Clearly, the point X is superior to the points A and B. Thus all points in the light gray rectangle are dominated by point X. All points in the dark gray rectangle, e.g., the point E, are said to *dominate* the point X. Since all points in the dark gray rectangle have larger throughput and smaller delay than X. The point E is superior to the point X. Based on the concept of Pareto dominance, the optimality criterion for multi-objective problems can be introduced. Consider the points C, D, E, F, and G. These points are unique among all the points in the plot in that each of them is not dominated by any other point. The set of these solutions is termed as *Pareto-Optimal* solution set or Efficient Frontier. The efficient frontier corresponding to Fig. 3 is shown in Fig. 4.

The goal of multi-objective optimization is to find such a feasible efficient frontier. Classical methods for generating the Pareto-optimal solution set aggregate the objectives into a single, parameterized objective function. The parameters of this function are not set by the decision maker, but systematically varied by the optimizer [82]. In contrast to classical search and optimization algorithms, evolutionary algorithms use a *population* of solutions in each iter-



Fig. 3. Illustration of Pareto–Optimal solutions for maximize throughput–minimize delay problem



Fig. 4. Illustration of Efficient Frontier for maximize throughputminimize delay problem

ation, instead of a single solution. Since a population of solutions is processed in each iteration, the outcome of an evolutionary algorithm is also a population of solutions for the conflicting objective functions. These multiple optimal solutions can be used to capture multiple efficient points of the problem [81].

We now proceed to develop a methodology for efficiently finding the Pareto–optimal solutions (optimal trade–off curve) of the multi–objective problem of maximizing throughput while minimizing delay in single–hop WDM networks. Our solution methodology is based on genetic algorithms, which are members of the family of evolutionary algorithms.

B. Basic Operation of Genetic Algorithm

The basic structure of a genetic algorithm is illustrated in Fig. 5. In the genetic algorithm, we consider a population of individuals. Each individual is represented by a string of the decision variables, i.e., D, F, M, and p (as well as the corresponding objective function values TH and Delay). In the terminology of genetic algorithms the string of decision variables is referred to as *chromosome*, while each individual decision variable is referred to as gene. The quality of an individual in the population with respect to the two objective functions is represented by a scalar value, called *fitness*. After generating the initial population (by randomly drawing the decision variables for each individual from uniform distributions over the respective ranges of the decision variables), each individual is assigned a fitness value. The population is evolved repeatedly, generation by generation, using the crossover operation and the mutation operation. The crossover and mutation operations produce offspring by manipulating the individuals in the current population that have good fitness values. The crossover operation swaps portions of the chromosomes. The mutation operation changes the value of a gene. Individuals with a better fitness value are more likely to survive and to participate in the crossover (mating) operation. After a number of generations, the population contains members with better fitness values. The Pareto-optimal individuals in the final population are the outcome of the genetic algorithm. Each operation is discussed in detail in the following subsections.

C. Fitness Function

The fitness function is typically a combination of objective functions. We evaluate three commonly used types of fitness function. We generate G = 20 generations, each with a population size of P = 200 to compare the quality of the fitness functions. We set the probability of crossover to 0.9 and the probability of mutation to 0.05, which are typical values. We compare the genetic algorithm outputs with the true Pareto-optimal solutions which were found by conducting an exhaustive search over all possible combinations of the decision variables. We fix $\sigma = 0.6$ and q = 0.1 for this evaluation. All results presented in this paper assume a channel spacing of 200 GHz, i.e., 1.6 nmat 1.55 μm . Thus, we can use 7 – 10 wavelengths at each AWG input port with fast tunable transceivers with a tuning range of $10-15 \ nm$ [69]. For all subsequent results, the number of wavelengths is fixed at eight, i.e., $\Lambda = 8$. D can take the values 2, 4, and 8. Thus, the corresponding R values are 4, 2, and 1. We fix the number of nodes in the network at N = 200. To reasonably limit the search space of the genetic algorithm, we restrict F to be smaller than 400 slots in this paper. We note that with a large F, the considered network generally achieves larger throughput values (at large delays), however, the computational effort for evaluating a given parameter combination increases as Fincreases. For the exhaustive search, we therefore limit Fto values less than or equal to 200 slots.

First, we evaluate the Vector Evaluated Genetic Algo-

rithm (VEGA), which is easy to implement. The VEGA algorithm divides the population into two subpopulations according to our two objective functions. The individuals in each subpopulation are assigned a fitness value based on the corresponding objective function. When using only one objective function to determine the fitness values of the individuals in a subpopulation, it is likely that solutions near the optimum of an individual objective function are preferred by the selection operator. Such preferences take place in parallel with other objective functions in different subpopulations. The main disadvantage of VEGA is that typically after several generations, the algorithm fails to sustain diversity among the Pareto-optimal solutions and converges near one of the individual solutions. Indeed, as reported in Table II, the VEGA finds only 15 Pareto-optimal solutions; the efficient frontier spanned by these solutions is plotted in Fig. 6. We observe, however, that the VEGA efficient frontier is overall quite close to the true efficient frontier (found by exhaustive search).

Next, we evaluate the Weight Based Genetic Algorithm (WBGA) which uses the weighted sum of the objective functions as fitness function. The main difficulty in WBGA is that it is hard to choose the weight factors. We use the same weight factor of 1/2 for each objective function. Since the mean delay should be minimized in our problem, we use the negative delay as the second objective function. The fitness function used is

$$Fitness = \frac{1}{2} \cdot TH - \frac{1}{2} \cdot Delay.$$
(10)

Our goal is to maximize the average throughput while minimizing the mean delay. Thus, with the WBGA approach, the larger the fitness value, the better. We observe from the results given in Fig. 6 and Table II that the WBGA finds more Pareto-optimal solutions than VEGA. However, the WBGA efficient frontier has parts (particularly in the throughput range from 7–13 packets/frame) that are distant from the true efficient frontier. We note that the average network delay given in (8) in units of slots is on the order of thousands of slots in typical scenarios, whereas the average throughput is typically on the order of one to 16 packets per frame. To achieve a fair weighing of both throughput and delay in the fitness function, we use the delay in unit of cycles (where one cycle corresponds to $D \cdot F$ slots) in the evaluation of the fitness in (10) (and the following fitness definition in (11); with this scaling, the delay is on the order of 1 to 20 cycles in typical scenarios.

Finally, we evaluate the Random Weight Genetic Algorithm (RWGA) which weighs the objective functions randomly. A new independent random set of weights is drawn each time an individual's fitness is calculated. We use the fitness function

$$Fitness = \varepsilon \cdot TH - (1 - \varepsilon) \cdot Delay, \tag{11}$$

where ε is uniformly distributed in the interval (0, 1). We observe from Fig. 6 that the RWGA efficient frontier is

```
Genetic Algorithm()
ł
    t = 0:
                                           //start with an initial generation
    init_population \mathcal{P}(t);
                                           //initialize a usually random population of individuals
    evaluate \mathcal{P}(t);
                                           //evaluate fitness of all individuals of initial population
    while not terminated do {
                                           //evolution cycle;
          t \leftarrow t + 1;
                                           //increase the generation counter
          \mathcal{P}'(t) = select_parents \mathcal{P}(t); //select a mating pool for offspring production
         recombine \mathcal{P}'(t);
                                           //recombine the 'chromosome' of selected parents
         mutate \mathcal{P}'(t);
                                           //perturb the mated population stochastically
          evaluate \mathcal{P}'(t);
                                           //evaluate fitness of new generation
          \mathcal{P}(t) \leftarrow \mathcal{P}'(t);
    }
}
```

Fig. 5. Basic structure of a Genetic Algorithm

relatively far from the true efficient frontier in the throughput range from 8–10 packets/frame. Also, the RWGA finds only a relatively small number of Pareto–optimal solutions.

We now study the concept of *elitism*. Elitism is one of the schemes used to improve the search; with elitism the good solutions in a given generation are kept for the next generation. This prevents losing the already found good solutions in the subsequent crossover operation(s), which may turn good solutions into bad solutions. For each generation we determine the Pareto-optimal solutions by comparing the throughput and delay achieved by the individuals in that generation. (Note that the thus determined Pareto-optimal solutions are not necessarily the true Pareto-optimal solutions to the optimization problem, rather they are Pareto-optimal with respect to the other individuals in the considered generation.) The determined Pareto-optimal solutions are kept for the next generation; they are not subjected to the crossover operation, they are, however, subjected to the mutation operation (as explained in Sections III-E and III-F). If we find that a Pareto-optimal solution from a previous generation is no longer Pareto-optimal solution in a new generation, i.e., it is dominated by some other individual in the new generation, then this old Pareto-optimal solution is discarded.

The results obtained with elitism are given in Fig. 7 and Table II. We observe that the number of Pareto– optimal solutions in the final population is dramatically larger and the efficient frontiers are closer to the true efficient frontier of the problem. From Fig. 7, it appears that all schemes with elitism perform quite well, with RWGA hugging the true efficient frontier most closely. This observation is corroborated by comparing the number of Pareto– optimal solutions in the final population in Table II, which indicates that RWGA gives the best performance. According to the observations made in this section, we use RWGA with elitism throughout the remainder of this paper.



Fig. 6. Efficient frontiers obtained with different fitness functions without elitism for $F \leq 400$ and with exhaustive search for $F \leq 200$

D. Population Size and Number of Generations

The population size trades off the time complexity (computational effort) and the number of optimal solutions. In order to accommodate all Pareto–optimal solutions, the population should be large enough. However, as the population size grows, the time complexity for processing a generation increases (whereby the most computational effort is typically expended on evaluating the throughput and delay achieved by an individual to determine its fitness value). On the other hand, for a smaller population, the time complexity for the population decreases while the population may lose some Pareto–optimal solutions. As a result, the smallest population size which can accommodate all Pareto–optimal solutions is preferable.

For schemes that employ elitism, we categorize the population in generation t into three groups. (i) The elite group of size $P_e(t)$ which contains the Pareto–optimal solutions from the preceding generation t - 1, (ii) the reproduction group of size $P_p(t)$ which is reproduced from the individuals with good fitness values in the preceding generation t - 1 through crossover (see Section III-E), and (iii) the

Number of Pareto–Optimal Solutions in Final Population for Genetic Algorithm based Search with $F \le 400$; Exhaustive Search for F < 200 Gives 580 Pareto–optimal Solutions

VEGA	WBGA	RWGA	VEGA with Elitism	WBGA with Elitism	RWGA with Elitism
15	23	13	55	82	115



Fig. 7. Efficient frontiers obtained with different fitness functions with elitism for $F \le 400$ and with exhaustive search for $F \le 200$

random group of size, $P_r(t)$ which is generated randomly (by drawing the decision variables from uniform distributions over their respective ranges). The random group is required to prevent the algorithm from getting stuck in local optima. The population size should accommodate these three groups appropriately. Furthermore, the size of the reproduction group and the random group need to be carefully considered. If the reproduction group is too large, the solution may get stuck in a local optimum. If the size of the random group is too large, we may spend most of the time calculating the fitness values of solutions that are very distant from the efficient frontier. However, the population size should at least be larger than the elite group. To find the proper population size, we evaluate the adopted RWGA with elitism for the population sizes P = 150, 200, and 300. We initially set the size of the reproduction group to one half of the population size, i.e., $P_p^{\text{init}} = P/2$. Once the number of Pareto-optimal solutions in a generation t-1exceeds P_p^{init} , i.e., $P_e(t) > P_p^{\text{init}}$, we set the size of the reproduction group to $P_p(t) = P - P_e(t)$ in the next generation. Thus $P_p(t) = \min(P_p^{\text{init}}, P - P_e(t))$. If the number of Pareto-optimal solutions in a generation t-1 is less than $P - P_p^{\text{init}}$, we set the size of the random group to $P_r(t) = P - P_p^{\text{init}} - P_e(t)$ in the next generation, otherwise we set $P_r(t) = 0$; i.e., $P_r(t) = \max(0, P - P_p^{\text{init}} - P_e(t))$. Thus, the more Pareto-optimal solutions there are in the preceding generation, the fewer randomly generated individuals are in the next generation. (If the number of Pareto-optimal solutions in a generation exceeds P_n^{init} , the succeeding generation does not contain randomly generated individuals.) For the following evaluation, the parameters

 Λ , σ , q, and the ranges of D, F, M, and p are set as given in Section II-C. For comparison, we set the number of generations to G = 20, 15, and 10, respectively. Thus, the total number of considered individuals is $P \cdot G = 3000$ in all cases. The results are shown in Fig. 8. We observe from Fig. 8 that all three efficient frontiers hug the true Pareto-optimal frontier quite closely, with all three curves having "humps" around a throughput of 14 packets/frame. The number of Pareto-optimal solutions obtained for the population sizes P = 150, 200, and 300 are 87, 104, and 70, respectively. The population size of P = 150 does not perform very well in our network optimization because it typically can not accommodate all the Pareto-optimal solutions. This is because the elite group takes up almost two thirds of the population. With a population size of P = 300 (and only G = 10 generations to ensure a fair comparison) the evolution of the generations does not settle down as much as for 20 and 15 generations and therefore gives only 70 Pareto-optimal solutions (although the efficient frontier has a relatively small "hump"). Overall, we conclude that all three considered population sizes give fairly good results. We choose P = 200 for the following experiments in this paper as it appears to accommodate all three population groups in a proper fashion. In Fig. 9 we plot the efficient frontiers obtained with different initial sizes $P_n^{\text{init}} = 50$ and 100 of the reproduction group (with P = 200, fixed). The number of Pareto-optimal solutions for $P_n^{\text{init}} = 50$ and 100, are 85 and 115, respectively. We observe from Fig. 9 that both efficient frontiers are quite close to the true Pareto-optimal frontier. We set $P_n^{\text{init}} = 100$ for all the following experiments in this paper.



Fig. 8. Efficient frontiers for different population sizes P with $P\cdot G=3000,$ fixed



Fig. 9. Efficient frontiers for different initial sizes P_p^{init} of the reproduction group (Population size P = 200, fixed)

We now investigate the impact of the number of generations G. In Fig. 10, we plot the size of the elite group $P_e(t)$ as a function of the generation counter t. Recall that $P_e(t)$ is defined as the number of Pareto-optimal solutions in generation t-1; thus $P_e(1)$ is the number of Pareto-optimal solutions in the initial generation t = 0. In Fig. 11, we plot the sum of the fitness values of the individuals in the elite group $P_e(t)$ as a function of the generation counter. We observe from Fig. 10 that the number of Pareto-optimal solutions in a generation first steadily increases and then settles on a fixed value as the generations evolve. (The slight drop around the 15th generation is because we found a Pareto-optimal solution which dominates several earlier Pareto-optimal solutions.) We observe from Fig. 11 that the sum of the fitness values of the Pareto-optimal solutions in a generation first increases quickly, then fluctuates, and finally settles down as the generations evolve. This behavior is typical for genetic algorithm based optimization and is due to the random nature of the evolution of the population. To allow for the evolution to settle down sufficiently, we set the total number of generations to G = 40. According to the decisions made in this section, we set the population size to P = 200, the number of generations to G = 40, and the initial size of the reproduction group to $P_p^{\text{init}} = 100.$

E. Crossover Operation

The crossover operation swaps parts of the chromosomes of the fittest individuals in the current generation to produce offspring with large fitness values for the reproduction group in the next generation. In our crossover operation the individuals in the generation t - 1 are sorted in decreasing order of their fitness values (whereby the individuals from all three groups, i.e., elite group, reproduction group, and random group, are considered). A mating pool is formed from the first $P_p(t)$ individuals in the ordering. Parts of the chromosomes of the individuals in the mating pool are then exchanged (swapped) with a fixed crossover



Fig. 10. Size of elite group $P_e(t)$ as a function of generation counter t



Fig. 11. Sum of fitness values of individuals in elite group as a function of the generation counter t

probability. We chose to swap their M values because we have observed that M (with D, F, and p fixed) tends to explore potential solutions in the vicinity of the parents (as is also evidenced by the tables in the Appendix, which are discussed in detail in Section IV). More specifically, the first $P_p(t)$ individuals in the ordering, i.e., the mating pool, are processed as follows. We take the first two individuals in the ordering. With the crossover probability (which we fix at the typical value 0.9), we swap their M values, i.e., we put the M value of the first individual (in the ordering) in place of the M value of the second individual, and vice versa. The other three decision values, D, F, and p, in the individuals' chromosomes remain unchanged. (Note that in our problem the swapping of M while keeping D, F, and p in place may result in a chromosome that violates the constraint $M \leq F$. If this situation arises, we discard the violating M value and randomly draw a new M from a uniform distribution over [1, F].) With the complementary crossover probability (0.1), the chromosomes of the two individuals remain unchanged. The two individuals (irrespective of whether their chromosomes were swapped or not) then become members of the reproduction group in the next generation. We then move on to the third and

fourth individuals in the ordering, and swap their M values with probability 0.9, move them to the reproduction group in the next generation, and so on. We note that the elite group of the next generation is formed from the Pareto– optimal individuals in the current generation, irrespective of whether these individuals are in the mating pool of the current generation. (An individual may appear twice in the next generation if it is Pareto–optimal in the current generation and participates in the crossover operation without having the M value changed. Only one copy of such a "duplicate" individual is processed in the next generation, the other copy is discarded.)

F. Mutation Operation

The mutation operation keeps diversity in the population by changing small parts in the individuals' chromosomes with a given (typically small) mutation probability. We mutate each individual in the elite group, the reproduction group and the random group with a mutation probability of 0.05 (a typical value). The mutation is typically performed by flipping a bit in the binary representation of the individual's chromosome. The location of the bit is typically drawn from a uniform distribution over the length of the chromosome. We chose not to use bitwise mutation because bitwise mutation would frequently produce offspring that are distant from the parents. Instead, we implement the mutation operation by randomly drawing an M value from a uniform distribution over [1, F]. This operation does not result in constraint violations, yet tends to keep the population sufficiently diverse.

After the mutation operation, we evaluate the average throughput and mean delay achieved by the individuals (in all three groups, i.e., elite group, reproduction group, and random group) in the new generation and start the next evolution cycle; as illustrated in Fig. 5. In this new evolution cycle, we select again the individuals with the largest fitness values for the crossover operation, which gives the reproduction group of the next generation. We also determine again the Pareto–optimal individuals to form the elite group in the next generation.

IV. NUMERICAL RESULTS

In this section, we employ the genetic algorithm based methodology developed in the preceding section to optimize the AWG-based single-hop WDM network. We determine the settings of the network architecture parameter D and the protocol parameters F, M, and p that give Pareto-optimal throughput-delay performance. We use the random weight genetic algorithm (RWGA) with elitism with the parameter settings found in the preceding section, i.e., a population size of P = 200, G = 40 generations, crossover probability 0.9, and mutation probability 0.05. Data packets can have one of two lengths. A data packet is F slots long with probability q, and K = F - Mslots long with probability (1 - q). To reasonably limit the search space we restrict F to be no larger than 400 slots. The number of nodes in the network is set to N = 200 and the transceiver tuning range is fixed at $\Lambda = 8$ wavelengths.

In the first set of optimizations, we determine the Pareto-optimal performance for different (but fixed) combinations of traffic load σ and fraction of long packet traffic q. Specifically, we optimize the network for a light traffic scenario with $\sigma = 0.1$, a medium traffic scenario with $\sigma = 0.3$, and heavy load scenarios with $\sigma = 0.6$ and $\sigma = 0.8$. For each traffic load level, we consider the fractions q = 0.1, 0.5, and 0.9 of long packet traffic. In these optimizations we determine the free decision variables D, F, M, and p that give the Pareto-optimal solutions.

To put the optimizations for fixed σ and q in perspective, we also conduct an optimization where the traffic load σ and the fraction q of long packet traffic are free decision variables (in addition to D, F, M, and p). This optimization gives the best achievable network performance, which we refer to as *network frontier*. Loosely speaking, the network frontier gives the Pareto-optimal performance when the network is "fed optimally" with traffic. (To find the network frontier, we exchange (swap) σ as well as M in the crossover operation and use a population size of P = 400rather than P = 200 to accommodate the larger chromosome.) The detailed solutions for the network frontier are given in Table IV in the Appendix.

A. Pareto-optimal Performance for Light Traffic Load

Fig. 12 shows the Pareto-optimal throughput-delay frontier for a light traffic load of $\sigma = 0.1$ for q = 0.1, 0.5, and 0.9 (along with the network frontier). Tables V, VI, and VII in the Appendix give the individual Paretooptimal solutions. The numbers of Pareto-optimal solutions with each D = 2, 4, and 8 are shown in Table III. We observe from Fig. 12 that for a small fraction q of long packets the network is able to achieve relatively small delays (of less than 1500 slots) even for large throughputs (of 8 packets/frame and more). When the fraction q of long packet traffic is large, however, the smallest achievable delays become very large (up to 2250 slots) for large throughputs. This is because the considered network allows for the scheduling of at most $R (= \Lambda/D)$ long packets in a cycle (consisting of D frames) at each of the D AWG input ports. (There are also $(D-1) \cdot R$ transmission slots exclusively for short packets in a cycle at each AWG input port; in addition short packets can fill up the R long packet transmission slots.) With a larger fraction of long packets, the probability increases that a data packet fails in the scheduling and requires re-transmission of the corresponding control packet, resulting in larger delays.

We also observe that the light traffic scenario is able to achieve the small delay (and small throughput) part of the network frontier. This is because a small number M of control slots is sufficient to ensure reasonably large success probabilities in the control packets contention when the



Fig. 12. Efficient frontiers for light traffic load $\sigma = 0.1$ for different fractions q of long packet traffic and network frontier (with σ and q as free decision variables).

probability σ of an idle node generating a new packet at the beginning of a cycle is small. The small M in turn allows for small frame length F, and thus short cycle length $D \cdot F$, which results in small delays.

We observe that there are some instances where the Pareto–optimal frontier for q = 0.9 dominates the network frontier, e.g., around a throughput of 7.7 packets/frame. This is due to the stochastic nature of the genetic algorithm, which finds a very close approximation of the true optimal frontier in a computationally efficient manner. By definition, the true network frontier can not be dominated by the true frontier for a fixed σ or q; finding these true frontiers, however, is computationally prohibitive.

We observe from Tables III, V, VI, and VII that for the considered light traffic load $\sigma = 0.1$, most of the Paretooptimal solutions have D = 2. However, for a larger fraction q of long packet traffic the number of Pareto-optimal solutions with D = 4 increases. We observe from the Table VII that D = 4 is the best choice to achieve low delay service. This is because the long packets are more difficult to schedule and therefore tend to require more re-transmissions of control packets, resulting in increased mean delay. Recall that a control packet is discarded if the corresponding data packet cannot be scheduled. This makes the control packet contention a bottleneck when the packet scheduling becomes difficult. With larger D, fewer nodes S = N/D contend for the M control slots available to them every Dth frame. This increases the probability of successful control slot contention, thus relieving the control packet contention bottleneck. Note that the control packet contention bottleneck could also be relieved by reducing the re-transmission probability p. However, we see from the results in Tables VI and VII that this strategy is not selected (except in the 9th row of Table VII when the transition from D = 4 to D = 2 occurs). The reason for this is that the smaller p would result in a relative large increase in the mean delay, making it preferable to increase D and keep p large (the first eight rows of Table VII).

Generally, we observe from Tables V, VI, and VII that the Pareto-optimal solutions with larger throughput are achieved for larger F. The Pareto-optimal M values, on the other hand, remain in the range 30-60 for q=0.1 and q = 0.5 and are typically 30 - 80 for q = 0.9, even for very large F. Upon close inspection we discover an interesting underlying trend in the F and M solutions as we move along the efficient frontier from small to large throughput values. The frame length F typically makes a jump to a new value (e.g., from F = 44 to 59 in the 4th row of Table V) and stays around the new value for a few solutions. For F (almost) fixed, several distinct Pareto-optimal solutions are obtained for decreasing M values (from M = 49 to 30 for F around 59 in Table V). Once F makes a jump (to values around 100 in line 20), M is reset to a larger value (of 50 in line 20). The explanation of this behavior is as follows. For large M, the probability of successful control packet contention is large, and the probability of control packet re-transmission is small, giving small delays. However, for large M, the length K = F - M of a short packet is small, resulting in a small contribution of a short packet to the throughput (Equation (1)). Now as M decreases (for F fixed), control packet re-transmission becomes more likely, increasing the mean delay, while the contribution of a short packet to the throughput increases. We also observe from the tables that for optimal network operation the re-transmission probability p should be in the range from 0.75 to 1.0.

B. Pareto-optimal Performance for Medium Traffic Load

Fig. 13 shows the Pareto-optimal solutions for a medium traffic load of $\sigma = 0.3$. The numbers of Pareto-optimal solutions with D = 2, 4, and 8 are shown in Table III and the individual Pareto-optimal solutions are given in Tables VIII, IX, and X in the Appendix. We observe from Fig. 13 that the differences in performance for the different fractions q of long packet traffic are more pronounced for the larger traffic load $\sigma = 0.3$, compared to the light traffic load $\sigma = 0.1$ shown in Fig. 12. For $\sigma = 0.1$, the efficient frontiers for q = 0.1 and q = 0.5 roughly overlap and give both a smallest achievable delay of roughly 715 slots for a throughput of 8 packets/frame. For $\sigma = 0.3$, on the other hand, the efficient frontier for q = 0.1 clearly dominates, giving a smallest achievable delay of roughly 555 slots for a throughput of 8 packets/frame, whereas the corresponding smallest achievable delay for q = 0.5 is more than twice as large. This increasing gap in performance is again due to the fact that long packets are more difficult to schedule and thus tend to cause larger delays. The smaller delay of 555 slots for $\sigma = 0.3$, compared to 715 slots for $\sigma = 0.1$ is achievable because with the larger σ , the throughput level of 8 transmitting nodes per slot is reached with smaller sized packets (i.e., smaller F and smaller K = F - M), thus reducing the cycle length and in turn the delay. We observe from Tables VIII, IX, and X that small delays are

	1	- Chibblit	01 1 11	0	1 1101711	00101	10110 11		- 2, 1,			
	0	$\sigma = 0.1$	1	0	$\sigma = 0.3$	3	($\sigma = 0.6$	3	0	$\sigma = 0.8$	3
q	0.1	0.5	0.9	0.1	0.5	0.9	0.1	0.5	0.9	0.1	0.5	0.9
D=2	148	132	133	108	84	158	31	102	121	23	105	135
D=4	0	1	8	2	65	4	86	46	5	102	46	3
D = 8	0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			2	2	1	4	1	0	4	1
Total	148	133	141	110 151 164 118 152 127 125 153						155	139	

TABLE III NUMBER OF PARETO-OPTIMAL SOLUTIONS WITH D = 21 AND S

again achieved for large D values. For q = 0.5 and q = 0.9, the first few Pareto-optimal solutions at the top of the tables have D = 8, then D = 4 is optimal as we go down the tables to larger delays. As in the case of $\sigma = 0.1$, this behavior is due to the control packet contention and data packet scheduling bottlenecks. From Table III we observe that there is no clear trend in the number of solutions with D=2 and D=4. This appears to be due to the stochastic nature of the genetic algorithm approach, which finds a large total number of solutions for q = 0.5, with many solutions being tightly spaced in the region where D = 4 is optimal. As before, larger throughput is optimally achieved for large F. The optimal settings of M are typically in the range from 60 - 80. The optimal settings of p are mostly 0.95 for q = 0.1 and q = 0.5. For q = 0.9, the optimal p settings are typically 0.7. This smaller p setting for a medium load of predominantly long packet traffic is better as it somewhat abates the control packet contention bottleneck at the expenses of slightly larger delays, as discussed above.

D D D



Fig. 13. Efficient frontiers for medium traffic load $\sigma = 0.3$ for different fractions q of long packet traffic and network frontier (with σ and q as free decision variables).

C. Pareto-optimal Performance for Heavy Traffic Load

Figs. 14 and 15 show the Pareto–optimal solutions for a heavy traffic load of $\sigma = 0.6$ and $\sigma = 0.8$, respectively. The number of Pareto–optimal solutions with D = 2, 4, and 8are given in Table III. The complete parameter vectors corresponding to the Pareto-optimal solutions are given in

Tables XI – XVI. We observe from the figures and the tables that both considered heavy load scenarios give similar results with the $\sigma = 0.8$, q = 0.1 scenario attaining the larger throughput region of the network frontier. We notice that with an increasing fraction q of long packet traffic, the number of Pareto-optimal solutions with D = 2 increases, while the number of solutions with D = 4 decreases. There are two primary effects at work here. On the one hand, a larger D allows for a larger throughput. To see this, note that the considered network allows for the scheduling of at most $R (= \Lambda/D)$ long packets at each of the D AWG input ports within one cycle (consisting of D frames); for a total of at most $D \cdot R = \Lambda$ scheduled long packets per cycle in the entire network. The network also allows for the scheduling of at most $(D-1) \cdot R$ short packets at each of the D AWG input ports within one cycle; for a total of at most $D \cdot (D-1) \cdot R = \Lambda \cdot (D-1)$ scheduled short packets per cycle in the network (in addition short packets may take up long packet transmission slots). Thus, for a larger D the network allows for the scheduling of more short packets and thus for an overall larger throughput; this is a result of the spatial reuse of all Λ wavelengths at all D AWG ports.



Fig. 14. Efficient frontiers for heavy traffic load $\sigma = 0.6$ for different fractions q of long packet traffic and network frontier (with σ and q as free decision variables).

On the other hand, a larger D increases the delay in the network (provided the frame length F is constant). This is because a larger cycle length $D\cdot F$ increases the delay incurred by the control packet pre-transmission coordination and re-transmissions, which operate on a cy-



Fig. 15. Efficient frontiers for heavy traffic load $\sigma = 0.8$ for different fractions q of long packet traffic and network frontier (with σ and q as free decision variables).

cle basis. These throughput and delay effects combine to make D = 2 the better choice when long packets dominate (i.e., when q is large), since short packets make only a small contribution to the throughput. We also observe from Tables XI and XIV that even when q is small, D = 2is a good choice for delay sensitive traffic. Although we see that some Pareto-optimal solutions in the small delay range have D = 4. This indicates that both a 2×2 AWG and a 4×4 AWG based network can achieve small delays for traffic consisting mostly of short packets, provided the protocol parameters F, M, and p are set properly. On the other hand, only a 4×4 AWG based network achieves the large throughputs on the efficient frontier for small q (i.e., predominantly short packet traffic). As before, we observe that the Pareto-optimal solutions with larger throughput values have larger frame lengths F. Also, as before, the Pareto-optimal solutions have typically between M = 60and 110 control slots per frame. We note, however, some differences in the optimal setting of the re-transmission probability p in this heavy traffic load scenario compared to the light/medium load scenario. As before for q = 0.1the optimal p setting is typically in the range of 0.9 - 1.0. For q = 0.5 and q = 0.9, however, the optimal p is now typically in the range from 0.6 to 0.95.

D. Pareto-optimal Planning of the Network Architecture

We now study the proper setting of the AWG degree Din detail. The setting of this network architecture (hardware) parameter has a profound impact on the network performance, as the results discussed so far illustrate. Importantly, once the network hardware for a particular Dvalue has been installed, it is very difficult and costly to change D; whereas the protocol parameters F, M, and pcan easily be changed by modifying the network protocol (software). For this reason, the proper setting of D warrants special attention. We have observed so far that for predominantly long packet traffic (i.e., large q), D = 2 is the best choice for all levels of traffic load σ . For predominantly short packet traffic (i.e., small q), on the other hand, the choice is not so clear. For light traffic loads, D = 2 is the best choice, whereas for heavy traffic loads, D = 4turns out to be the best choice.

To explore the optimal setting of D as a function of the traffic load σ , we plot in Figs. 16 and 17 the percentage of Pareto-optimal solutions with D = 2, 4, and 8 for q = 0.1and q = 0.9, respectively. We observe from Fig. 16 that for σ less than 0.4, most Pareto-optimal solutions have D = 2, whereas for σ larger than 0.4, most Pareto-optimal solutions have D = 4. The explanation of this behavior is as follows. For light traffic loads, D = 2 is preferred as it achieves smaller delays while at the same time providing sufficient resources for control packet contention and data packet scheduling. (Recall that S = N/D nodes at an AWG input port content for the M control slots available to them in one frame (out of the D frames in a cycle), and that spatial wavelength reuse provides for $\Lambda \cdot (D-1)$ transmission slots for short packets.) As the traffic load increases, however, the control packets contention and data packet scheduling become increasingly bottlenecks which are relieved for larger D.



Fig. 16. Percentage of Pareto–optimal solutions with D=2, 4, and 8 as a function of the traffic load σ . (fraction of long packet traffic q=0.1)

E. Pareto-optimal MAC Protocol Tuning (Network Operation) for Fixed Network Architecture

Next, we fix the AWG degree D at D = 2 and D = 4, and allow only the protocol parameters F, M, and p to vary (i.e., only F, M, and p are decision variables, D is fixed). We employ our genetic algorithm based methodology to obtain the Pareto-optimal throughput-delay frontiers in these settings; we refer to these efficient frontiers as the $2 \\ \times 2$ network frontier and the $4 \\ \times 4$ network frontier, respectively. We compare the thus obtained efficient frontiers with the efficient frontier obtained when both the hardware parameter D and the software parameters F, M, and p are decision variables, which we refer to as optimal frontier. We compare the $2 \\ \times 2$ frontier and the $4 \\ \times 4$ frontier with the optimal frontier in Fig. 18 (a) - (h). The correspond-



Fig. 17. Percentage of Pareto–optimal solutions with D = 2, 4, and 8 as a function of the traffic load σ . (fraction of long packet traffic q = 0.9)

ing Pareto-optimal solutions are tabulated in Tables XVII – XXXII. A number of observations are in order. First, as expected the 2×2 frontier approximately coincides with the optimal frontier for light to medium loads of predominantly short packet traffic, and all load levels of predominantly long packet traffic. For heavy loads of predominantly short packet traffic, on the other hand, the 4×4 network frontier achieves the optimal frontier, as we expect from our earlier results. We also observe that there are some instances where the optimal frontier is dominated by the 2×2 network frontier or the 4×4 network frontier, e.g., in Fig. 18 (c) around a throughput of 11.5 packets/frame. These instances are again due to the stochastic nature of the employed genetic algorithms. By definition, the 2×2 network frontier and the 4×4 network frontier can not dominate the true optimal frontier, which however could only be found by a computationally prohibitive exhaustive search. The genetic algorithm methodology finds a very close approximation of the true optimal frontier in a computationally efficient manner.

Figs. 18 (a)-(h) give also a number of surprising results, which we would not expect, based on our earlier observations. First, the 4×4 network is able to come close to the optimal frontier for medium and heavy loads of predominantly long packet traffic, which is a surprise given the results in Table III and Fig. 17. The 4×4 network achieves this by properly tuning its three protocol parameters, F, M, and p, as detailed in Tables XX, XXIV, XXVIII, and XXXII. Overall, the 4×4 network shows some flexibility in achieving good performance close to the optimal frontier for medium to heavy loads of both short and long packet traffic by properly tuning the protocol parameters (in software). For light traffic loads, however, the 4×4 network is not able to come close to the optimal frontier. The 2×2 network, on the other hand, appears to be more flexible than the 4×4 network. By properly tuning its protocol parameters, the 2×2 network is able to come fairly close to the optimal frontier even for heavy loads of short packet traffic (see Figs. 18 (e) and (g)). Overall, our results indicate that the 2×2 network is the best choice for achieving efficient multi–service convergence in a metro WDM network. The 2×2 network frontier approximately coincides with the optimal frontier for all load levels of long packet traffic and for light to medium loads of short packet traffic. For heavy loads of short packet traffic, the 4×4 network attains the optimal frontier. But the 2×2 network is able to come fairly close to the optimal frontier, simply by adjusting its protocol parameters in software.

V. CONCLUSION

We have developed a genetic algorithm based methodology for the multi–objective optimization problem of maximizing throughput while minimizing delay in an AWG– based metro WDM network. Our methodology finds the Pareto–optimal throughput–delay trade–off curve in a computationally efficient manner. The optimal trade–off curve can be used to optimally provide varying degrees of small delay (and moderate throughput) or large throughput (and moderate delay) packet transport services. Our methodology thus facilitates efficient multi–service convergence for increased cost–effectiveness in metropolitan and local area networks.

Specifically, for the AWG based network considered as an example throughout this paper, we find that a network based on a 2×2 AWG is most flexible in efficiently providing different transport services under a wide range of traffic loads and packet size distributions. In addition, using an AWG with the minimum degree of D = 2 minimizes the network cost (see Section II-D) which is an important consideration in cost-sensitive metro WDM networks.

For a fixed network hardware the different transport services are achieved by optimally tuning the MAC protocol parameters (software) according to the found Pareto– optimal solutions. In particular, small frame lengths in the timing structure of the AWG network's MAC protocol give Pareto–optimal performance with small delay (and moderate throughput), while large frame lengths achieve optimal performance with large throughput (and moderate delays). The optimal number of control packet contention slots per frame is typically in the range from 30 to 80. The optimal control packet re–transmission probabilities are close to one for light traffic loads and in the range from 0.6 -0.75 for heavy loads.

The developed genetic algorithm methodology can be applied in analogous fashion to networks with a similar throughput–delay trade–off. The methodology is especially useful for the multi–objective optimization of networks with complex, highly non–linear characterizations of the network throughput and delay.

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Fig. 18. Optimal frontier (with D a free decision variable), 2×2 network frontier (with D = 2, fixed), and 4×4 network frontier (with D = 4, fixed) for different (fixed) traffic loads σ and fractions q of long packet traffic.

assisting us in the implementation of our methodology in a C program.

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Appendix

I. Objective Functions for M = F

In this appendix, we derive the objective functions mean throughput and mean delay for the special case M = F. In case M = F, the length K of a short packet degenerates to zero and hence short packets do not contribute to the throughput. There are different scenarios for evaluating the network performance for the case M = F. One scenario is to still consider short packets in the control packet contention. In this scenario, the packet generation probability is unchanged at σ ; and all short packets that are successful in the control slot contention are successfully scheduled, i.e.,

$$E[\mathcal{S}] = \sum_{k=0}^{M} (1 - \tilde{q}) \cdot k \cdot P(Z = k) =: h(\tilde{q}, \beta) \quad (12)$$

(which replaces Eqn. (5) in Section II-B).

An alternative scenario is to completely ignore short packets and to consider only long packets in the control slot contention and data packet scheduling. In this alternative scenario the packet generation probability is effectively $q \cdot \sigma$, and each generated packet is long with probability one. (The network equilibrium condition is $q \cdot \frac{\sigma}{D} \cdot E[\eta] = E[\mathcal{L}]$ in this scenario.)

We consider the first scenario, where control packets are sent for short packets (of length zero), in our network optimization in this paper. We chose the first scenario because it ensures that the packet generation probability and thus the level of control packet contention are the same both for the case M = F and the case M < F. The alternative scenario would result in a reduced level of control packet contention in the case M = F (especially when q is small) and thus an unfair performance comparison.

II. TABLES FOR PARETO-OPTIMAL SOLUTIONS

D	F	M	p	σ	q	TH	Delay	D	F	M	p	σ	q	TH	Delay
4	17	16	0.90	0.10	0.10	0.7145	115.8411	2	225	57	1.00	0.15	0.20	10.3502	916.6104
2	32	30	0.90	0.10	0.10	1.4367	120.0612	2	228	58	1.00	0.15	0.20	10.3625	920.9398
2	41	36	0.90	0.10	0.10	1.9752	132.7913	2	223	57	1.00	0.15	0.20	10.3848	928.8318
2	37	31	0.90	0.10	0.10	2.2737	134.4635	2	225	55	1.00	0.15	0.20	10.3913	933.6846
4	23	21	1.00	0.10	0.55	2.7933	142.1494	2	228	56	1.00	0.15	0.20	10.4055	937.2099
2	50 50	39	0.80	0.10	0.15	3.1624	165.6575	2	225	54 55	1.00	0.15	0.20	10.4092	943.0707 946.1338
2	44	43	1.00	0.10	0.55	5.0891	176.7281	2	228	54	1.00	0.15	0.20	10.4417	955.6449
2	44	39	1.00	0.10	0.55	5.4073	186.3178	2	251	65	1.00	0.15	0.20	10.4474	964.9112
2	44	38	1.00	0.10	0.55	5.4824	189.3144	2	251	64	1.00	0.15	0.20	10.4730	970.8729
2	44	37	1.00	0.10	0.55	5.5552	192.6479	2	246	61 56	1.00	0.15	0.20	10.4924	970.8972
2	44	33	1.00	0.10	0.55	5.8142	210.7215	2	250	61	1.00	0.15	0.20	10.5442	990.6309
2	54	42	1.00	0.10	0.55	5.8919	219.4786	2	246	58	1.00	0.15	0.20	10.5563	993.6456
2	60	45	1.00	0.10	0.55	6.0414	235.9437	2	251	60	1.00	0.15	0.20	10.5658	997.9322
2	54 65	35	1.00	0.10	0.55	6.2799	246.1695	2	246	57	1.00	0.15	0.20	10.5748	1002.1607
2	65	44	1.00	0.10	0.55	6.5221	271.2333	2	240	58	1.00	0.15	0.20	10.6051	1011.2001
2	65	38	1.00	0.10	0.55	6.6082	279.7183	2	246	55	1.00	0.15	0.20	10.6069	1020.8285
2	65	36	1.00	0.10	0.55	6.6843	290.1489	2	251	57	1.00	0.15	0.20	10.6227	1022.5298
2	65 71	34	1.00	0.10	0.55	6.7467	303.3178	2	251 251	55	1.00	0.15	0.20	10.6387	1031.7530
2	80	45	1.00	0.10	0.55	6.8106	314.6119	2	264	61	1.00	0.15	0.20	10.6695	1041.9385
2	80	43	1.00	0.10	0.55	6.8866	321.4020	2	260	57	1.00	0.15	0.20	10.7043	1059.1942
2	80	42	1.00	0.10	0.55	6.9228	325.1686	2	264	58	1.00	0.15	0.20	10.7236	1066.3514
2	80	41 30	1.00	0.10	0.55	6.9575 7.0200	329.3052	2	261	56 64	1.00	0.15	0.20	10.7272	1072.8587
2	80	37	1.00	0.10	0.55	7.0753	350.7444	2	264	57	1.00	0.15	0.20	10.7388	1075.4895
2	80	36	1.00	0.10	0.55	7.0987	357.5131	2	264	56	1.00	0.15	0.20	10.7525	1085.1904
2	92	52	1.00	0.15	0.20	7.1606	365.0482	2	283	64	1.00	0.15	0.20	10.7764	1094.6495
2	98	56 55	1.00	0.15	0.20	7.1768	371.8966	2	278	61 56	1.00	0.15	0.20	10.7913	1097.1928
2	98	54	1.00	0.15	0.20	7.3534	379.7875	2	283	61	1.00	0.15	0.20	10.8319	1116.9265
2	98	53	1.00	0.15	0.20	7.4390	384.1617	2	278	58	1.00	0.15	0.20	10.8387	1122.9003
2	98	52	1.00	0.15	0.20	7.5224	388.8557	2	278	57	1.00	0.15	0.20	10.8517	1132.5230
2	104	56 55	1.00	0.15	0.20	7.5254	394.6658	2	294	64 58	1.00	0.15	0.20	10.8655	1137.1977
2	98	50	1.00	0.15	0.20	7.6822	399.3170	2	283	64	1.00	0.15	0.20	10.8810	1144.9337
2	104	54	1.00	0.15	0.20	7.6879	403.0398	2	296	61	1.00	0.15	0.20	10.9310	1168.2340
2	104	52	1.00	0.15	0.20	7.8425	412.6632	2	309	66	1.00	0.15	0.20	10.9420	1180.8834
2	116	58 65	1.00	0.15	0.20	7.9697	431.9546	2	294	58	1.00	0.15	0.20	10.9569	1187.5277
2	128	64	1.00	0.15	0.20	8.0609	454.8187	2	315	66	1.00	0.15	0.20	10.9849	1203.8132
2	104	46	1.00	0.15	0.20	8.0777	485.1692	2	152	78	0.70	0.60	0.05	11.0368	1208.9706
2	116	54	1.00	0.15	0.20	8.0850	486.2053	2	152	77	0.70	0.60	0.05	11.1314	1214.0486
2	104	45	1.00	0.15	0.20	8.1304	494.0690	2	152	76	0.70	0.60	0.05	11.2224	1219.4886
2	118	52	1.00	0.15	0.20	8.2916	505.5001	2	364	66	1.00	0.15	0.20	11.2827	1391.0730
2	116	49	1.00	0.15	0.20	8.3889	516.3276	4	179	77	0.70	0.60	0.05	11.3135	1393.8773
2	128	56	1.00	0.15	0.20	8.4176	526.1529	4	173	90	0.70	0.85	0.05	11.4318	1408.7031
2	128	55 54	1.00	0.15	0.20	8.4770	531.1628	4	179	90 87	0.70	0.85	0.05	11.8062	1457.5599
2	128	52	1.00	0.15	0.20	8.6443	548.3391	4	194	97	0.70	0.85	0.05	12.1860	1534.6495
2	135	56	1.00	0.15	0.20	8.6526	554.9269	4	194	101	0.70	0.95	0.05	12.2049	1565.8844
2	135	55	1.00	0.15	0.20	8.7073	560.2108	4	199	73	0.70	0.60	0.05	12.2457	1586.8121
2	128	50 49	1.00	0.15	0.20	8.7443	569.7408	4	199	104	0.70	0.95	0.05	12.2805	1589.9627
2	135	50	1.00	0.15	0.20	8.9504	592.8039	4	199	101	0.70	0.95	0.05	12.5050	1606.2423
2	153	58	1.00	0.15	0.20	9.0646	617.9991	4	199	90	0.70	0.85	0.05	12.5746	1664.7491
2	156	58	1.00	0.15	0.20	9.1405	630.1167	4	194	87	0.70	0.95	0.05	12.7661	1703.6212
2	156	55	1.00	0.15	0.20	9.2740	647.3547	4	199	81	0.70	0.95	0.05	13.0629	1751.2576
2	156	54	1.00	0.15	0.20	9.3151	653.8623	4	194	74	0.70	0.85	0.05	13.0660	1756.5210
2	161	56	1.00	0.15	0.20	9.3466	661.8017	4	199	81	0.70	0.95	0.05	13.2787	1796.3931
2	165	58 52	1.00	0.15	0.20	9.3516	668 2883	4	223	90	0.70	0.85	0.05	13.5941	1865.5228
2	165	57	1.00	0.15	0.20	9.3935	672.1809	4	227	85	0.70	0.95	0.05	14.2085	2010.8314
2	165	56	1.00	0.15	0.20	9.4340	678.2440	4	266	97	0.70	0.85	0.05	14.7519	2169.2170
2	165	55	1.00	0.15	0.20	9.4727	684.7021	4	266	95	0.70	0.85	0.05	14.8194	2184.1303
2	165	54	1.00	0.15	0.20	9.4800	691,5852	4	200 266	90	0.70	0.95	0.05	14.8892	2215.4511 2225.2425
2	171	57	1.00	0.15	0.20	9.5194	696.6239	4	266	87	0.70	0.95	0.05	15.3310	2335.8930
2	173	58	1.00	0.15	0.20	9.5208	698.7833	4	266	81	0.70	0.95	0.05	15.3874	2401.2089
2	172	57	1.00	0.15	0.20	9.5395	700.6977	4	302	97	0.70	0.85	0.05	15.6840	2462.7953
2	171	57	1.00	0.15	0.20	9.5594	704.7715	4	302	106	0.70	0.85	0.05	15.7833	2487.2202
2	165	52	1.00	0.15	0.20	9.5776	706.8434	4	302	105	0.70	0.95	0.05	15.8159	2493.9754
2	171	55	1.00	0.15	0.20	9.5936	709.6003	4	302	104	0.70	0.95	0.05	15.8473	2500.9007
2	173	56	1.00	0.15	0.20	9.5965	711.1286	4	302	102	0.70	0.95	0.05	15.9062	2515.2866
2	171	54	1.00	0.15	0.20	9.6281	716.7337	4	310	106	0.70	0.95	0.05	15.9870	2553.1068
2	173	55	1.00	0.15	0.20	9.6320	717.8997	4	310	104	0.70	0.95	0.05	16.0461	2567.1497
2	172	54	1.00	0.15	0.20	9.6470	720.9251	4	310	102	0.70	0.95	0.05	16.1001	2581.9167
2	173	54	1.00	0.15	0.20	9.6657	725.1166	4	302	87	0.70	0.95	0.05	16.1548	2652.0289
2	172	52 52	1.00	0.15	0.20	9.0909	736,8307	4	330	97	0.70	0.85	0.05	16.2952	2091.1339 2709.6354
2	173	52	1.00	0.15	0.20	9.7269	741.1146	4	330	106	0.70	0.95	0.05	16.4532	2717.8234
2	171	50	1.00	0.15	0.20	9.7438	750.8849	4	330	105	0.70	0.95	0.05	16.4777	2725.2049
2	172	50	1.00	0.15	0.20	9.7611	755.2760	4	330	104	0.70	0.95	0.05	16.5011	2732.7723
2	190	57	1.00	0.15	0.20	9.1182	774,0265	4	330	102	0.70	0.95	0.05	10.5438	2756,6606
2	190	56	1.00	0.15	0.20	9.8966	781.0082	4	343	106	0.70	0.95	0.05	16.7271	2824.8892
2	190	55	1.00	0.15	0.20	9.9260	788.4448	4	343	104	0.70	0.95	0.05	16.7683	2840.4270
2	190	54	1.00	0.15	0.20	9.9535	796.3708	4	343	103	0.70	0.95	0.05	16.7871	2848.4926
Z	190	- o2	1.00	0.15	0.20	10.0024	013.9409	4	399	90	0.70	0.85	0.05	10.7907	2941.1049

TABLE IV: Network Frontier: Pareto–Optimal Solutions with σ and q as free decision variables

D	F	M	p	σ	q	TH	Delay	D	F	M	p	σ	q	TH	Delay
2	197	55	1.00	0.15	0.20	10.0323	817.4928	4	359	106	0.70	0.95	0.05	17.0369	2956.6624
2	203	57	1.00	0.15	0.20	10.0651	826.9863	4	359	105	0.70	0.95	0.05	17.0544	2964.6926
2	203	56	1.00	0.15	0.20	10.0921	834.4456	4	359	104	0.70	0.95	0.05	17.0707	2972.9250
2	203	55	1.00	0.15	0.20	10.1175	842.3910	4	359	103	0.70	0.95	0.05	17.0857	2981.3669
2	210	58	1.00	0.15	0.20	10.1356	848.2341	4	359	102	0.70	0.95	0.05	17.0994	2990.0261
2	203	54	1.00	0.15	0.20	10.1411	850.8593	4	381	97	0.70	0.85	0.05	17.1121	3107.0365
2	210	57	1.00	0.15	0.20	10.1623	855.5030	4	359	87	0.70	0.95	0.05	17.1212	3152.5775
2	210	56	1.00	0.15	0.20	10.1874	863.2196	4	386	95	0.70	0.85	0.05	17.1852	3169.4523
2	211	56	1.00	0.15	0.20	10.2005	867.3302	4	386	106	0.70	0.95	0.05	17.5015	3179.0298
2	210	55	1.00	0.15	0.20	10.2109	871.4390	4	386	105	0.70	0.95	0.05	17.5134	3187.6639
2	217	58	1.00	0.15	0.20	10.2283	876.5085	4	386	104	0.70	0.95	0.05	17.5241	3196.5155
2	210	54	1.00	0.15	0.20	10.2325	880.1993	4	386	103	0.70	0.95	0.05	17.5335	3205.5923
2	217	57	1.00	0.15	0.20	10.2532	884.0198	4	386	102	0.70	0.95	0.05	17.5416	3214.9027
2	220	58	1.00	0.15	0.20	10.2662	888.6262	4	399	106	0.70	0.95	0.05	17.7028	3286.0956
2	217	56	1.00	0.15	0.20	10.2765	891.9936	4	400	106	0.70	0.95	0.05	17.7177	3294.3314
2	220	57	1.00	0.15	0.20	10.2904	896.2413	4	400	105	0.70	0.95	0.05	17.7270	3303.2787
2	217	55	1.00	0.15	0.20	10.2982	900.4870	4	400	104	0.70	0.95	0.05	17.7351	3312.4513
2	220	56	1.00	0.15	0.20	10.3130	904.3253	4	400	102	0.70	0.95	0.05	17.7474	3331.5054
2	225	58	1.00	0.15	0.20	10.3272	908.8222	4	400	101	0.70	0.95	0.05	17.7515	3341.4067
2	220	55	1.00	0.15	0.20	10.3339	912.9361								

TABLE IV: continued

D	F	M	p	TH	Delay	D	F	M	p	TH	Delay
-	10	20	0.00	1.1010	100 5405	0	010	20	0.00	F 0905	005 1050
2	40	39	0.90	1.1018	123.5485	2	218	39	0.90	7.9365	685.1076
2	37	34	0.75	1.6017	133.1404	2	220	39	0.90	7.9503	691.3930
-	4.4		0.75	0.0001	146.6609	0	010	0.0	0.00	7.050F	604.0419
2	44	38	0.75	2.0881	146.6693	2	218	38	0.90	7.9585	694.9413
2	59	49	0.75	2.4125	173.2367	2	226	40	0.90	7.9684	700.8297
-	50	40	0.75	0.5550	174 0084	0	000		0.00	7.0700	701 91 60
4	- 59	40	0.75	2.3332	174.0934	4	220	30	0.90	1.9120	701.3109
2	59	47	0.75	2.6973	176.2499	2	226	39	0.90	7.9904	710.2492
	60	16	0.75	2.0502	180.0521	2	010	26	0.00	7 0067	717 0951
4	60	40	0.75	2.9502	180.9551	4	210	30	0.90	1.9907	717.9231
2	59	44	0.75	3.1199	181.6177	2	226	38	0.90	8.0110	720.4437
	FO	4.9	0.75	2 2079	195 9649	2	226	26	0.00	8 0461	744 9710
4	39	44	0.75	3.3918	185.8042	4	220	30	0.90	8.0401	744.2710
2	59	39	0.75	3.8068	193.6569	2	260	45	0.90	8.0644	763.7058
2	50	27	0.75	4 0727	200.0604	2	260	4.4	0.00	8 0866	770 0084
4	- 39	31	0.75	4.0121	200.0094	2	200	44	0.90	8.0800	110.9984
2	59	34	0.75	4.4570	212.3851	2	267	45	0.90	8.1034	784.2671
2	69	30	0.90	4 6591	213 2121	2	260	42	0.90	8 1 2 8 /	787 2516
2	05	- 55	0.50	4.0001	210.2121	2	200	-12	0.50	0.1204	101.2010
2	69	38	0.90	4.7726	216.3246	2	260	41	0.90	8.1477	796.3622
2	59	31	0.75	4 8148	229 8407	2	260	40	0.90	8 1658	806 2642
2	05	51	0.10	4.0140	223.0401	2	200	40	0.50	0.1000	000.2042
2	65	34	0.75	4.9003	233.9836	2	260	39	0.90	8.1825	817.1008
2	59	30	0.75	4 0253	237 3986	2	267	/11	0.90	8 1831	817 8027
2	05	50	0.10	4.5205	201.0000	2	201	-11	0.50	0.1001	017.0027
2	99	52	0.90	5.0858	270.7719	2	267	40	0.90	8.2003	827.9714
2	68	28	0.90	5 6910	280 1374	2	267	39	0.90	8 2160	839 0997
-	00	20	0.00	0.0010	200.1011	-	201	00	0.00	0.2100	000.0001
2	111	50	0.90	5.7112	313.2584	2	280	42	0.90	8.2272	847.8094
2	111	49	0.90	5.7835	315,4947	2	267	38	0.90	8.2303	851.1437
	111	40	0.00	5.1000	015 0000	Ĩ	201	41	0.00	0.0110	055 0000
2	111	48	0.90	5.8552	317.8999	2	280	41	0.90	8.2440	857.6208
2	111	47	0.90	5.9265	320.3998	2	286	42	0.90	8.2541	865.9768
			0.00	0.0200	020.0000		200	10	0.00	0.2041	000.0100
2	84	32	0.75	6.0170	322.7897	2	280	40	0.90	8.2596	868.2846
2	111	45	0.90	6.0670	326.0436	2	285	41	0.90	8.2660	872,9355
	110	10	0.00	0.00010	000.0000		200	4.1	0.00	0.2500	0.2.0000
2	112	45	0.90	6.0981	328.9809	2	286	41	0.90	8.2703	875.9984
2	111	44	0.90	6 1362	329 1570	2	280	39	0.90	8 2737	879 9547
	444	40	0.00	0.1002	000.0070		200	40	0.00	0.2101	000 5001
2	111	42	0.90	6.2722	336.0959	2	285	40	0.90	8.2810	883.7897
2	112	42	0.90	6.3012	339.1238	2	286	40	0.90	8.2852	886.8907
-	112	12	0.00	0.0012	000.1200	-	200	10	0.00	0.2002	000.0001
2	111	41	0.90	6.3388	339.9854	2	280	38	0.90	8.2864	892.5851
2	112	41	0.90	6.3670	343.0483	2	285	39	0.90	8.2945	895.6682
		10	0.00	0.0010	0110100	-		0.0	0.00	0.0000	000.0002
2	111	40	0.90	6.4042	344.2128	2	286	39	0.90	8.2986	898.8109
2	112	40	0.90	6.4316	347.3138	2	297	42	0.90	8.3007	899.2836
			0.00	0.1000	0.10.0000	-			0.00	0.000	000.5000
2	111	39	0.90	6.4683	348.8392	2	285	38	0.90	8.3067	908.5241
2	112	39	0.90	6.4950	351.9819	2	297	41	0.90	8.3156	909.6907
			0.00	0.5000	000.0000	-			0.00	0.0000	001.0010
2	111	38	0.90	0.5310	353.8462	2	297	40	0.90	8.3293	921.0018
2	112	38	0.90	6.5570	357.0340	2	297	39	0.90	8.3416	933.3806
	111	26	0.00	6 6510	265 E 400	2	911	49	0.00	0.9559	041 6740
2	111	30	0.90	0.0510	305.5490	2	311	42	0.90	8.3002	941.0740
2	112	36	0.90	6.6755	368.8423	2	309	41	0.90	8.3614	946.4459
2	111	24	0.00	6 7610	280.0412	2	200	4.4	0.00	9 2664	054 9510
4	111	34	0.90	0.7019	360.0412	2	322	44	0.90	8.3004	904.8019
2	112	34	0.90	6.7848	383.4650	2	309	39	0.90	8.3850	971.0929
2	133	42	0.90	6 8080	402 7095	2	300	42	0.90	8 39/6	974 9808
2	100	42	0.50	0.0000	402.1050	2	522	-12	0.50	0.0040	514.5606
2	133	41	0.90	6.8609	407.3699	2	322	41	0.90	8.4072	986.2640
2	130	39	0.90	6 9055	408 5504	2	322	40	0.90	8 4185	998 5273
	100	00	0.00	0.0000	100.0001	-	022	10	0.00	0.1100	00010210
2	133	40	0.90	6.9127	412.4352	2	322	39	0.90	8.4284	1011.9480
2	112	31	0.90	6 9232	413 5080	2	344	44	0.90	8 4414	1020 0902
2	112	51	0.50	0.5252	415.0000	2	044	44	0.50	0.4414	1020.0302
2	133	39	0.90	6.9631	417.9785	2	344	42	0.90	8.4661	1041.5944
2	133	38	0.90	7.0121	423.9779	2	346	42	0.90	8.4721	1047.6502
	100	00	0.00	R 1045	490,0002	Ĩ	0.1.4	4.1	0.00	0.4500	1059.0405
2	133	36	0.90	7.1045	438.0002	2	344	41	0.90	8.4768	1053.6485
2	148	41	0.90	7.1279	453.3139	2	346	41	0.90	8.4827	1059.7743
2	199	24	0.00	7 1976	455 2646	2	244	40	0.00	9 4962	1066 7406
-	100	34	0.90	7.1070	400.0040	4	344	40	0.50	3.4003	1000.7430
2	155	42	0.90	7.1917	469.3231	2	346	40	0.90	8.4920	1072.9516
2	155	40	0.90	7.2768	480.6575	2	366	45	0.90	8.4953	1075.0627
	100		0.00	T.2100	100.0010	- ⁴	050	40	0.00	0.1000	1000.0021
2	141	34	0.90	7.3094	482.7550	2	358	42	0.90	8.5069	1083.9849
2	155	39	0.90	7.3174	487.1178	2	366	44	0.90	8.5074	1085.3285
-	107	90	0.05	7 4000	E1E 0000	-	207	4.4	0.00	0 5100	1000.0000
2	101	39	0.95	7.4903	010.8923	2	307	44	0.90	8.5102	1088.2939
2	155	34	0.90	7.4924	530.6881	2	366	42	0.90	8.5289	1108.2080
0	155	20	0.00	7 5104	549 6909	0	270	15	0.00	9 5916	1112 0400
2	100	აპ	0.90	1.0194	042.0893	- 2	319	40	0.90	0.0310	1113.2480
2	218	52	0.90	7.5566	607.1496	2	380	45	0.90	8.5342	1116.1854
2	919	51	0.00	7 5808	611.0590	2	266	41	0.00	0 5290	1191 0220
4	210	01	0.90	1.0090	011.0300	4	300	*±1	0.90	0.0000	1121.0000
2	218	50	0.90	7.6224	615.2282	2	379	44	0.90	8.5428	1123.8784
9	218	40	0 00	7 6547	619 6202	2	380	41	0 00	8 5/15/	1126 8438
-	210	47	0.90	7.0347	019.0202	4	380	44	0.50	3.3434	1120.0400
2	218	48	0.90	7.6863	624.3439	2	366	40	0.90	8.5459	1134.9720
2	218	47	0.90	7 7176	629 2536	2	379	42	0.90	8 5626	1147 5706
-	210		0.50	7.1110	020.2000		010		0.50	5.0020	1141.0100
2	220	47	0.90	7.7344	635.0265	2	380	42	0.90	8.5651	1150.5985
2	218	45	0.90	7.7777	640.3379	2	379	41	0.90	8.5709	1160.8511
		45	0.00	5.5000	646.0102	Ĩ	200	41	0.00	0.5700	1100.0142
2	220	45	0.90	1.1938	040.2126	2	380	41	0.90	8.0733	1103.9140
2	218	44	0.90	7.8067	646.4525	2	379	40	0.90	8.5779	1175.2852
	010	49	0.00	7 8690	660 0800	-	280	40	0.00	0 5000	1170 2060
2	218	42	0.90	1.0020	000.0802	4	380	40	0.90	0.0803	11/0.3802
2	220	42	0.90	7.8770	666.1360	2	379	39	0.90	8.5835	1191.0816
0	910	41	0.00	7 9001	667 7101	0	260	20	0.00	Q EOFO	1104 9949
4	210	41	0.90	1.0001	007.7191	4	380	39	0.90	0.0000	1194.2243
2	220	41	0.90	7.9027	673.8450	2	379	38	0.90	8.5876	1208.1777
2	218	40	0.90	7 9130	676.0216	2	380	38	0.90	8 5898	1211 3655
4	210	4U	0.90	1.9130	070.0210	4	380	- 00	0.90	0.0090	1411.3033
2	220	40	0.90	7.9272	682.2236	2	380	36	0.90	8.5918	1251.4291

TABLE V: Pareto–Optimal Solutions for $\sigma = 0.1$ and q = 0.1

D	F	M	n	TH	Delay	D	F	М	n	TH	Delan
4	24	18	0.80	2 8935	172 7559	2	157	40	0.95	7 9155	635 5594
2	49	48	0.95	4.7014	181.5074	2	157	38	0.95	7.9282	655.2609
2	46	40	0.75	5.0460	202.5229	2	157	37	0.95	7.9309	666.6763
2	35	26	0.85	5.1285	227.9409	2	202	58	0.95	7.9743	702.9611
2	63	55	0.80	5.1828	235.9143	2	202	57	0.95	7.9906	706.5663
2	63	54	0.80	5.2502	237.3885	2	202	56	0.95	8.0065	710.4594
2	63	53	0.80	5.3172	238.9075	2	202	55	0.95	8.0221	714.5020
2	63	52	0.80	5.3836	240.5442	2	202	54	0.95	8.0372	718.7521
2	63	51	0.80	5.4496	242.2687	2	202	53	0.95	8.0518	723.2725
2	63	50	0.80	5.5149	244.0861	2	202	52	0.95	8.0659	728.0405
2	63	49	0.80	5.5796	246.0167	2	202	50	0.95	8.0926	738.3690
2	63	47	0.80	5.7070	250.2833	2	202	49	0.95	8.1050	744.0235
2	63	46	0.80	5.7695	252.5996	2	202	48	0.95	8.1167	750.0286
2	63	45	0.80	5.8311	255.1112	2	202	47	0.95	8.1275	756.5036
2	63	43	0.80	5.9512	260.6752	2	202	45	0.95	8.1464	770.8353
2	63	42	0.80	6.0095	263.8060	2	202	43	0.95	8.1612	787.3646
2	63	41	0.80	6.0662	267.2139	2	202	42	0.95	8.1000	796.6705
2	62	42	0.80	6.1752	272.2189	2	202	41 20	0.95	8.1703	842.0745
2	63	38	0.80	6 2260	279 2256	2	202	- 30 - 45	0.90	8 1021	893 2008
2	63	37	0.80	6.2763	284.0409	2	225	43	0.85	8.2015	912.4978
2	63	36	0.80	6.3232	289.3329	2	225	42	0.85	8.2036	923.4136
2	65	37	0.80	6.3566	293.0580	2	225	41	0.85	8.2044	935.1091
2	63	34	0.80	6.4073	301.8711	2	260	55	0.80	8.2212	976.1365
2	63	33	0.80	6.4434	309.3252	2	259	54	0.80	8.2265	978.2901
2	69	37	0.80	6.5032	311.0924	2	260	54	0.80	8.2302	982.0673
2	85	48	0.80	6.5424	334.7668	2	260	53	0.80	8.2387	988.3947
2	85	47	0.80	6.5855	337.7496	2	295	66	0.95	8.3150	991.8486
2	69	33	0.80	6.6401	339.2893	2	295	65	0.95	8.3261	995.4873
2	71	34	0.80	6.6719	340.7103	2	263	45	0.95	8.3833	1003.6123
2	87	44	0.85	6.7911	348.2774	2	295	59	0.95	8.3866	1021.5497
2	85	41	0.80	6.8211	361.1938	2	295	58	0.95	8.3957	1026.6016
2	85	38	0.80	6.9204	377.4029	2	295	57	0.95	8.4045	1031.8667
2	85	37	0.80	6.9493	383.8631	2	295	56	0.95	8.4127	1037.5520
2	109	54	0.95	6.9792 7.0145	387.8415	2	295	55	0.95	8.4206	1043.4558
2	109	52	0.95	7.0143	390.2807	2	295	53	0.95	8.4261	1049.0028
2	109	50	0.95	7 1174	398 4268	2	295	52	0.95	8 4416	1063 2274
2	100	49	0.95	7.1505	401.4780	2	295	50	0.95	8.4529	1078.3111
2	109							~ ~	0.00		
2		47	0.95	7.2145	408.2124	2	295	49	0.95	8.4577	1086.5690
	109	47 45	0.95	7.2145 7.2752	408.2124 415.9458	$\frac{2}{2}$	295 309	49 55	$0.95 \\ 0.95$	8.4577 8.4598	1086.5690 1092.9758
2	109 109	47 45 43	0.95 0.95 0.95	7.2145 7.2752 7.3318	408.2124 415.9458 424.8651	2 2 2	295 309 309	49 55 54	0.95 0.95 0.95	8.4577 8.4598 8.4666	1086.5690 1092.9758 1099.4773
2	109 109 109	47 45 43 42	0.95 0.95 0.95 0.95	7.2145 7.2752 7.3318 7.3582	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\end{array}$	2 2 2 2	295 309 309 309	49 55 54 53	0.95 0.95 0.95 0.95	8.4577 8.4598 8.4666 8.4728	$\begin{array}{r} 1086.5690 \\ 1092.9758 \\ 1099.4773 \\ 1106.3920 \end{array}$
$\begin{array}{c} 2\\ 2\\ 2\\ \end{array}$	109 109 109 109	47 45 43 42 41	0.95 0.95 0.95 0.95 0.95	7.2145 7.2752 7.3318 7.3582 7.3832	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574 \end{array}$	2 2 2 2 2	295 309 309 309 309	49 55 54 53 52	0.95 0.95 0.95 0.95 0.95	$\begin{array}{r} 8.4577 \\ 8.4598 \\ 8.4666 \\ 8.4728 \\ 8.4785 \end{array}$	$\begin{array}{r} 1086.5690 \\ 1092.9758 \\ 1099.4773 \\ 1106.3920 \\ 1113.6856 \end{array}$
$\begin{array}{c} 2\\ 2\\ 2\\ 2\\ 2\\ 2\end{array}$	109 109 109 109 110	$ \begin{array}{r} 47 \\ 45 \\ 43 \\ 42 \\ 41 \\ 41 \\ 41 \end{array} $	$\begin{array}{c} 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \end{array}$	7.2145 7.2752 7.3318 7.3582 7.3832 7.3987	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\end{array}$	2 2 2 2 2 2 2	295 309 309 309 309 309	49 55 54 53 52 50	$\begin{array}{c} 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \end{array}$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4884\end{array}$	$\begin{array}{c} 1086.5690 \\ 1092.9758 \\ 1099.4773 \\ 1106.3920 \\ 1113.6856 \\ 1129.4852 \end{array}$
$\begin{array}{c} 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ $	109 109 109 109 110 109	47 45 43 42 41 41 38	0.95 0.95 0.95 0.95 0.95 0.95 0.95	7.2145 7.2752 7.3318 7.3582 7.3832 7.3987 7.4475	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 452.9565\\ 455.9565\\ 455.9565\\ 455.9565\\ 455.9565\\ 455.9565\\ 455.9565\\ 455.956\\ $	2 2 2 2 2 2 2 2 2	295 309 309 309 309 309 309		0.95 0.95 0.95 0.95 0.95 0.95 0.95	8.4577 8.4598 8.4666 8.4728 8.4785 8.4884 8.4924	$\begin{array}{r} 1086.5690 \\ 1092.9758 \\ 1099.4773 \\ 1106.3920 \\ 1113.6856 \\ 1129.4852 \\ 1138.1350 \\ 1128.0251 \end{array}$
	109 109 109 109 110 109	$ \begin{array}{r} 47 \\ 45 \\ 43 \\ 42 \\ 41 \\ 41 \\ 38 \\ 37 \\ 57 \\ 57 \\ 57 \\ 57 \\ 57 \\ 57 \\ 57 \\ 5$	0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95	7.2145 7.2752 7.3318 7.3582 7.3832 7.3987 7.4475 7.4475	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ \end{array}$	2 2 2 2 2 2 2 2 2 2 2 2	295 309 309 309 309 309 309 309	$ \begin{array}{r} 49 \\ 55 \\ 54 \\ 53 \\ 52 \\ 50 \\ 49 \\ 47 \\ \end{array} $	0.95 0.95 0.95 0.95 0.95 0.95 0.95	8.4577 8.4598 8.4666 8.4728 8.4785 8.4884 8.4924 8.4980	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1157.2259\end{array}$
	109 109 109 109 109 110 109 109 109 141 141	$ \begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ \end{array} $	0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95	$\begin{array}{r} 7.2145 \\ 7.2752 \\ 7.3318 \\ 7.3582 \\ 7.3832 \\ 7.3987 \\ 7.4475 \\ 7.4644 \\ 7.4644 \\ 7.4507 \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7022\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	295 309 309 309 309 309 309 309 309 309	$ \begin{array}{r} 49 \\ 55 \\ 54 \\ 53 \\ 52 \\ 50 \\ 49 \\ 47 \\ 45 \\ 52 \\ \end{array} $	$\begin{array}{c} 0.95 \\ 0.$	8.4577 8.4598 8.4666 8.4728 8.4785 8.4884 8.4924 8.4980 8.5000 8.5000	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1201.0252\end{array}$
	109 109 109 109 109 110 109 109 141 141	$ \begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 52\\ \end{array} $	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145 \\ 7.2752 \\ 7.3318 \\ 7.3582 \\ 7.3832 \\ 7.3987 \\ 7.4475 \\ 7.4644 \\ 7.4751 \\ 7.5007 \\ 7.5259 \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8587\end{array}$	$ \begin{array}{c} 2 \\ $	295 309 309 309 309 309 309 309 309 309 360	$ \begin{array}{r} 49 \\ 55 \\ 54 \\ 53 \\ 52 \\ 50 \\ 49 \\ 47 \\ 45 \\ 58 \\ 58 \\ 58 \\ \end{array} $	$\begin{array}{c} 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.85 \\ 0.$	8.4577 8.4598 8.4666 8.4728 8.4785 8.4884 8.4924 8.4924 8.4980 8.5000 8.5009 8.5079	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1204.6221\\ \end{array}$
	$ \begin{array}{r} 109 \\ 109 \\ 109 \\ 109 \\ 110 \\ 109 \\ 109 \\ 141 $	$ \begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ \end{array} $	$\begin{array}{c} 0.95 \\ 0.$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4475\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.505\end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\end{array}$	$ \begin{array}{c} 2 \\ $	295 309 309 309 309 309 309 309 309 360 361 360	$ \begin{array}{r} 49 \\ 55 \\ 54 \\ 53 \\ 52 \\ 50 \\ 49 \\ 47 \\ 45 \\ 58 \\ 57 \\ \end{array} $	$\begin{array}{c} 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.85 \\ 0.$	8.4577 8.4598 8.4666 8.4728 8.4785 8.4884 8.4924 8.4924 8.4980 8.5000 8.5079 8.5100 8.5100	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1307.9220\end{array}$
	109 109 109 109 109 109 109 141 141 141 141	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ \end{array}$	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4475\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.5505\\ 7.5981 \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	295 309 309 309 309 309 309 309 309 360 361 360 361	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 57\end{array}$	$\begin{array}{c} 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.85 \\ 0.$	8.4577 8.4598 8.4666 8.4728 8.4785 8.4884 8.4924 8.4924 8.5000 8.5079 8.5132 8.5152	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1304.6221\\ 1307.9339\\ 1311.5670\end{array}$
$ \begin{array}{c} 2 \\ 2 \\ $	$109 \\ 109 \\ 109 \\ 109 \\ 109 \\ 109 \\ 109 \\ 141 $	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ \end{array}$	$\begin{array}{c} 0.95 \\ 0.$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4475\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.5505\\ 7.5981\\ 7.6210\\ \end{array}$	$\begin{array}{c} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 57\\ 56\\ \end{array}$	$\begin{array}{c} 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.85 \\ 0.85 \\ 0.85 \\ 0.85 \\ 0.85 \\ 0.85 \\ \end{array}$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.484\\ 8.4924\\ 8.4980\\ 8.5000\\ 8.5079\\ 8.5079\\ 8.5132\\ 8.5132\\ 8.5152\\ 8.5152\end{array}$	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\end{array}$
	$109 \\ 109 \\ 109 \\ 109 \\ 109 \\ 109 \\ 109 \\ 141 $	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ \end{array}$	$\begin{array}{c} 0.95 \\ 0.$	$\begin{array}{r} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3832\\ 7.4475\\ 7.4475\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.5981\\ 7.6210\\ 7.6432\\ \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 523.5348\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 57\\ 56\\ 56\\ 56\end{array}$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ \end{array}$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4980\\ 8.5000\\ 8.5079\\ 8.5100\\ 8.5132\\ 8.5132\\ 8.5152\\ 8.5180\\ 8.5200\end{array}$	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996 \end{array}$
$ \begin{array}{c} 2 \\ 2 \\ $	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ \end{array}$	$\begin{array}{c} 0.95\\$	$\begin{array}{r} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4475\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.5505\\ 7.5981\\ 7.6210\\ 7.6432\\ 7.6646\end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 412.8451\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 452.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 516.3962\\ 519.3432\\ 523.5348\\ 528.0545\\ \end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 57\\ 57\\ 56\\ 56\\ 56\\ 55\\ \end{array}$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ \end{array}$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4884\\ 8.4924\\ 8.4980\\ 8.5000\\ 8.5079\\ 8.5100\\ 8.5132\\ 8.5132\\ 8.5132\\ 8.5152\\ 8.5180\\ 8.5200\\ 8.5225\end{array}$	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\end{array}$
$ \begin{array}{c} 2 \\ 2 \\ $	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 110\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ \end{array}$	$\begin{array}{c} 0.95\\$	$\begin{array}{r} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.5505\\ 7.5981\\ 7.6210\\ 7.6432\\ 7.6646\\ 7.6851\\ \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 523.5348\\ 528.0545\\ 532.8790\\ \end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 57\\ 57\\ 56\\ 56\\ 55\\ 55\\ 55\\ 55\\ \end{array}$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4980\\ 8.5000\\ 8.5000\\ 8.5079\\ 8.5100\\ 8.5132\\ 8.5132\\ 8.5152\\ 8.5180\\ 8.5225\\ 8.5225\\ 8.5224\end{array}$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1326.5533\end{array}$
$ \begin{array}{c} \frac{1}{2} \\ \frac{2}{2} \\ $	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 110\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ \end{array}$	$\begin{array}{c} 0.95\\ \end{array}$	$\begin{array}{r} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4475\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.5505\\ 7.5981\\ 7.6210\\ 7.6432\\ 7.6646\\ 7.66851\\ 7.7047\\ \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 528.0545\\ 522.5348\\ 528.0545\\ 538.0583\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 57\\ 56\\ 56\\ 56\\ 55\\ 55\\ 54\\ \end{array}$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.484\\ 8.4924\\ 8.4980\\ 8.5000\\ 8.5079\\ 8.5100\\ 8.5100\\ 8.5152\\ 8.5152\\ 8.5152\\ 8.5180\\ 8.5220\\ 8.5225\\ 8.5244\\ 8.5264\end{array}$	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1322.8786\\ 1322.8786\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ \end{array}$
	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 110\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 43\\ \end{array}$	$\begin{array}{c} 0.95\\$	$\begin{array}{r} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4475\\ 7.4644\\ 7.4751\\ 7.5007\\ 7.5258\\ 7.5505\\ 7.5981\\ 7.6210\\ 7.6432\\ 7.6646\\ 7.6851\\ 7.7047\\ 7.7047\\ 7.7406\\ \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 412.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 452.8517\\ 498.7365\\ 501.7032\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 523.6348\\ 528.0545\\ 532.8790\\ 538.0583\\ 549.5961\\ \end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 56\\ 56\\ 56\\ 55\\ 55\\ 55\\ 54\\ 54\\ 54\\ \end{array}$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\$	$\begin{array}{c} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.5900\\ 8.5000\\ 8.5079\\ 8.5132\\ 8.5132\\ 8.5132\\ 8.5132\\ 8.5132\\ 8.51200\\ 8.5225\\ 8.5244\\ 8.5224\end{array}$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ \end{array}$
	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 110\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 43\\ 42\\ \end{array}$	$\begin{array}{c} 0.95\\$	7.2145 7.2752 7.3318 7.33582 7.3582 7.3887 7.4644 7.4751 7.4751 7.4751 7.5258 7.5505 7.5981 7.6210 7.6432 7.66451 7.7047 7.7047	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 523.5348\\ 528.0545\\ 532.8790\\ 538.0583\\ 549.5961\\ 556.0918\\ \end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 56\\ 55\\ 56\\ 55\\ 55\\ 54\\ 54\\ 53\\ \end{array}$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4884\\ 8.4984\\ 8.4980\\ 8.5000\\ 8.5000\\ 8.5000\\ 8.5120\\ 8.5180\\ 8.5180\\ 8.5225\\ 8.5225\\ 8.5224\\ 8.5244\\ 8.5224\\ 8.5244\\$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1157.2259\\ 1157.2259\\ 11304.6221\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ 1339.5062\end{array}$
$ \begin{array}{r} \overline{2} \\ \overline{2} \\ $	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 110\\ 109\\ 109\\$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 43\\ 42\\ 41\\ \end{array}$	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3382\\ 7.3987\\ 7.4475\\ 7.4475\\ 7.4475\\ 7.505\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.6501\\ 7.6642\\ 7.6646\\ 7.6681\\ 7.7647\\ 7.7406\\ 7.7647\\ 7.7713\\ \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 528.0545\\ 522.5348\\ 528.0545\\ 532.8790\\ 538.0583\\ 549.5961\\ 556.0918\\ 556.0918\\ 556.1687\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 57\\ 56\\ 55\\ 55\\ 55\\ 55\\ 55\\ 54\\ 53\\ 53\\ 53\\ \end{array}$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.5152\\ 8.5150\\ 8.5100\\ 8.5100\\ 8.5100\\ 8.5112\\ 8.5180\\ 8.5205\\ 8.5218\\ 8.5225\\ 8.5224\\ 8.5223\\ 8.5224\\ 8.5223\\ 8.5203\\ 8.5300\\ 8.5318\\ 8.5300\\ 8.5318\\ 8.5310\\ 8.5318\\ 8.5310\\ 8.5318\\ 8.5310\\ 8.5318\\ 8.5318\\ 8.5320\\ 8.5318\\$	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.622\\ 1304.622\\ 1304.622\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1326.5533\\ 1326.5533\\ 1326.5533\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ 1339.5062\\ 1343.2270\\ \end{array}$
	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 43\\ 42\\ 41\\ 40\\ \end{array}$	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3882\\ 7.3987\\ 7.4475\\ 7.4751\\ 7.5088\\ 7.5056\\ 7.5505\\ 7.5505\\ 7.5051\\ 7.6210\\ 7.6240\\ 7.6851\\ 7.6047\\ 7.7047\\ 7.7047\\ 7.77667\\ 7.77667\\ 7.77667\\ 7.77667\\ 7.7844\\ \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 452.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 516.3962\\ 519.3432\\ 523.5348\\ 528.0545\\ 532.8790\\ 538.0583\\ 549.5961\\ 556.0918\\ 563.1687\\ 570.7890\\ \end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 56\\ 55\\ 56\\ 55\\ 55\\ 54\\ 53\\ 53\\ 52\\ \end{array}$	0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.85	$\begin{array}{c} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.5475\\ 8.5100\\ 8.5000\\ 8.5000\\ 8.5000\\ 8.5100\\ 8.5132\\ 8.5132\\ 8.5132\\ 8.51200\\ 8.5226\\ 8.5224\\ 8.5224\\ 8.5224\\ 8.5224\\ 8.5224\\ 8.5231\\ 8.5329\\ \end{array}$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ 1339.5062\\ 1334.2270\\ 1348.5740\\ \end{array}$
- 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 110\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 43\\ 42\\ 41\\ 40\\ 48\\ 56\\ 43\\ 42\\ 41\\ 40\\ 48\\ 56\\ 43\\ 42\\ 41\\ 40\\ 48\\ 56\\ 56\\ 48\\ 56\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48\\ 48$	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3887\\ 7.3887\\ 7.4475\\ 7.4751\\ 7.5007\\ 7.4644\\ 7.4751\\ 7.5088\\ 7.5505\\ 7.5981\\ 7.6210\\ 7.6825\\ 7.6845\\ 7.7047\\ 7.7047\\ 7.7047\\ 7.7047\\ 7.77047\\ 7.77047\\ 7.77047\\ 7.7713\\ 7.7764\\ 7.8030\\ \end{array}$	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 4435.3574\\ 439.3515\\ 454.9263\\ 452.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 523.5348\\ 528.0545\\ 552.8790\\ 538.0583\\ 549.5961\\ 556.0918\\ 556.0918\\ 556.0918\\ 556.0918\\ 5570.7890\\ 582.9430\\ \end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 57\\ 56\\ 55\\ 55\\ 56\\ 55\\ 55\\ 54\\ 53\\ 53\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52$	$\begin{array}{c} 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.85\\$	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.5799\\ 8.5000\\ 8.5000\\ 8.5012\\ 8.5180\\ 8.5180\\ 8.5225\\ 8.5244\\ 8.5225\\ 8.5244\\ 8.5224\\ 8.5329\\ 8.5318\\ 8.5329\\ 8.5318\\ 8.5329\\ 8.5347\\ \end{array}$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1157.2259\\ 1157.2259\\ 1157.1490\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5470\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1322.8786\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ 1339.5062\\ 1334.5740\\ 1352.3200\\ \end{array}$
$ \begin{array}{c} 2 \\ 2 \\ $	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 43\\ 42\\ 41\\ 40\\ 48\\ 47\\ 52\\ 52\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 48\\ 47\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52\\ 52$	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3383\\ 7.3832\\ 7.3987\\ 7.4474\\ 7.4751\\ 7.5258\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.6210\\ 7.6240\\ 7.6642\\ 7.6642\\ 7.6642\\ 7.6642\\ 7.6642\\ 7.6642\\ 7.7647\\ 7.7406\\ 7.7642\\ 7.7713\\ 7.7406\\ 7.7713\\ 7.7743\\ 7.7743\\ 7.7844\\ 7.7713\\ 7.7844\\ 7.7844\\ 7.7844\\ 7.7844\\ 7.7844\\ 7.7844\\ 7.7844\\ 7.8208\\$	$\begin{array}{r} 408.2124\\ 415.9458\\ 412.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 442.8517\\ 458.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 528.0545\\ 528.0545\\ 528.0545\\ 558.0583\\ 549.5961\\ 556.0918\\ 556.0918\\ 556.0918\\ 556.31687\\ 570.7890\\ 587.9756\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 57\\ 57\\ 56\\ 55\\ 55\\ 54\\ 53\\ 52\\ 52\\ 52\\ 50\\ 82\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50$	0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.85	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.5152\\ 8.5150\\ 8.5150\\ 8.5152\\ 8.5153\\ 8.5153\\ 8.5255\\ 8.5225\\ 8.5224\\ 8.5223\\ 8.5224\\ 8.5223\\ 8.5324\\ 8.5329\\ 8.5334\\ 8.5337\\ 8.5337\\ 8.5372\\$	$\begin{array}{c} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ 1339.5062\\ 1334.2270\\ 1343.2270\\ 1348.5740\\ 1352.3200\\ 1367.9894\\ \end{array}$
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 38\\ 37\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 43\\ 42\\ 41\\ 40\\ 48\\ 47\\ 45\\ 42\\ 41\\ 40\\ 8\\ 47\\ 45\\ 42\\ 41\\ 40\\ 8\\ 47\\ 45\\ 42\\ 41\\ 40\\ 48\\ 47\\ 45\\ 42\\ 41\\ 48\\ 47\\ 45\\ 42\\ 42\\ 41\\ 48\\ 47\\ 45\\ 42\\ 45\\ 42\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45$	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3832\\ 7.3987\\ 7.4475\\ 7.4475\\ 7.4751\\ 7.5028\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.6210\\ 7.6240\\ 7.6851\\ 7.6432\\ 7.6432\\ 7.6645\\ 7.66432\\ 7.7046\\ 7.75667\\ 7.7046\\ 7.7567\\ 7.7746\\ 7.7746\\ 7.7746\\ 7.7567\\ 7.7444\\ 7.8030\\ 7.8208\\ 7.8538\\ 7.8588\\ 7.8588\\ 7.8588\\ 7.8588\\ 7.8588\\ 7.8588\\ 7.8588\\ 7.858$	$\begin{array}{r} 408.2124\\ 415.9458\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 455.5\\ 501.7032\\ 504.8585\\ 508.1867\\ 516.3962\\ 519.3432\\ 528.0545\\ 532.8790\\ 538.0583\\ 549.5961\\ 5563.1687\\ 550.7890\\ 587.9756\\ 587.9756\\ 599.1146\\ 5$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 45\\ 58\\ 58\\ 57\\ 56\\ 56\\ 55\\ 55\\ 54\\ 53\\ 53\\ 52\\ 52\\ 52\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50\\ 50$	0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.85	$\begin{array}{c} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4788\\ 8.4785\\ 8.4884\\ 8.4980\\ 8.5000\\ 8.50079\\ 8.5100\\ 8.5100\\ 8.5132\\ 8.5132\\ 8.5132\\ 8.5132\\ 8.5180\\ 8.5225\\ 8.5224\\ 8.5224\\ 8.5224\\ 8.5224\\ 8.5328\\ 8.5329\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5330\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.5330\\ 8.5337\\ 8.5330\\ 8.530\\ 8.$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ 1339.5062\\ 1334.5740\\ 1352.3200\\ 1348.5740\\ 1352.3200\\ 1367.9894\\ 1371.7893\\ 1367.9894\\ 1371.7893\\ 1367.7894\\ 1371.7894\\ 1371.789\\ 1367.7894\\ 1371.789\\ 1367.789\\$
	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 141\\ 14$	$\begin{array}{r} 47\\ 45\\ 43\\ 42\\ 41\\ 38\\ 37\\ 55\\ 54\\ 55\\ 52\\ 50\\ 49\\ 47\\ 46\\ 45\\ 43\\ 42\\ 41\\ 40\\ 48\\ 47\\ 45\\ 43\\ 42\\ 41\\ 40\\ 48\\ 47\\ 45\\ 43\\ 42\\ 41\\ 40\\ 48\\ 47\\ 45\\ 43\\ 42\\ 45\\ 43\\ 45\\ 43\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45\\ 45$	$\begin{array}{c} 0.95\\$	7.2145 7.2752 7.3318 7.3382 7.3882 7.3887 7.4475 7.4644 7.4751 7.5088 7.5505 7.55081 7.6432 7.66451 7.6432 7.6651 7.7047 7.77047 7.77047 7.77047 7.77047 7.75667 7.7713 7.75667 7.7713 7.75881 7.75667 7.7713 7.75667 7.7713 7.7584 7.75667 7.7713 7.7584 7.75867 7.7584 7.7567 7.7713 7.7584 7.7587 7.7587 7.7587 7.7587 7.7587 7.7587 7.7587 7.7587 7.7587 7.7587 7.7587 7.75977 7.75977 7.75977 7.75977 7.7597777777777	$\begin{array}{r} 408.2124\\ 415.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 4435.3574\\ 439.3515\\ 454.9263\\ 452.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 504.8585\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3422\\ 523.5348\\ 528.0545\\ 532.8790\\ 538.0583\\ 549.5961\\ 556.0918\\ 556.0918\\ 556.0918\\ 556.0918\\ 556.0918\\ 556.0918\\ 556.0918\\ 558.9430\\ 570.7890\\ 582.9430\\ 587.9756\\ 599.1146\\ 611.9616\\ 611.9616\\ 610.957\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 49\\ 47\\ 45\\ 58\\ 57\\ 56\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55$	0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.85	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4666\\ 8.4728\\ 8.4788\\ 8.4980\\ 8.5000\\ 8.5079\\ 8.5000\\ 8.5120\\ 8.5120\\ 8.5120\\ 8.5120\\ 8.5120\\ 8.5244\\ 8.5225\\ 8.5224\\ 8.5225\\ 8.5300\\ 8.5244\\ 8.5224\\ 8.5320\\ 8.5318\\ 8.5329\\ 8.5328\\ 8.5347\\ 8.5372\\ 8.5392\\ 8.5340\\ 8.5340\\$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1157.2259\\ 1157.2259\\ 1157.2259\\ 1157.1490\\ 1301.0082\\ 1304.6221\\ 1307.9339\\ 1311.5470\\ 1315.2462\\ 1318.8966\\ 1322.8786\\ 1322.8786\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.792\\ 1334.5740\\ 1352.3200\\ 1352.$
	$\begin{array}{c} 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\ 109\\$	$\begin{array}{c} 47\\ 45\\ 43\\ 42\\ 41\\ 38\\ 37\\ 55\\ 54\\ 55\\ 55\\ 50\\ 49\\ 48\\ 47\\ 46\\ 45\\ 42\\ 41\\ 40\\ 48\\ 47\\ 45\\ 43\\ 42\\ 43\\ 42\\ 43\\ 42\\ 41\\ 43\\ 42\\ 43\\ 42\\ 41\\ 43\\ 42\\ 43\\ 42\\ 43\\ 42\\ 43\\ 42\\ 43\\ 42\\ 43\\ 42\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 44\\ 43\\ 44\\ 43\\ 44\\ 44\\ 45\\ 44\\ 44\\ 45\\ 44\\ 44\\ 44\\ 45\\ 44\\ 44$	$\begin{array}{c} 0.95\\$	$\begin{array}{c} 7.2145\\ 7.2752\\ 7.3318\\ 7.3582\\ 7.3382\\ 7.3987\\ 7.4454\\ 7.4751\\ 7.5258\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.5505\\ 7.5581\\ 7.6210\\ 7.6240\\ 7.68811\\ 7.6240\\ 7.68811\\ 7.7047\\ 7.7406\\ 7.7643\\ 7.7713\\ 7.7743\\ 7.7743\\ 7.7713\\ 7.7844\\ 7.8208\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8528\\ 7.8526\\ 7.856$	$\begin{array}{r} 408.2124\\ 415.9458\\ 412.9458\\ 424.8651\\ 429.8866\\ 435.3574\\ 439.3515\\ 454.9263\\ 462.8517\\ 498.7365\\ 501.7032\\ 504.8585\\ 508.1867\\ 515.3962\\ 519.3432\\ 528.0545\\ 522.35348\\ 528.0545\\ 532.8790\\ 553.0583\\ 549.5961\\ 556.0918\\ 5563.1687\\ 570.7890\\ 587.9756\\ 599.1146\\ 611.9616\\ 619.1944\\ 627.0744\end{array}$	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 295\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309\\ 309$	$\begin{array}{r} 49\\ 55\\ 54\\ 53\\ 52\\ 50\\ 49\\ 47\\ 58\\ 58\\ 58\\ 58\\ 57\\ 56\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55$	0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.85	$\begin{array}{r} 8.4577\\ 8.4598\\ 8.4666\\ 8.4728\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4785\\ 8.4980\\ 8.5079\\ 8.5152\\ 8.5152\\ 8.5152\\ 8.5152\\ 8.5122\\ 8.5264\\ 8.5225\\ 8.5244\\ 8.5225\\ 8.5244\\ 8.5223\\ 8.5316\\ 8.5329\\ 8.5317\\ 8.5347\\ 8.5347\\ 8.5372\\ 8.5390\\ 8.5401\\ 8.5347\\ 8.5390\\ 8.5411\\ 8.5338\\ 8.5347\\ 8.5393\\ 8.5412\\ 8.5412\\ 8.5412\\ 8.5412\\ 8.5412\\ 8.5412\\ 8.5422\\$	$\begin{array}{r} 1086.5690\\ 1092.9758\\ 1099.4773\\ 1106.3920\\ 1113.6856\\ 1129.4852\\ 1138.1350\\ 1157.2259\\ 1179.1490\\ 1301.0082\\ 1304.6221\\ 1304.6221\\ 1307.9339\\ 1311.5670\\ 1315.2462\\ 1318.8996\\ 1322.8786\\ 1326.5533\\ 1331.0818\\ 1334.7792\\ 1339.5062\\ 1334.2770\\ 1343.2270\\ 1343.2270\\ 1343.2270\\ 1343.24704\\ 1352.3200\\ 1367.9894\\ 1371.7893\\ 1382.4794\\ 1546.3247\\ \end{array}$

TABLE VI: Pareto–Optimal Solutions for $\sigma = 0.1$ and q = 0.5

MTHDelaiMDela p 1.00 21 1.00 4.2673 162.3399 2 175 55 1053.2001 24 8.0653 0.80 0.80 $4.3202 \\ 4.3356$ 282.2721284.05202 190 58 199 76 8.0905 8.0915 4948 46 1.001133.455649 1.00 1148.9174 4 49 44 0.80 4.3505286.3995 2 199 74 1.00 8.09491151.8905 4 40 22 0.80 4.3782286.7716 2 199 73 1.00 8.0965 1153.41221.00 8.100 51 35 1.00 4.4633 292.49942 199 68 1.00 8.1025 1162.19354 8.1041 315.4406 1994.487 66 1.001166.2122 1.00 315.5049 2 4640 0.757.3458211 78 1.00 8.1064 1215.3322 43 43 7.49897.5260318.8284 331.5815 1.00 8.1098 8.1127 1.00 1.00 2 2 1218.1989 1221.3512 $\frac{50}{52}$ 2 7241 1.00 7.7049466.50472 211 73 1.008.1140 1222.96472 82 590.90 7.7184 495.9218 2 21170 1.00 8.1173 1228.3070 580.907.7233497.25012 211 68 1.008.1188 1232.275582 82 57 0.90 7.7279 498.6781 2 211 66 1.00 8.1199 1236.5365 2 82 56 0.90 7.7322500.13562 211 64 1.00 8.1201 1241.3024 2 82 51 0.90 7.7479509.0388 2 213 68 1.00 8.1214 1243.95581407.0085 507.7496511.1888 24895 1.00 8.124682 0.90 82 49 0.90 7.7507 513.46912 24883 1.00 8.1463 1420.8232 48 66 7.7512 7.7604 515.9489 521.5716 248 78 248 76 8.1529 1428.4473 8.1550 1431.8167 82 89 2 1.00 1.00 2 64 62 1.007.7719 7.7827 523.5819 525.7972 2
 248
 74

 248
 73
 1.00 8.1566 1435.5218 8.1574 1437.4182 89 89 1.00 2 2 89 581.00 7.8014530.9339 2 24870 1.008.15891443.69742 89 51 1.00 7.8215 543.3548 2 248 68 1.00 8.1592 1448.3617 $254 \\ 254$ 89 99 49 1.007.8229548.10312 76 1.008.1610 8.1626 1466.4574 $\mathbf{2}$ 64 1.00 7.8327 582.4113 2 74 1.00 1470.2522 2 2 100 64 1.00 7.8382588.29432 25473 1.00 8.1632 1472.1945 2 100 62 1.00 7.8468 590.78342 254 70 1.00 8.1645 1478.6255 $\frac{58}{51}$ 1.00 7.8612596.5549 610.5110 2 261 261 78 77 1.008.1660 8.1670 1503.32561002 100 1.00 7.8738 2 1.00 1505.0477 106 60 7.8829 629.1163 2 261 261 76 1.00 8.1678 1506.8716 109 51 1.00 7.9088665.4576 74 1.00 8.1691 1510.7709 70 704 3835 26 1.00 8.1697 1512.7668 8.1702 1514.8259 7 9101 2 73 121 1.00 7.9178 706.6594 261 72 68 2 12166 65 $1.00 \\ 1.00$ 7.9248709.1030 261 287 70 1.008.1707 8.1907 1519.37512 2 121 7.9281 710.5023 74 1.00 1661.2692 121 64 1.00 7.9312711.8361 2 29478 1.00 8.1943 1693.40122 121 62 1.00 7.9368 714.8479 2 294 76 1.00 8.1953 1697.3956 121 591.00 7.9435 719.9596 2 294 74 1.00 8.1959 1701.7880 2 2 121 58 1.00 7.9452 721.8323 2 294 73 1.00 8.1961 1704.036112156 1.00 7.9477725.99442 297 1.00 8.1971 1712.6405121 54 1.00 7.9489730.5792 2 303 78 1.00 8.2009 1745.24001749.3567 808.2825 14076 1.00 7.9561 2 303 76 1.00 8.2018 2 2 140 74 1.007.9632 810.3741 303 74 1.008.2022 1753.88357.9666 303 73 306 78 $140 \\ 140$ 73 70 1.00 811.4447 814.9894 2 2 1.00 8.2023 1756.2005 8.2030 1762.5196 2 $140 \\ 140$ 1.00 7.9817 7.9869 817.6235820.4508306 306 76 74 $1.00 \\ 1.00$ 8.20388.20421766.6770 1771.2487 68 66 2 65 64 $1.00 \\ 1.00$ 7.98917.9913822.0698 823.6130 306 309 1.00 8.2043 8.2051 2 140 $\frac{2}{2}$ 73 1773.5886140 78 1779.799 140 62 1.00 7.9950 827.0978 $\overline{2}$ 309 76 1.00 8.2058 1783.9974140 59 1.00 7.9988 833.0111 2 309 74 1.00 8.2062 1788 6139 2 14058 56 1.007.9995835.1778 839.9935 2 309 73 82 1.008.2062 8.2064 1790.97672 140 1.00 8.0001 2 314 1.001800.7522 68 1.008.0164893.5457 3141.008.2085 1808.5986 76 155 70 1.00 8.0167 902.3109 2 314 1.00 8.20911812.8647905.2261 908.3562 8.0212 314 1.00 1819.9570 155 314 74 8.02511.00 8.2094 1817.5559 66 1.00 2 2 $155 \\ 155$ 64 59 1.00 $\begin{array}{c} 8.0284\\ 8.0328\end{array}$ 911.8572 922.2623 2 332 332 83 82 $1.00 \\ 1.00$ $\frac{8.2177}{8.2183}$ 1902.0698 1903.9800 15558 1.00 8.0330 924.6612 2 332 78 1.00 8.2198 1912.2762 166 73 1.00 8.0352 962.1428 2 332 76 1.00 8.2202 1916.7868 708.2204 166 1.00 8.0418 966.3458 $\mathbf{2}$ 333 78 1.00 1918.0361 16668 1.00 8.0456969.46792 333 76 1.00 8.2208 1922.560316666 1.008.0488972.8202 2 343 355 701.008.22451996.7266 2 166 64 1.00 8.0513 976.5697 2 82 1.00 8.2318 2035.8822 8.2337 2053.8106 8.2350 2070.2915 357 361 79 166591.008.0539987.7132 2 2 1.00 66 8.05851002.1220 82 171 1.00 171 64 1.00 8.0607 1005.9844 2 390 78 1.00 8.2492 2246.3486 171 1.00 8.0622 58 1020.1101

TABLE VII: Pareto–Optimal Solutions for $\sigma = 0.1$ and q = 0.9

D	F	M	p	TH	Delay	D	F	M	p	TH	Delay
4	45	40	1.00	2.3723	338.7587	2	261	62	1.00	12.0755	2180.6202
2	79	78	1.00	2.3846	369.4111	2	261	61	1.00	12.0815	2193.8380
4	49	43	0.65	2.4049	399.2489	2	261	60	1.00	12.0822	2208.5330
2	92	87	0.95	3.2832	405.2141	2	284	73	0.95	12.0953	2284.3395
2	64	57	0.90	3.5741	412.0022	2	284	72	0.95	12.1290	2289.1439
2	81	70	1.00	4.5445	414.1696	2	284	71	0.95	12.1611	2294,4007
2	93	79	0.95	5.0265	437.3718	2	284	70	0.95	12,1915	2300.1592
2	92	77	0.95	5.2183	440.6751	2	284	68	0.95	12.2460	2313.3933
2	103	87	0.95	5.2786	455.1786	2	284	64	0.95	12.3243	2348.7182
2	103	85	0.95	5.6153	463.1780	2	284	63	0.95	12.3357	2359.9178
2	103	84	0.95	5.7852	466.5696	2	295	68	0.95	12.3715	2402.9965
2	103	83	0.95	5 9531	470.0984	2	293	64	0.95	12 4206	2423 1494
2	109	87	0.95	6 1609	487 9397	2	295	64	0.95	12.4412	2439 6897
2	103	79	0.95	6.5769	489.3956	2	295	63	0.95	12.4504	2451 3231
2	103	78	0.95	6 7329	493.6560	2	205	62	0.05	12.1001	2464 1731
2	100	83	0.95	6 7896	501 7065	2	213	72	0.95	12.4000	2522 8945
2	103	77	0.95	6 7996	510 5624	2	312	70	1.00	12.4012	2524 5831
2	103	76	0.95	6.9505	514 9480	2	311	68	0.95	12.5107	2533 3285
2	118	89	0.95	7.0692	521 5902	2	313	68	0.95	12.5577	2549 6200
2	92	64	0.95	7 1915	527 3516	2	315	68	0.95	12.5571	2565 9115
2	103	73	0.95	7 3851	529 4723	2	312	64	1.00	12.6076	2579 6491
2	103	72	0.95	7 5235	534 8245	2	313	64	0.95	12.6016	2588 5521
2	109	77	0.95	7 5693	540 3039	2	313	63	0.95	12.6208	2600.8953
2	103	71	0.95	7 6582	540 4673	2	315	64	0.95	12.6208	2605.0924
2	109	76	0.95	7 7068	544 9450	2	315	63	0.95	12.6385	2617 5144
2	103	70	0.95	7 7890	546 4250	2	335	70	0.95	12 7205	2713 2160
2	109	73	0.95	8.1012	560.3153	2	338	70	0.95	12.7467	2737.5134
2	141	96	0.95	8.5295	622.2562	2	353	70	0.95	12.8708	2859.0007
2	141	95	0.95	8.6511	625.0717	2	360	72	0.95	12.8860	2901.7317
2	109	64	0.95	8.7259	669.4365	2	360	71	0.95	12.9065	2908.3953
2	159	106	0.95	8.9770	674.9582	2	360	70	0.95	12.9251	2915.6948
2	114	65	0.95	9.0673	692.1787	2	361	70	0.95	12.9327	2923.7939
2	109	59	0.95	9.1208	717.1048	2	360	68	0.95	12.9562	2932.4703
2	141	85	0.95	9.1926	745.3059	2	361	68	0.95	12.9635	2940.6161
2	141	84	0.95	9.2996	748.5159	2	364	68	0.95	12.9853	2965.0533
2	141	83	0.95	9.4051	751.8767	2	360	64	0.95	12.9862	2977.2484
2	141	79	0.95	9.8101	767.0674	2	361	64	0.95	12.9931	2985.5185
2	141	78	0.95	9.9065	771.3613	2	370	70	0.95	12.9992	2996.6863
2	141	77	0.95	10.0008	775.8835	2	364	64	0.95	13.0134	3010.3289
2	141	76	0.95	10.0928	780.6497	2	370	68	0.95	13.0279	3013.9278
2	141	73	0.95	10.3533	796.6159	2	373	70	1.00	13.0284	3018.1715
2	141	72	0.95	10.4344	802.5597	2	373	68	1.00	13.0552	3035.9763
2	141	71	0.95	10.5122	808.8675	2	373	64	1.00	13.0745	3084.0035
2	159	83	0.95	10.6047	847.8610	2	389	72	0.90	13.0856	3139.7224
2	220	114	0.90	11.1053	1087.6350	2	389	71	0.90	13.1031	3146.8529
2	240	121	0.95	11.4684	1166.2799	2	389	70	0.90	13.1188	3154.6406
2	295	148	0.95	11.6569	1399.3660	2	389	68	0.90	13.1441	3172.4436
2	389	195	0.90	11.7478	1819.3841	2	395	71	0.95	13.1533	3191.1560
2	240	64	0.95	11.7494	1984.8323	2	395	70	0.95	13.1681	3199.1651
2	240	63	0.95	11.7715	1994.2967	2	395	68	0.95	13.1913	3217.5716
2	240	59	0.95	11.8166	2043.3565	2	400	71	1.00	13.1932	3228.3818
2	252	63	1.00	11.9452	2093.9313	2	400	70	1.00	13.2071	3236.6450
2	261	68	1.00	11.9556	2124.3695	2	399	68	0.95	13.2156	3250.1546
2	261	64	1.00	12.0499	$2\overline{157.9757}$	2	400	68	1.00	13.2282	3255.7387
2	261	63	1.00	12.0648	2168.7146	2	400	64	1.00	13.2356	3307.2424

TABLE VIII: Pareto–Optimal Solutions for $\sigma = 0.3$ and q = 0.1

D	F	M	p	TH	Delay	D	F'	M	p	TH	Delay
8	17	16	0.95	2.5709	382.7429	2	123	67	0.95	8.7557	1470.3953
8	23	21	0.95	2.9794	409.8701	2	123	64	0.95	8.7974	1494.7925
4	36	29	0.95	4.9584	531.2120	2	123	62	0.95	8.8147	1513.4240
4	49	43	0.65	5.2394	592.3880	2	141	77	0.95	9.0127	1616.5634
4	59	55	0.95	5.4939	596.0768	2	165	96	0.95	9.0944	1803.0229
4	63	59	0.95	5.5325	623.0541	2	167	96	0.95	9.1391	1824.8777
4	63	58	0.95	5.6006	626.1531	2	165	89	0.95	9.2716	1829.3365
4	63	57	0.95	5.6677	629 4164	2	165	87	0.95	9.3175	1838 0165
4	63	56	0.05	5 7337	632 8654	2	165	86	0.95	0.3306	1842 5371
4	63	55	0.05	5 7984	636 4888	2	165	85	0.95	9.3610	1847 2491
-+	63	55	0.95	5.7584	640.2000	2	103	80	0.95	9.3010	1841.2451
4	03	54	0.95	5.8019	640.2999	4	107	00	0.95	9.3790	1804.8709
4	63	53	0.95	5.9238	644.2895	2	107	80	0.95	9.3999	1869.6400
4	63	52	0.95	5.9844	648.5409	2	165	78	0.95	9.4442	1898.3002
4	63	50	0.95	6.1005	657.7897	2	167	78	0.95	9.4792	1921.3099
4	63	48	0.95	6.2091	668.2208	2	165	74	0.95	9.4992	1924.9458
4	63	47	0.95	6.2601	673.9414	2	165	71	0.95	9.5286	1948.1425
4	63	46	0.95	6.3089	680.0671	2	167	74	0.95	9.5321	1948.2784
4	63	45	0.95	6.3549	686.6102	2	165	70	0.95	9.5358	1956.5473
4	63	44	0.95	6.3982	693.6183	2	167	70	0.95	9.5666	1980.2630
4	63	43	0.95	6.4383	701.1650	2	177	78	0.95	9.6424	2036.3584
4	63	42	0.95	6.4751	709.2991	2	178	79	0.95	9.6447	2041.3628
4	63	41	0.95	6.5080	718.0637	2	183	81	0.95	9.6936	2086.0797
4	63	40	0,95	6.5369	727,6188	2	183	78	0.95	9.7317	2105.3875
4	63	39	0.95	6.5612	737,9782	2	183	71	0.95	9.7855	2160 6671
4	67	44	0.90	6 5640	745 8004	2	183	70	0.95	9 7884	2169 9888
-1	62	20	0.90	6 5904	740 2101	2	102	79	0.90	0.1004	22200.0000
4	62	27	0.95	6 5040	761 7190	2	102	71	0.95	0.0076	2220.4300
4	03	31	0.95	0.3940	762.0200	4	193	70	0.95	9.9076	2210.1304
4	67	42	0.90	0.0303	762.2380	2	193	70	0.95	9.9083	2288.5674
4	67	40	0.90	6.6820	781.3981	2	210	86	0.95	9.9942	2361.9468
4	67	39	0.90	6.7016	792.2349	2	210	78	0.95	10.0706	2416.0184
4	79	55	0.95	6.7081	798.1368	2	210	72	0.95	10.0894	2469.1626
4	79	54	0.95	6.7522	802.9158	2	230	94	0.95	10.1241	2541.7967
4	79	53	0.95	6.7949	807.9186	2	230	78	0.95	10.2703	2646.1154
4	79	52	0.95	6.8361	813.2507	2	232	78	0.95	10.2884	2669.1251
4	79	50	0.95	6.9134	824.8483	2	254	100	0.95	10.2973	2776.8890
4	74	42	0.95	6.9563	833.1455	2	254	96	0.95	10.3473	2796.3660
4	79	48	0.95	6.9829	837.9284	2	246	81	0.95	10.3992	2804.2383
4	79	47	0.95	7.0145	845,1018	2	254	89	0.95	10.4178	2836.6264
4	79	46	0.95	7 0435	852 7832	2	254	87	0.95	10 4332	2849 8842
4	79	45	0.05	7.0700	860.9880	2	254	86	0.95	10.4400	2856 8309
4	70	40	0.95	7.0025	860.7758	2	204	95	0.05	10.4461	2864.0117
-+	79	44	0.95	7.1120	870.2202	2	204	0.0	0.95	10.4401	2804.0117
4	79	43	0.95	7.1139	879.2392	4	234	81	0.95	10.4037	2893.4330
4	79	42	0.95	7.1307	889.4391	2	260	89	0.95	10.4689	2903.6333
4	79	41	0.95	7.1438	900.4291	2	264	85	0.95	10.5256	2976.7680
4	79	40	0.95	7.1527	912.4109	2	272	93	0.95	10.5343	3011.9094
4	79	39	0.95	7.1569	925.4063	2	272	89	0.95	10.5642	3037.6472
4	96	60	0.95	7.1706	944.8269	2	272	87	0.95	10.5758	3051.8445
4	96	59	0.95	7.2072	949.4172	2	272	86	0.95	10.5808	3059.2835
4	96	58	0.95	7.2427	954.1395	2	272	85	0.95	10.5850	3066.9731
4	96	57	0.95	7.2772	959.1121	2	284	96	0.95	10.6020	3126.6454
4	96	55	0.95	7.3424	969.8890	2	284	89	0.95	10.6515	3171.6610
4	96	54	0.95	7.3731	975.6963	2	284	87	0.95	10.6609	3186.4847
4	96	53	0.95	7.4023	981.7756	2	284	86	0.95	10.6647	3194.2518
4	96	52	0.95	7,4300	988.2540	2	284	85	0.95	10.6679	3202.2808
4	96	48	0.95	7.5225	1018,2421	2	295	96	0.95	10.6824	3247.7479
4	96	47	0.95	7.5404	1026.9687	2	295	89	0.95	10.7253	3294 5070
4	96	46	0.95	7 5558	1036 3027	2	205	87	0.95	10 7328	3309 9049
4	102	53	0.95	7 5682	1043 1366	2	205	86	0.95	10.7357	3317 9729
4	102	45	0.95	7.5005	1046 2727	2	295	95	0.95	10.7337	2226 2129
4	90 02	40	0.95	7 5799	1040.2727	2	290	00	0.95	10.7305	2224 0170
4	96	44	0.95	1.5783	1020.9511	2	295	84	0.95	10.7395	3334.9172
4	96	43	0.95	7.5849	1068.4505	2	316	85	0.95	10.8580	3563.1011
4	96	42	0.95	7.5879	1080.8448	2	354	112	0.95	10.9240	3803.8598
4	99	44	0.95	7.6466	1089.9809	2	354	100	0.95	11.0102	3870.1524
2	89	58	0.95	7.7789	1127.3006	2	352	96	0.95	11.0186	3875.2788
4	113	54	0.95	7.8071	1148.4903	2	354	96	0.95	11.0284	3897.2974
4	120	55	0.95	7.9319	1212.3771	2	354	89	0.95	11.0429	3953.4084
4	118	51	0.95	7.9587	1223.1750	2	364	100	0.95	11.0600	3979.4787
4	125	52	0.95	8.0702	1286.8042	2	373	100	0.95	11.1025	4077.8724
2	119	85	0.95	8.1154	1329.9973	2	373	96	0.95	11.1165	4106.4744
2	119	78	0.95	8.3546	1359.7707	2	381	100	0.95	11.1386	4165.3335
2	119	74	0.95	8.4775	1379.2029	2	381	96	0.95	11.1510	4194,5489
2	119	71	0.95	8.5578	1396.1073	2	381	89	0.95	11.1554	4254 9396
2	120	72	0.95	8 5631	1401 8800	2	388	96	0.95	11 1800	4271 6142
- 4	120	74	0.95	8 6010	1401.0090	2	200	20	0.95	11 1990	4211.0142
2	120	74	0.95	8.0019	14420.0027	4	300	09	0.95	11.1620	4433 6347
2	123	(1	0.95	0.0701	1443.0352	4	391	-09	0.95	11.2149	4433.0247
2	123	70	0.95	8.6983	1449.3770	1					

TABLE IX: Pareto–Optimal Solutions for $\sigma = 0.3$ and q = 0.5

D	P			77 II	D I	D				<i>T</i> II	D I
D	P 15	1/1	<i>p</i>	1 H	Delay	D	F 100	M	<i>p</i>	1 H	Delay
8	15	14	0.65	3.5494	486.2434	2	190	80	0.65	8.2488	3526.0701
8	21	20	0.70	4.1795	517.2701	2	190	78	0.65	8.2532	3528.6310
4	27	25	0.70	5.9640	569.5834	2	190	77	0.65	8.2553	3529.8855
4	30	34	0.70	6.6902	638.5545	2	190	76	0.65	8.2572	3531.3037
4	45	40	0.05	0.8980	761 5621	2	190	73	0.05	8.2091	3532.0045
4	40	39	0.70	0.9309	701.3031	2	190	74	0.05	8.2008	3534.2299
2	40	39	0.65	7.3231	799.2733	2	190	(2	0.65	8.2639	3537.3681
2	40	40	0.75	7.5092	923.1974	2	190	69	0.05	8.2070	3542.0321
2	49	47	0.70	7.6208	940.0313	2	190	60	0.05	8.2093	3008.0003
2	53	52	0.65	7.0398	1005.9920	2	192	80	0.70	8.2713	3001.3333
2	52	19	0.65	7.6526	1003.7809	2	203	79	0.70	8.2708	2767 2459
2	57	40 56	0.03	7.6727	1012.3009	2	203	77	0.70	8.2803	2768 0142
2	58	57	0.70	7.6799	1073.7923	2	203	76	0.70	8 2836	3708.9142
2	58	56	0.70	7.6871	1092.6309	2	203	75	0.70	8 2851	3771 9770
2	58	54	0.70	7.6996	1095.6516	2	203	74	0.70	8 2864	3773 6576
2	58	53	0.70	7.7045	1097.3687	2	203	72	0.70	8.2886	3777.2528
2	58	52	0.70	7.7083	1099.2644	2	203	69	0.70	8.2910	3783.1159
2	58	51	0.70	7.7111	1101.3748	2	211	75	0.65	8.2929	3923.1169
2	58	50	0.70	7.7124	1103.7255	2	211	74	0.65	8.2941	3924.8553
2	66	64	0.65	7.7283	1234.3443	2	211	72	0.65	8.2963	3928.3404
2	60	47	0.70	7.7283	1151.0835	2	211	69	0.65	8.2986	3934.1862
2	66	62	0.65	7.7452	1236.1641	2	216	82	0.80	8.3009	3998.6755
2	66	60	0.65	7.7608	1238.2040	2	227	84	0.70	8.3063	4204.1572
2	66	58	0.65	7.7750	1240.5655	2	227	80	0.70	8.3127	4209.7116
2	66	56	0.65	7.7872	1243.2832	2	227	78	0.70	8.3155	4212.7463
2	66	55	0.65	7.7924	1244.7943	2	227	77	0.70	8.3166	4214.5001
2	66	54	0.65	7.7969	1246.4572	2	227	76	0.70	8.3177	4216.1664
2	66	53	0.65	7.8007	1248.2644	2	227	75	0.70	8.3187	4217.9250
2	66	52	0.65	7.8035	1250.2541	2	227	74	0.70	8.3195	4219.8043
2	66	51	0.65	7.8054	1252.4819	2	227	72	0.70	8.3208	4223.8246
2	66	50	0.65	7.8059	1254.8955	2	227	69	0.70	8.3218	4230.3808
2	68	52	0.50	7.8177	1289.2939	2	231	70	0.70	8.3262	4302.6695
2	68	49	0.50	7.8252	1295.4080	2	241	80	0.70	8.3304	4469.3414
2	71	50	0.70	7.8457	1351.1122	2	241	78	0.70	8.3327	4472.5632
2	82	66	0.55	7.8678	1534.0174	2	241	77	0.70	8.3335	4474.4252
2	86	67	0.70	7.9066	1604.6209	2	241	75	0.70	8.3352	4478.0613
2	88	62	0.65	7.9460	1648.2188	2	241	74	0.70	8.3358	4480.0565
2	89	52	0.65	7.9760	1685.9488	2	241	72	0.70	8.3367	4484.3248
2	99	69	0.70	7.9845	1844.9667	2	241	69	0.70	8.3370	4491.2853
2	99	60	0.70	8.0208	1856.9478	2	243	75	0.70	8.3374	4515.2237
2	99	58	0.70	8.0252	1860.6909	2	243	74	0.70	8.3380	4517.2354
2	99	56	0.70	8.0274	1865.0080	2	243	72	0.70	8.3388	4521.5391
2	101	61	0.70	8.0284	1892.7587	2	243	69	0.70	8.3390	4528.5574
2	101	60	0.70	8.0311	1894.4619	2	250	80	0.70	8.3407	4636.2463
2	101	58	0.70	8.0351	1898.2807	2	250	78	0.70	8.3427	4639.5884
2	101	50	0.70	8.0369	1902.6850	2	250	77	0.70	8.3434	4641.5199
2	112	60	0.65	8.0372	2085.1841	2	250	76	0.70	8.3442	4643.3550
2	112	69	0.65	8.0506	2088.2872	2	250	73	0.70	8.3448	4645.2918
2	112	60	0.65	8.07706	2099.4495	2	250	74	0.70	8.3433	4047.3010
2	112	59	0.65	8.0790	2101.1947	2	250	72	0.70	8 2470	4031.7892
2	112	56	0.65	8.0820	2103.2021	2	259	80	0.70	8 3502	4091.3043
2	12	51	0.03	8 1177	2430 6213	2	259	77	0.70	8 3526	4808.6146
2	134	72	0.70	8.1317	2493.3574	2	259	75	0.70	8.3538	4812.5223
2	134	69	0.70	8.1407	2497.2277	2	259	74	0.70	8.3542	4814.6666
2	134	62	0.70	8.1546	2509.0903	2	261	86	1.00	8.3603	4820.1051
2	134	61	0.70	8.1555	2511.1862	2	277	80	0.65	8.3627	5140.6391
2	134	60	0.70	8.1560	2513.4459	2	277	76	0.65	8.3653	5148.2691
2	141	69	0.70	8.1627	2627.6815	2	277	75	0.65	8.3657	5150.2530
2	149	77	0.70	8.1637	2766.3441	2	277	74	0.65	8.3659	5152.5351
2	149	76	0.70	8.1669	2767.4378	2	277	72	0.65	8.3662	5157.1104
2	149	75	0.70	8.1699	2768.5922	2	308	92	0.70	8.3827	5691.5973
2	149	74	0.70	8.1728	2769.8275	2	308	85	0.70	8.3895	5702.5459
2	149	69	0.70	8.1852	2776.7698	2	308	84	0.70	8.3903	5704.3190
2	149	64	0.70	8.1931	2785.6431	2	308	80	0.70	8.3926	5711.8554
2	149	61	0.70	8.1947	2792.2891	2	308	78	0.70	8.3933	5715.9729
2	156	69	0.65	8.1997	2908.6874	2	308	77	0.70	8.3934	5718.3525
2	156	61	0.65	8.2087	2924.2348	2	308	75	0.70	8.3935	5722.9995
2	157	61	0.65	8.2108	2942.9799	2	318	80	0.65	8.3948	5901.5279
2	167	78	0.95	8.2187	3094.7539	2	318	78	0.65	8.3954	5905.8141
2	167	76	0.95	8.2224	3097.8993	2	318	75	0.65	8.3958	5912.5648
2	167	74	0.95	8.2256	3101.1971	2	320	72	0.70	8.4000	5954.2901
2	167	72	0.95	8.2281	3104.9101	2	322	76	0.70	8.4027	5980.6413
2	167	69	0.95	8.2303	3111.1743	2	338	84	0.70	8.4111	6259.9345
2	175	76	0.70	8.2321	3250.3485	2	340	84	0.70	8.4124	6296.9755
2	175	75	0.70	8.2342	3251.7043	2	340	80	0.70	8.4136	6305.2950
2	175	(4	0.70	8.2362	3253.1531	2	348	11	0.70	8.4181	0400.9957
2	175	(2	0.70	8.2398	3230.2524	2	371	84	0.60	8.4185	0882.9977
2	175	61	0.70	0.2443	3201.3008	2	3/1	00	0.60	0.4190	7140 8620
2	175	62	0.70	8 9479	3219.0342	2	307	93 75	0.70	0.4047 8 / 261	7381 4005
4	110	03	0.00	0.4413	0400.9000	4	391	10	0.00	0.4301	1001.4090

TABLE X: Pareto–Optimal Solutions for $\sigma = 0.3$ and q = 0.9

D	F	М	n	TH	Delay	D	F	М	n	TH	Delay
8	24	23	0.95	1.0816	482.1846	4	282	100	0.80	13.3747	2119.0839
4	45	44	0.80	1.7129	510.5045	4	282	99	0.80	13.4082	2125.3488
4	50	49	0.80	1.7998	522.3037	4	307	115	0.95	13.7849	2133.8342
4	44	41	0.80	2.1929	530.2067	4	307	114	0.95	13.8244	2138.4273
4	51	46	0.80	2.7648	558.4541	4	307	108	0.95	14.0478	2168.2810
4	49	43	0.65	2.8875	582.7430	4	307	107	0.95	14.0826	2173.6675
4	84	77	0.95	3.3419	655.7478	4	307	106	0.95	14.1167	2179.1983
2	106	99	0.80	4 1350	676.0835	4	307	103	0.95	14 2145	2196 5686
4	84	70	0.95	4.6197	685.1580	4	307	100	0.95	14.3047	2215.2925
2	94	80	0.80	5.3874	691.3841	4	307	99	0.95	14.3331	2221.8408
2	82	66	0.55	5.4999	712,4999	4	307	96	0.95	14.4124	2242.5935
2	94	76	0.80	6.0519	720.6762	4	307	95	0.95	14.4367	2249.8936
2	106	86	0.80	6.4505	745.4130	4	307	94	0.95	14.4601	2257.3807
2	113	92	0.80	6.6102	763.0810	4	307	93	0.95	14.4822	2265.1139
2	106	80	0.80	7.3030	789,7908	4	307	88	0.95	14.5754	2307.1432
2	113	87	0.80	7.3064	799.1850	4	307	87	0.95	14.5902	2316.3117
2	113	86	0.80	7.4536	804.5776	4	307	86	0.95	14.6036	2325.7678
2	106	77	0.80	7.5440	831.6270	4	307	85	0.95	14.6155	2335.5275
2	106	76	0.80	7.6750	838.4724	4	320	96	0.95	14.6417	2337.5567
2	141	110	0.95	7.8908	876.5295	4	320	95	0.95	14.6631	2345.1660
2	113	78	0.80	8.3085	879.6103	4	320	94	0.95	14.6836	2352.9701
2	113	77	0.80	8.4264	886.5457	4	320	93	0.95	14.7028	2361.0308
2	113	76	0.80	8.5399	893.8432	4	320	89	0.95	14.7682	2395.5419
2	133	94	0.80	8.6201	945.6255	4	320	88	0.95	14.7813	2404.8398
2	141	100	0.95	8.8192	968.5614	4	320	87	0.95	14.7931	2414.3966
2	141	99	0.95	8.9484	971.9871	4	320	86	0.95	14.8036	2424.2531
2	131	88	0.65	9.0119	974.9198	4	320	85	0.95	14.8125	2434.4260
2	141	96	0.95	9.3237	983.2123	4	344	103	0.95	14.8758	2461.3017
2	141	95	0.95	9.4444	987.2952	4	344	100	0.95	14.9429	2482.2822
2	141	94	0.95	9.5628	991.5692	4	344	99	0.95	14.9635	2489.6197
2	167	115	0.95	9.5820	1102.7337	4	344	96	0.95	15.0195	2512.8735
2	167	114	0.95	9.7016	1104.9455	4	344	95	0.95	15.0361	2521.0534
4	140	73	0.95	9.9381	1121.9289	4	344	94	0.95	15.0517	2529.4429
2	135	73	0.80	10.1506	1185.4403	4	344	93	0.95	15.0661	2538.1081
2	141	77	0.95	10.2458	1211.5940	4	360	103	0.95	15.1197	2575.7808
2	141	75	0.95	10.3925	1226.4849	4	344	87	0.95	15.1275	2595.4763
2	141	74	0.95	10.4585	1234.7695	4	360	100	0.95	15.1782	2597.7372
2	141	73	0.95	10.5192	1243.6733	4	360	99	0.95	15.1960	2605.4159
2	167	93	0.95	10.5568	1355.4545	4	360	96	0.95	15.2434	2629.7513
4	198	108	0.95	10.5770	1378.0303	4	360	95	0.95	15.2572	2638.3117
4	107	70	0.80	10.8044	1379.8561	4	360	94	0.95	15.2699	2647.0914
2	107	86	0.95	11.1804	1380.1322	4	371	103	0.95	15.2752	2654.4852
4	198	99	0.95	11.2162	1413.8372	4	360	93	0.95	15.2814	2656.1596
-4	100		0.95	11.3049	1440.3032	-4	971	100	0.95	15.3282	2077.1123
4	198	95	0.95	11.3090	1451.0714	4	371	99	0.95	15.3442	2085.0259
4	198	03	0.95	11.4320	1455.9005	4	371	95	0.95	15 3981	2718 9268
4	198	87	0.95	11.4303	1400.0070	-1	371	94	0.95	15 4090	2710.5200
4	198	86	0.95	11 8934	1500.0066	4	371	93	0.95	15 4187	2737 3201
4	198	85	0.95	11.9451	1506.3011	4	387	103	0.95	15,4855	2768.9644
4	198	80	0.95	12.1798	1540.9922	4	394	106	0.95	15.5221	2796.7561
4	198	78	0.95	12.2614	1556.5868	4	394	103	0.95	15.5722	2819.0490
4	198	77	0.95	12.2993	1564.7940	4	394	100	0.95	15.6148	2843.0790
4	198	75	0.95	12.3690	1582.1176	4	394	99	0.95	15.6273	2851.4830
4	198	74	0.95	12.4004	1591.2887	4	394	96	0.95	15.6588	2878.1167
4	198	73	0.95	12.4296	1600.7821	4	394	95	0.95	15.6672	2887.4856
4	198	58	0.95	12.5055	1803.7844	4	394	94	0.95	15.6747	2897.0944
4	234	78	0.95	13.2976	1839.6026	4	394	93	0.95	15.6809	2907.0192
4	252	75	0.80	13.3429	2093.5234	4	394	87	0.95	15.6932	2972.7258

TABLE XI: Pareto–Optimal Solutions for $\sigma = 0.6$ and q = 0.1

MTHDela 21 20 0.80 3.0617 606.5836 2 134 82 0.65 1964.2666 8.679 $0.80 \\ 0.65$ 3.08663.2343633.1166645.0447134 131 80 66 $0.65 \\ 0.65$ 8.7377 8.9691 1972.9318 2010.5983 19 2123 24 2 8 2422 0.65 3.2872662.9600 2 13466 0.658.9983 2066.19644 33 32 0.80 4.5097665.9423 2 134 62 0.659.0370 2100.8596 764.08 5.2184 44 41 0.65 5.2858771.8553 2 165 96 0.80 9.14522338.72372342.5424 2354.7310 5.347780.2228 9.1706 0.65 16595 0.80 789.3018 4 44 39 0.655.40452 165 92 0.80 9.243'799.1628 809.8669 165 165 89 87 0.80 2368.0712 2377.7307 38 0.65 37 0.65 9.3119 9.3543 44 5.45575.500444 4 4 44 36 0.655.5385821.5762 2 16586 0.809.37442382.8307 44 35 0.65 5.5690 834.3767 2 164 82 0.65 9.3797 2404.0278 49 43 0.655.6496842.8861 165 0.809.3999 2418.33214 2 82 80 53 52 0.65 5.6880 878,6946 2 165 0.80 9.4320 2430.5392 2 4 57 55 0.80 5.6973883.5793 2 164 760.659.43922451.04624 57 54 0.80 5.7677888.2728 2 165 76 0.80 9.4848 2457.96709.492 5.8359 0.6 2478.31060.80 1644 4 57 51 0.80 5.9653904.0813 2 165 72 0.80 9.51942490.2428910.0245 916.3409 9.5322 9.5361 2519.4115 2528.7776 57 57 6.026 $0.65 \\ 0.65$ 0.80 16449 0.80 6.0842 164 66 4 2 0.80 0.80 6.1390 923.0690 164 173 65 72 0.65 9.5384 9.6310 2538.6201 57 57 482 2 930.2820 47 2614.31546.1906 4 4 4 57 46 0.806.2386937.9995 2 173 67 0.659.65952657.671957 45 0.80 6.2827 946.2612 2 173 66 0.65 9.6611 2667.5520 57 44 0.80 6.3226955.1494 975.0618 2 176 67 87 0.809.68242708.81254 4 57 42 0.80 6.3882 2 188 0.80 9.7132 2724.6827 4 57 41 0.80 6.4132986.2627 2 188 82 0.80 9.7801 2755.43294 57 40 0.80 6.4323998.4370 2 188 80 0.80 9.8013 2769.341757 39 38 0.806.4451 6.4507 1011.69193 188 86 72 0.80 9.802 2803.02984 4 57 0.80 1026.15942 0.80 9.84452837.367660 40 0.80 6.6062 1050.9864 205 216 70 0.80 10.02933116.7413 68 58 0.50 6.64721082.7653 2 82 0.80 10.1337 3165.8165 2 10.1457 222 82 3272 002'68 53 0.50 6.9030 1111.7013 2 222 80 0.65 10.1613 3286.2108 2 $0.50 \\ 0.50$ 6.94656.98681118.573222278 72 0.6510.17393301.4415 2 68 68 522 51 1125.9050 2 222 0.65 10.1896 3354.7863 68 500.507.02321133.8587 230740.8010.28103447.8134 2 2 49 2 68 0.50 7.0565 1142.2236 2 243 96 0.80 10.2936 3464.7542 68 46 0.50 7.1316 1171.3265241 89 0.70 10.3003 3494.0982 10.3335 68 45 0.507.1447 1183.0110 2 241 85 0.70 3520.55592 3521.7973 68 44 0.507.15451195.248424387 0.80 10.375068 43 0.507.15811208.569024380 0.80 10.40083579.52144 80 56 0.80 7.1863 1233.8766 259 94 0.80 10.4684 3704.9638 271 1253.66674 80 53 0.80 7.2937 2 92 0.6510.5039 3922.8083 1261.0516 1270.6889 0.95 $\frac{4}{2}$ 80 76 52 0.80 51 0.65 7.32507.3614295 313 106 112 $\begin{array}{rrrr} 10.7171 & 4122.8338 \\ 10.7346 & 4370.9054 \end{array}$ 2 0.80 7.37987.40281277.2288 1286.0939 313 305 111 87 0.80 10.744910.76444375.6552 4451.9255 80 80 50 49 2 80 80 0.80 7.4227 1295.53661328.0868313 313 96 92 0.80 10.860310.87514 48 2 4462.8316 45 4492.9683 4 80 44 0.80 7.46511340.5615338 115 0.80 10.88024705 2 2 88 66 0.657.50141349 0509 2 338 112 0.80 10.90764720 0192 2 8964 53 0.657.62781375.8701 2 338 338 111 0.8010.91624725.14844 91 0.807.7305 1426.04592 104 0.8010.96824764.41290.80 7.7514 1434.4462338 96 0.80 11.0058 4819.2878 338 4 88 46 0.857.75251442.22302 95 0.8011.00854827.0804.847 785 338 11.0137 4851.8316 91 0.80 14527.8318 94 53 0.80 1473.0584 2 338 89 4 0.8011.0139 4878.9640 7.8997 7.9644 1546.89011578.270594 105 46 62 0.80 $354 \\ 371$ 105 0.80 11.052811.07864983.60455164.9186105 580.80 8.0666 1604.2988 2 371 1120.80 11.1003 5180.8495 4 105 54 0.80 8.1407 1636.2943 371 111 0.80 11.1069 5186 4795 373 1645.4376 4 105 0.80 8.1539 112 0.80 11.1109 5208 786 105 510.80 8.1730 1665.43312 373 111 0.80 11.11745214.43894 110 69 0.808.3080 1670.8476 2 3711040.8011.1456 5229.57 119 80 0.808.3164 1741.20822 373 106 0.80 11.1461 5244.5778 373 371 11.1553 5257.7693 11.1678 5289.8100 78 77 1753.0259 1758.1192 119 119 0.80 8.3695 8.3995 104 96 0.80 0.800.801774.6982 1786.9638 95 96 11.1686 119 0.80 8.4826 371 0.80 5298 3634 74 2 72 373 11.1767 5318.3265 119 0.80 8.5319 0.80 119 119 68 67 0.80 8.6130 8.6292 1815.0873 1822.9924 373 388 95 112 0.80 $11.1774 \\ 11.1868$ 5326.9260 5418.2469 2 8.64348.65570.80 119 66 65 0.80 1831.27372 388 388 111 104 11.1925 11.2252 5424.1348 5469.2077 119 0.80 1840.0329 8.6792 11.2405119 62 0.80 1869.1775 388 96 0.80 5532.2002

TABLE XII: Pareto–Optimal Solutions for σ = 0.6 and q = 0.5

D	F	M	p	TH	Delay	D	F	M	p	TH	Delay
8	20	19	0.80	4.4211	712.0432	2	241	78	0.70	8.3404	5270.6887
2	31	26	0.25	6.6935	807.2328	2	241	77	0.70	8.3410	5272.7466
4	39	37	0.80	6.9757	908.1188	2	241	76	0.70	8.3414	5274.8697
4	44	43	0.80	7.2158	983.0341	2	241	75	0.70	8.3418	5276.9815
4	45	44	0.80	7.2471	1000.4334	2	260	95	0.80	8.3475	5655.1146
2	46	45	0.80	7.3657	1065.5176	2	261	99	1.00	8.3477	5668.0079
2	49	48	0.90	7.4056	1128.3589	2	261	95	1.00	8.3528	5673.9279
4	57	55	0.80	7.4836	1224.3075	2	261	93	1.00	8.3550	5677.0893
4	57	54	0.80	7.4841	1226.8717	2	261	89	1.00	8.3584	5684.2392
2	57	54	0.80	7.6501	1272.9937	2	261	88	1.00	8.3591	5686.0937
2	69	50	0.80	7.7049	1408.3339	2	201	86	1.00	8.3390	5600 2274
2	68	56	0.50	7 8069	1507.2090	2	201	82	1.00	8.3606	5699 4040
2	68	55	0.50	7.8122	1509.3825	2	263	77	0.90	8 3642	5753 9560
2	68	54	0.50	7.8169	1510.9754	2	269	89	0.80	8.3653	5859.9126
2	68	50	0.50	7.8275	1519.0360	2	269	87	0.80	8.3673	5863.1766
2	76	51	0.80	7.8279	1710.1501	2	269	86	0.80	8.3682	5864.8578
2	82	66	0.55	7.8783	1804.7541	2	269	77	0.80	8.3714	5884.0144
2	100	65	0.80	8.0055	2202.5175	2	271	78	0.90	8.3721	5926.2778
2	109	73	0.90	8.0235	2389.7177	2	282	95	0.90	8.3752	6131.3354
2	110	64	0.80	8.0577	2424.7774	2	282	93	0.90	8.3773	6134.4438
2	125	77	0.90	8.0857	2734.7684	2	282	89	0.90	8.3806	6141.4300
2	129	64	0.80	8.1311	2843.6039	2	282	88	0.90	8.3812	6143.3341
2	133	64	0.80	8.1438	2931.7776	2	282	87	0.90	8.3818	6145.2561
2	134	64	0.80	8.1469	2953.8211	2	282	86	0.90	8.3822	6147.2888
2	145	75	0.80	8.1654	3174.5546	2	286	80	0.90	8.3860	6248.8011
2	152	60	0.90	8.1714	3370.7711	2	296	87	0.80	8.3928	6451.6739
2	164	86	0.80	8.1912	3575.5989	2	296	86	0.80	8.3934	6453.5238
2	164	76	0.80	8.2134	3587.2802	2	296	11	0.80	8.3939	6754 8208
2	164	64	0.80	8.2132	2615 1242	2	211	80	0.80	8.4038	6774 8422
2	174	78	0.80	8 2338	3805 0640	2	311	88	0.80	8 4046	6776 6196
2	174	77	0.90	8 2351	3806 7998	2	311	87	0.80	8 4051	6778 6168
2	174	76	0.90	8.2363	3808.6910	2	311	86	0.80	8.4055	6780.5605
2	174	75	0.90	8.2373	3810.5736	2	312	89	0.90	8.4069	6794.7736
2	187	89	0.80	8.2398	4073.6195	2	312	87	0.90	8.4075	6799.0067
2	187	87	0.80	8.2447	4075.8886	2	312	86	0.90	8.4076	6801.2557
2	187	86	0.80	8.2470	4077.0573	2	320	80	0.90	8.4116	6991.6656
2	187	78	0.80	8.2618	4088.6954	2	333	93	0.90	8.4211	7243.8645
2	187	77	0.80	8.2632	4090.3743	2	333	88	0.90	8.4226	7254.3626
2	187	76	0.80	8.2643	4092.2465	2	336	93	0.90	8.4232	7309.1245
2	187	75	0.80	8.2654	4094.0830	2	336	89	0.90	8.4245	7317.4485
2	195	78	0.90	8.2754	4264.2958	2	336	88	0.90	8.4246	7319.7172
2	195	76	0.90	8.2762	4200.2411	2	300	89	0.90	0.43/4	1103.0109
2	195	75	0.90	8.2708	4208.3006	2	311	105	0.80	8.4380	0183.0986
2	200	75	0.90	8 2855	4270.4705	2	377	99	0.80	8 4457	8199.9162
2	202	78	0.90	8 2873	4417 3731	2	377	93	0.80	8 4465	8203 8182
2	202	77	0.90	8,2880	4419,3883	2	377	89	0.80	8,4473	8212.5913
2	202	76	0.90	8.2884	4421.5838	2	377	88	0.80	8.4475	8214.7447
2	202	75	0.90	8.2887	4423.7694	2	383	101	0.90	8.4497	8315.6270
2	204	75	0.90	8.2919	4467.5691	2	383	99	0.90	8.4508	8319.2897
2	205	70	0.80	8.2962	4499.9777	2	383	95	0.90	8.4522	8327.3102
2	210	78	0.90	8.3000	4592.3186	2	383	93	0.90	8.4527	8331.5318
2	210	77	0.90	8.3005	4594.4135	2	389	101	0.90	8.4533	8445.8979
2	210	76	0.90	8.3007	4596.6960	2	389	99	0.90	8.4542	8449.6180
2	210	75	0.90	8.3009	4598.9682	2	389	96	0.90	8.4554	8455.4837
2	216	82	0.80	8.3060	4715.6547	2	389	95	0.90	8.4555	8457.7641
2	217	73	0.80	8.3135	4755.4892	2	389	93	0.90	8.4559	8462.0519
2	225	78	0.90	8.3214	4920.3413	2	394	89	0.80	8.4561	8582.9203
2	241	89	0.70	8.3272	5253.1880	2	398	95	0.80	8.4573	8650.5754
2	241	08 87	0.70	0.0288	5255 2007	2	308	80	0.80	0.40/8 8 /591	8670 0566
2	2/1	86	0.70	8 3318	5257 2650	4	330	- 69	0.80	0.4001	3010.0300
	241	00	0.70	0.0010	0401.4009	1	1				

TABLE XIII: Pareto–Optimal Solutions for $\sigma = 0.6$ and q = 0.9

D	F	M	p	TH	Delay	D	F	M	p	TH	Delay
4	40	30	0 00	1 6003	572 3656	4	250	87	0.95	14 6678	2204 8949
-1	40	49	0.50	1.0005	612.0000	-1	200	07	0.55	14.0070	2204.0343
4	49	43	0.65	2.9521	648.8098	4	259	80	0.95	14.6854	2214.1994
4	66	61	0.95	3.0709	656.9047	4	276	102	0.95	14.6941	2231.1267
4	67	61	0.90	3.2746	672.0162	4	276	100	0.95	14.7605	2244.2382
2	75	69	0.35	3.3980	721.7626	4	276	99	0.95	14.7919	2251.0551
2	70	62	0.95	3.6486	743.3753	4	276	98	0.95	14.8220	2258.0739
2	75	64	0.35	4 3944	754 4130	4	276	96	0.95	14 8785	2272 6482
2	67	52	0.00	4.8460	762.0047	4	276	0.4	0.05	14.0204	2212.0102
- 4	07	00	0.35	4.8402	703.0047	4	210	54	0.95	14.5254	2288.0018
Z	82	66	0.55	5.5338	775.7964	4	276	92	0.95	14.9745	2304.3787
2	75	57	0.35	5.5746	812.7838	4	286	100	0.95	15.0102	2325.5511
2	111	93	0.95	6.2698	815.3383	4	276	89	0.95	15.0305	2330.7009
2	80	57	0.35	6.3019	870.8308	4	286	99	0.95	15.0385	2332.6151
2	80	55	0.35	6.5507	891.1966	4	286	98	0.95	15.0654	2339.8881
2	141	120	0.95	6 7672	904 8020	4	286	96	0.95	15 1155	2354 9905
2	141	120	0.55	0.1012	000.55020	-1	200	50	0.55	15.1001	2004.0000
2	141	117	0.95	7.1466	928.5723	4	286	94	0.95	15.1601	2370.9688
2	141	114	0.95	7.6108	938.5886	4	286	92	0.95	15.1989	2387.8707
2	141	113	0.95	7.7620	942.1270	4	286	89	0.95	15.2454	2415.1466
2	131	100	0.65	7.8672	976.8011	4	286	88	0.95	15.2575	2424.8071
2	131	99	0.65	8.0095	980.7535	4	286	87	0.95	15.2679	2434.7488
2	141	107	0.95	8.4203	991.2166	4	286	86	0.95	15.2763	2445.0233
2	141	106	0.05	8 5580	995.0520	1	305	105	0.05	15 3082	2445 1651
2	191	100	0.55	0.0000	1052 0247	-1	300	107	0.95	15 2202	2440.1001
2	131	92	0.65	8.0184	1053.0347	4	309	107	0.95	10.3393	2404.2739
2	131	89	0.65	8.9953	1066.2043	4	305	102	0.95	15.3904	2465.5567
2	141	99	0.95	8.9991	1082.9416	4	309	105	0.95	15.3971	2477.2328
2	141	98	0.95	9.1244	1086.8355	4	305	100	0.95	15.4396	2480.0458
2	141	96	0.95	9.3679	1095.1867	4	305	98	0.95	15.4839	2495.3352
2	141	94	0.95	9.6011	1104.3618	4	305	96	0.95	15.5231	2511.4409
4	117	58	0.95	9 7605	1210 7953	4	309	100	0.95	15 5233	2512 5710
4	140	79	0.05	10 1006	1220.0000	4	200	00	0.05	15 5450	2520.2020
4	140	70	0.95	10.1990	1228.0812	4	309	33	0.95	15.5450	2520.2030
4	135	71	0.95	10.3554	1238.1972	4	309	98	0.95	15.5654	2528.0610
4	140	73	0.95	10.5635	1266.7329	4	309	96	0.95	15.6026	2544.3779
4	154	75	0.95	11.1962	1391.1716	4	309	94	0.95	15.6341	2561.6411
4	153	63	0.75	11.2093	1565.2193	4	309	92	0.95	15.6599	2579.9023
4	208	118	0.95	11.3660	1583.3111	4	309	89	0.95	15.6868	2609.3716
4	208	114	0.95	11.6720	1598.0383	4	309	88	0.95	15.6924	2619.8091
4	208	107	0.95	12,1733	1627.1673	4	309	87	0.95	15.6963	2630.5503
4	194	90	0.95	12 3775	1631 8985	4	300	86	0.95	15 6982	2641.6510
4	208	100	0.55	12.0110	1601.3000	-1	220	114	0.05	15.0502	2650.0710
4	208	100	0.95	12.4200	1091.3099	4	0.1.4	114	0.95	15.7512	2030.9719
4	208	99	0.95	12.4865	1696.4473	4	344	118	0.95	15.7527	2675.1656
4	208	98	0.95	12.5462	1701.7368	4	342	114	0.95	15.8315	2682.3444
4	208	96	0.95	12.6619	1712.7204	4	338	107	0.95	15.9351	2695.5488
4	208	94	0.95	12.7721	1724.3410	4	338	105	0.95	15.9791	2709.7239
4	208	92	0.95	12.8765	1736.6332	4	342	107	0.95	16.0094	2727.4488
4	208	88	0.95	13.0662	1763.4961	4	338	102	0.95	16.0374	2732.3219
4	208	87	0.95	13,1094	1770.7264	4	342	105	0.95	16.0517	2741.7916
4	210	96	0.05	13 1139	1803 2060	1	338	100	0.05	16.0706	2748 3786
-± 4	215	04	0.95	12 2110	1915 5201	-+	242	100	0.95	16.0714	2740.2120
4	219	94	0.95	10.2119	1010.0321	4	342	104	0.95	10.0714	2149.2129
4	219	92	0.95	13.3042	1828.4744	4	338	99	0.95	16.0854	2756.7269
4	219	88	0.95	13.4698	1856.7579	4	344	105	0.95	16.0873	2757.8255
4	219	87	0.95	13.5070	1864.3706	4	342	102	0.95	16.1073	2764.6571
4	253	107	0.95	13.8021	2017.6741	4	344	102	0.95	16.1417	2780.8246
4	258	110	0.95	13.8243	2042.2914	4	342	99	0.95	16.1528	2789.3509
4	259	107	0.95	13 9986	2065 5241	4	344	100	0.95	16 1723	2797 1664
4	250	105	0.05	14.0876	2076 3861	1	344	00	0.05	16 1859	2805 6620
	250	104	0.05	14 1207	2010.0001		244	08	0.05	16 1080	2814 4100
4	209	104	0.95	14.1307	2082.0003	4	344	90	0.95	10.1980	2014.4109
4	259	102	0.95	14.2134	2093.7023	4	344	96	0.95	16.2187	2832.5760
4	259	100	0.95	14.2917	2106.0061	4	344	94	0.95	16.2338	2851.7947
4	259	99	0.95	14.3291	2112.4032	4	344	92	0.95	16.2432	2872.1242
4	259	98	0.95	14.3651	2118.9896	4	344	89	0.95	16.2453	2904.9315
4	259	96	0.95	14.4334	2132.6662	4	397	123	0.90	16.4166	3090.9416
4	259	94	0.95	14,4963	2147 1361	4	397	114	0.90	16.6104	3147,7727
х Л	250	02	0.05	14 5599	2162 4492	4	300	00	0.05	16 8522	3180 0200
4	209	94	0.95	14.0003	2102.4423	4	390	99	0.95	10.0002	3100.0308
4	259	88	0.95	14.6483	2195.8917	1				1	

TABLE XIV: Pareto–Optimal Solutions for σ = 0.8 and q = 0.1

MTHTHDelas 15 14 0.65 2.3127 661.8219 2 131 72 0.65 2076.7187 8.8693 8.9083 8.9567 $0.65 \\ 0.65$ 2.95193.3045671.3739708.5869131 131 $0.65 \\ 0.65$ 2089.7811 2111.6505 $\frac{20}{24}$ 19 70 67 23 2 8 29270.95 3.8514746.8732 2 131 66 0.658.9698 2119.6131 4 36 34 0.654.8151 753.1532 2 131 61 0.658.9725 2174.6842141 4 45 42 0.655.3697848.8844 2 145 76 0.659.1234 2273.13282285.3644 0.655.43001450.6 9.1608 876.4810 2291.90144 4539 0.655.53452 14573 0.659.17789.2041 9.2220 2339.4613 2356.4765 38 0.65 36 0.65 5.57775.6432 $145 \\ 145$ 68 $0.65 \\ 0.65$ 45.2810911.8767 45 66 4 4 49 43 0.655.7008915.7795 2 14562 0.659.23682395.881955 53 0.65 5.8079 953.9355 4 154 62 0.95 9.2598 2502.6493 0.655.9137165 9.26072566.97404 5447 977.5025 4 77 0.952572.6750 4 54 46 0.65 5.9694 984.6409 4 165 76 0.95 9.2780 54450.65 6.0214992.2821 165 740.95 9.31052584.61364 4 4 54 41 0.656.18731028.8474 4 165 73 0.959.32552590.89119.339 0.65 1039.8 1650.9 2597.446340 6.21663 53 0.656.49361092.6915 17597 0.959.3813 2609.3509 2 2 62 0.95 61 0.95 6.5317 6.5885 1153.7952 4 1158.4285 2 165 175 9.4009 9.5291 2643.2502 2651.4667 71 71 $0.95 \\ 0.95$ 66 89 4 0.95 6.6967 6.7970 1168.4388 2 1179.5347 2 175 175 88 83 0.95 9.5444 9.5584 2657.5715 2705.8605 7157 71 4 4 4 71 56 0.956.8439 1185.6087 2 167 63 0.659.5736 2747.202971 55 0.95 6.8884 1192.0081 2 184 95 0.95 9.5939 2753.5331 71 $\frac{54}{53}$ 0.956.93036.96941198.78902 175 76 75 0.959.6035 2765.62194 4 71 0.95 1206.0031 2 175 0.95 9.6047 2775.6963 4 71 520.95 7.0055 1213.68092 184 91 0.95 9.6080 2791.02124 71 51 0.957.03851221.87292 184 89 0.959.6369 2803.12657150 0.95 49 0.95 7.0681 18485 83 0.95 9.685 4 1230.6556 1239.9972 4 71 2 184 9.7037 2845.019071 0.95 7.1156 1250.0440 1255.9469 0.95 9.7315 2888.0089 68 44 0.507.13202 184 76 0.95 9.7338 2907.8539 2 0.95 189 2930 8273 4 47 7 1330 83 9 751(57 0.65 7.1339 1266.1304 2 189 76 0.65 9.8303 2977.6490 752 46 $0.95 \\ 0.65$ 7.1457 1272.4479189 189 74 73 0.659.8448 9.8505 2993.41224 71 2 7.1665 2 56 1274.1739 2 0.65 3001.7868 75 55 0.657.19681282.5376189 720.659.8551 3010.5032 2 2 54 2 75 0.65 7.223 1291.4465 2 202 89 0.95 9.9108 3077.3453 75520.65 7.26611311.2252202 85 0.95 9.9443 3106.86942 75 50 0.657.29081334.07422 210 91 0.959.9988 3185.4046 1405.777410.017 76 43 0.95 7.3560 21089 0.95 3199.22044 Δ 85 56 0.657.3634 1463.20222 210 85 0.95 10.04523229.9137 7.396 3247.0326 85 55 0.65 1469.8165 2 210 83 0.95 10.0536 216 7.42734 85 54 0.65 1476.80412 82 0.8010.13913343.9824 7.4827
7.5069
 1110.0011
 2

 1491.9769
 2

 1500.2244
 2
 85 78 85 85 52 0.65 51 0.65 222 219 0.65 10.14073429.167910.16133433.3420 4 4 0.65 7.5472 1518.25791538.6625222 222 0.65 10.198010.20013497.55603506.627785 85 49 47 2 76 75 0.65 7.62847.67101549.7942 1553.9355 $222 \\ 248$ 74 94 0.65 10.201110.4056 99 99 76 2 3516.071475 3739.2999 25799 0.657.71061558.6908 2 99 0.95 10.455'3840.644374 99 73 0.657.75121563 1527 2 260 102 0.9510.45783866.9956 2 99720.65 7.7907 1567.8185 1580.1359 2 25789 99 0.95 10.5101 10.5126 3915.236446 263 4 88 2 3930.30910.658.077 1621.812426194 1.00 10.52633935 8.1017 263 10.5612 99 62 0.651629.16632 88 0.954015.7829
 61
 0.65
 8.1238

 57
 0.65
 8.1877
 292 292 10.6181 00 1636.902101 4402 99 1672.5753 2 10.6365 4413.7618 99 0.658.1967 1682.9037 1693.9069 292 292 10.668810.703899 99 56 55 0.65 95 89 0.6 4437.4355 4478.5551 99 540.658.2045 1705.6286 2 311 120 0.95 10.72624524.6355120 83 0.95 8.2485 1843.3711 312 120 0.95 10.7344 4539.1842 10.8754120 0.95 8.4002 1880.4273 309 99 0.95 4617 396 120 76 0.958.4227 1887.1168311 101 0.9510.8809 4632.71552 1200.958.4975 8.5276 1917.0384 2 31199 0.9510.8887 4647.6279 72121 72 0.951933.0137 2 312 99 0.95 10.89534662.5721311 312 10.8978 123 121 0.95 95 95 8.586 1964.96430.9 4680.33562 8.62340.9510.90414 1966.3316 2 4695.3844121 121 127 61 75 327 355 0.95 8.638 1974.2276 98 0.9 10.9915 4894 9571 2 11.0092 5145.3129 0.958.6553 2004.58711240.95 2020.40422028.8656127 127 0.95 8.6856 $355 \\ 355$ 120 99 0.95 11.044011.14425164.7769 5305.1701 73 72 2 11.1922 11.2212 11.2878 127 131 $0.95 \\ 0.65$ 389 389 0.90 70 76 8.7179 8.7771 2047.10812 124 120 5648.83442053.6580 5669.42768.8018 2059.067131 0.65389 106 0.90 131 74 0.658.82542064.7085389 99 0.90 11.29435817.364873 0.65 8.8479 131 2070.6144

TABLE XV: Pareto–Optimal Solutions for σ = 0.8 and q = 0.5

TABLE XVI: Pareto–Optimal Solutions for σ = 0.8 and q = 0.9

				<i>T</i>H	D	5		14			DI
<i>D</i>	F	M	<i>p</i>	1 H	Delay	D	F 150	M	<i>p</i>	1 H	Delay
8	4	4	0.10	1.2232	580.6966	2	153	78	0.90	8.1797	3473.7790
4	9	9	0.10	2.7377	582.7466	2	153	((0.90	8.1815	3475.4053
2	10	12	0.10	3.9130	744.9778	2	155	73	0.90	0.1047	3478.8940
2	21	22	0.10	6 8607	806 5820	2	152	79	0.90	8.1800	2484 8211
4	45	40	0.20	7 1671	1009 1132	2	153	68	0.90	8 1884	3484.8211
4	40	40	0.65	7 3153	1159 4253	2	167	82	0.95	8 2082	3785 8383
2	55	53	0.90	7.5638	1286.6573	2	174	88	0.90	8.2137	3935.5270
2	56	54	0.65	7.6617	1292.8592	2	171	55	0.40	8.2167	3942.9031
2	57	54	0.35	7.6664	1317.6165	2	174	81	0.90	8.2283	3945.4780
2	57	53	0.35	7.6741	1318.8991	2	174	78	0.90	8.2327	3950.5744
2	57	52	0.35	7.6812	1320.2712	2	174	77	0.90	8.2339	3952.4238
2	57	51	0.35	7.6874	1321.7345	2	174	75	0.90	8.2356	3956.3899
2	57	50	0.35	7.6930	1323.3494	2	174	74	0.90	8.2362	3958.5477
2	57	49	0.35	7.6978	1325.1288	2	174	72	0.90	8.2367	3963.1299
2	57	48	0.35	7.7015	1327.0671	2	185	72	0.90	8.2579	4213.6726
2	57	47	0.35	7.7042	1329.2275	2	206	65	0.35	8.2595	4727.8212
2	57	46	0.35	7.7055	1331.5755	2	210	74	0.90	8.2989	4777.5576
2	66	59	0.35	7.7410	1519.7440	2	210	82	0.80	8.3003	4895.4450
2	66	53	0.35	7 7814	1527 1463	2	222	81	0.05	8 3110	5035 8132
2	66	49	0.35	7.7965	1534.3596	2	222	78	0.65	8.3156	5040.7448
2	66	48	0.35	7.7981	1536.6040	2	222	77	0.65	8.3165	5042.5951
2	76	51	0.35	7.8763	1762.3127	2	222	75	0.65	8.3182	5046.4049
2	77	57	0.65	7.8813	1770.8244	2	222	74	0.65	8.3189	5048.3225
2	97	73	0.90	7.9503	2208.0011	2	222	72	0.65	8.3196	5052.6777
2	100	69	0.35	7.9533	2291.1564	2	222	70	0.65	8.3198	5057.3573
2	100	68	0.35	7.9588	2292.0469	2	231	88	0.90	8.3217	5224.7544
2	100	65	0.35	7.9743	2295.0578	2	231	82	0.90	8.3270	5235.7903
2	100	64	0.35	7.9791	2296.1463	2	231	81	0.90	8.3274	5237.9622
2	100	60	0.35	7.9959	2301.2085	2	231	78	0.90	8.3280	5244.7280
2	100	58	0.35	8.0027	2304.2115	2	232	- 77	0.90	8.3292	5269.8984
2	100	57	0.35	8.0055	2305.8556	2	233	82	0.90	8.3296	5281.1218
2	100	54	0.35	8.0079	2307.0701	2	233	77	0.90	8 3304	5202 6135
2	100	53	0.35	8 0124	2313 8581	2	234	77	0.90	8 3316	5315 3286
2	100	52	0.35	8.0127	2316.2652	2	240	88	0.90	8.3341	5428.3163
2	107	72	0.65	8.0199	2435.2983	2	240	82	0.90	8.3385	5439.7821
2	107	70	0.65	8.0287	2437.5539	2	240	81	0.90	8.3387	5442.0386
2	107	69	0.65	8.0327	2438.7950	2	240	78	0.90	8.3389	5449.0681
2	107	68	0.65	8.0366	2440.1145	2	241	81	0.70	8.3390	5465.3048
2	107	65	0.65	8.0469	2444.3455	2	241	78	0.70	8.3414	5470.8672
2	107	64	0.65	8.0497	2445.9472	2	241	77	0.70	8.3419	5472.8820
2	107	60	0.65	8.0575	2453.4791	2	241	75	0.70	8.3425	5477.3519
2	107	58	0.65	8.0584	2458.1665	2	261	87	1.00	8.3587	5906.2749
2	121	78	0.90	8.0635	2747.2370	2	268	83	0.90	8.3692	6072.0590
2	121	71	0.90	8.0009	2748.3231	2	290	100	0.90	8.3760	6548 1022
2	121	73	0.90	8.0751	2752 7817	2	290	88	0.90	8 3887	6559 2155
2	121	72	0.90	8.0810	2755,9682	2	290	82	0.90	8,3893	6573,0700
2	121	69	0.90	8.0865	2761.4835	2	293	88	0.90	8.3914	6627.0695
2	121	68	0.90	8.0877	2763.5555	2	305	77	0.90	8.3976	6928.0992
2	121	65	0.90	8.0887	2770.5941	2	310	100	0.90	8.3979	6989.6680
2	127	75	0.65	8.1006	2886.9058	2	310	94	0.90	8.4029	6999.6956
2	128	75	0.90	8.1023	2910.4462	2	310	88	0.90	8.4057	7011.5752
2	128	74	0.90	8.1047	2912.0336	2	355	100	0.90	8.4334	8004.2972
2	128	72	0.90	8.1090	2915.4044	2	355	94	0.90	8.4362	8015.7804
2	128	68	0.90	8.1140	2923.4306	2	357	94	0.90	8.4375	8060.9397
2	129		0.35	8.1147	2970.8955	2	307	88	0.90	8.4380 8.449F	8074.6205
2	133	75	0.05	8 1 2 3 5	3021.0120	2	365	94 88	0.90	8 4420	8255 5644
2	133	74	0.65	8.1269	3024,4439	2	371	100	0.90	8.4439	8365.0543
2	133	72	0.65	8.1330	3027,0531	2	371	94	0.90	8,4461	8377,0550
2	133	70	0.65	8.1385	3029.8567	2	380	94	0.90	8.4513	8580.2720
2	133	69	0.65	8.1410	3031.3993	2	389	100	0.90	8.4547	8770.9060
2	133	68	0.65	8.1432	3033.0395	2	389	95	0.90	8.4562	8781.1819
2	133	65	0.65	8.1486	3038.3001	2	389	94	0.90	8.4563	8783.4890
2	133	60	0.65	8.1511	3049.6529	2	391	94	0.90	8.4573	8828.6483
2	147	79	0.90	8.1595	3336.0577	2	392	94	0.90	8.4579	8851.2279
2	153	81	0.90	8.1731	3469.2977	1			1		

F	M	p	TH	Delay	F	M	p	TH	Delay
35	31	0.90	1.8753	127.1952	202	39	0.90	7.8158	634.8245
38	32	0.90	2.2487	134.2682	206	40	0.90	7.8218	638.8094
42	33	0.90	2.7312	144.7044	202	38	0.90	7.8412	643.9364
42	32	0.70	2.8720	168.0062	206	39	0.90	7.8477	647.6156
55	39	0.90	3.4313	169.8965	200	39	0.90	7.8555	650.5380
44	30	0.80	3.5247	172.6169	202	37	0.90	7.8646	654.0918
58	40	0.90	3.6043	176.7670	207	38	0.90	7.8798	659.8754
58	39	0.90	3.7444	179.1636	215	40	0.90	7.8912	666.7185
58	37	0.90	4.0204	184.7209	206	37	0.90	7.8948	667.0441
58	35	0.90	4.2899	191.4523	207	37	0.90	7.9021	670.2821
58	34	0.90	4.4214	195.4144	215	39	0.90	7.9152	675.6795
58	33	0.85	4.5351	204.0413	209	37	0.90	7.9166	676.7583
58	30	0.90	4.9142	217.6605	216	38	0.90	7.9448	688.5657
74	29	0.90	5 19247	225.7215	215	35	0.90	7 9933	721 3374
63	30	0.85	5.2203	245.2353	215	34	0.90	8.0067	736.1158
79	39	0.90	5.2566	248.2729	234	37	0.90	8.0769	757.7103
81	40	0.90	5.2657	251.1823	261	44	0.90	8.0922	773.9638
63	29	0.85	5.3160	254.2610	262	44	0.90	8.0977	776.9291
81	39	0.90	5.3604	254.5583	261	43	0.90	8.1136	781.7019
67	30	0.90	5.4746	255.2908	261	42	0.90	8.1337	790.2795
81	37	0.90	5.5456	262.2843	271	44	0.90	8.1456	803.6176
79	35	0.90	5.6311	265.0496	261	40	0.90	8.1709	809.3653
79	34	0.90	5.7194	270.4798	261	39	0.90	8.1874	820.2435
85	30	0.90	5 7278	211.1091	∠00 271	39	0.90	0.2000 8.2101	032.8143 840.3754
81	34	0.90	5 8087	277 3273	283	40	0.90	8 2234	847 5925
85	35	0.90	5.8947	285.1799	271	39	0.90	8.2343	851.6705
85	34	0.90	5.9747	291.0225	282	42	0.90	8.2363	853.8652
83	32	0.90	6.0492	297.9668	283	42	0.90	8.2408	856.8931
84	32	0.90	6.0875	301.5568	282	40	0.90	8.2682	874.4866
85	32	0.90	6.1249	305.1467	283	40	0.90	8.2725	877.5876
84	31	0.90	6.1576	310.1310	282	39	0.90	8.2821	886.2401
85	31	0.90	6.1937	313.8230	283	39	0.90	8.2863	889.3828
80	30	0.90	6.2372	323.8763	304	43	0.90	8.3134	910.4880
101	29	0.90	6 4446	338 8608	311	44	0.90	8 3407	922.2327
119	42	0.95	6.5051	354.5080	316	44	0.90	8.3441	937.0596
110	37	0.90	6.5663	356.1886	311	42	0.90	8.3552	941.6740
119	40	0.95	6.6271	362.8811	316	43	0.90	8.3594	946.4283
119	39	0.95	6.6863	367.6119	316	42	0.90	8.3734	956.8135
107	33	0.90	6.7199	374.6307	311	40	0.90	8.3811	964.4161
119	37	0.95	6.8001	378.5494	311	39	0.90	8.3919	977.3783
119	35	0.95	6.9062	391.9717	316	40	0.90	8.3984	979.9212
119	34	0.95	6.9556	399.8521	316	39	0.90	8.4088	993.0918
129	37	0.90	7.0217	417.7121	242	43	0.90	8.4190	997.3438
124	34	0.90	7.0317	424.5505	343	44	0.90	8 4513	1017.1248
120	34	0.90	7.1210	441.6695	343	42	0.90	8.4630	1038.5665
151	42	0.90	7.1302	457.2115	353	44	0.90	8.4694	1046.7786
119	29	0.95	7.1383	460.8672	355	44	0.90	8.4754	1052.7093
151	40	0.90	7.2185	468.2535	353	43	0.90	8.4817	1057.2443
151	39	0.90	7.2607	474.5470	355	43	0.90	8.4876	1063.2344
135	32	0.90	7.2873	484.6448	353	42	0.90	8.4927	1068.8454
167	44	0.95	7.2936	487.4915	355	42	0.90	8.4984	1074.9012
101	31	0.90	7 3755	488.9498	359	43	0.90	8.4992	10/0.2145
151	35	0.90	7.4117	497.3029 506.6137	355	40	0.90	8.5170	1100.8608
167	40	0.95	7.4532	509.2534	359	40	0.90	8.5278	1113.2649
167	39	0.95	7.4903	515.8923	359	39	0.90	8.5347	1128.2277
167	37	0.95	7.5596	531.2415	382	43	0.90	8.5610	1144.1001
167	35	0.95	7.6208	550.0780	396	44	0.90	8.5856	1174.2899
183	39	0.85	7.6238	585.9487	393	43	0.90	8.5880	1177.0454
167	32	0.95	7.6906	588.0055	396	43	0.90	8.5951	1186.0304
202	43	0.90	7.7010	604.9953	393	42	0.90	8.5964	1189.9611
206	44	0.90	7.7057	610.8680	396	42	0.90	8.6033	1199.0447
202	42	0.90	7.7314	616.0754	393	40	0.90	8.6100	1218.6994
200	43	0.90	7 7451	619 9705	396	30	0.90	8 6211	1226.0025
206	42	0.90	7.7659	623.7455	396	38	0.90	8.6242	1262.3704
202	40	0.90	7.7890	626.4053	396	37	0.90	8.6252	1282.2789
195	37	0.90	7.8089	631.4252					

TABLE XVII: Pareto–Optimal Solutions with D = 2 for σ = 0.1 and q = 0.1

F	M	p	TH	Delay	F	M	p	TH	Delay
15	14	0.90	0.7306	116.9667	187	18	1.00	4.3440	1131.6741
28	26	0.95	0.7969	146.3892	200	20	0.95	4.3541	1159.9393
24	18	0.95	1.5421	147.5957	213	23	0.95	4.3552	1162.8256
22	15	0.95	1.7935	155.8577	213	22	0.95	4.3657	1182.8624
28	17	0.95	2.1403	178.7617	213	21	0.95	4.3738	1207.6106
41	25	0.90	2.1817	219.9218	222	23	0.95	4.3742	1211.9590
41	24	0.90	2.2834	223.2549	222	22	0.95	4.3838	1232.8425
41	23	0.90	2.3841	226.9657	232	24	0.95	4.3841	1246.3708
34	16	0.95	2.7010	227.3394	233	24	0.95	4.3860	1251.7431
32	14	0.95	2.7783	244.5266	222	21	0.95	4.3911	1258.6364
41	17	0.90	2.9497	266.5662	232	23	0.95	4.3936	1266.5518
41	16	0.90	3.0307	279.3819	243	25	0.95	4.3944	1287.5142
54	22	0.90	3.0422	304.3452	222	20	0.95	4.3968	1287.5326
54	21	0.90	3.1134	310.7936	232	22	0.95	4.4023	1288.3759
52	19	0.90	3.1916	314.9895	237	23	0.95	4.4027	1293.8481
54	19	0.90	3.2495	327.1045	233	22	0.95	4.4041	1293.9292
54	18	0.90	3.3130	337.8956	232	21	0.95	4.4087	1315.3317
54	17	0.90	3.3724	351.0871	233	21	0.95	4.4103	1321.0013
54	16	0.90	3.4257	367.9664	252	25	0.95	4.4104	1335.1999
66	20	0.90	3.4721	388.8944	237	21	0.95	4.4169	1343.6794
66	19	0.90	3.5233	399.7943	252	24	0.95	4.4198	1353.8165
66	18	0.90	3.5712	412.9835	252	23	0.95	4.4278	1375.7373
66	16	0.90	3.6522	449.7367	252	22	0.95	4.4349	1399.4428
86	23	0.95	3.6629	469.4976	260	23	0.95	4.4399	1419.4115
86	22	0.95	3.7050	477.5876	252	20	0.95	4.4430	1461.5235
75	17	0.95	3.7561	478.8267	260	21	0.95	4.4508	1474.0787
86	20	0.95	3.7833	498.7739	269	21	1.00	4.4709	1503.9981
86	19	0.95	3.8187	512.5226	281	22	0.95	4.4739	1560.4898
85	18	0.95	3.8406	522.7357	286	23	0.95	4.4749	1561.3526
86	18	0.95	3.8512	528.8856	291	24	0.95	4.4753	1563.3358
86	17	0.95	3.8792	549.0546	294	24	0.95	4.4790	1579.4526
86	16	0.95	3.9008	575.0351	306	26	1.00	4.4861	1582.8646
99	20	0.90	3.9061	583.3416	306	25	1.00	4.4935	1602.0943
103	21	0.95	3.9190	583.9619	306	24	1.00	4.5001	1623.8486
105	21	0.95	3.9357	595.3010	306	23	1.00	4.5053	1649.0165
110	22	0.95	3.9467	610.8679	306	22	1.00	4.5094	1677.3951
110	21	0.95	3.9750	623.6487	306	21	1.00	4.5117	1710.8677
110	20	0.95	4.0018	637.9666	306	20	1.00	4.5122	1749.3075
110	19	0.95	4.0255	655.5522	332	25	0.95	4.5146	1759.0729
119	21	0.95	4.0374	674.6745	339	26	0.95	4.5162	1772.3652
110	18	0.95	4.0462	676.4815	335	25	0.95	4.5175	1774.9681
119	20	0.95	4.0610	690.1639	332	24	0.95	4.5196	1783.5996
110	17	0.95	4.0624	702.2791	339	25	0.95	4.5214	1796.1618
118	19	0.90	4.0663	714.7838	335	24	0.95	4.5225	1799.7164
133	23	1.00	4.0801	716.7294	332	23	0.95	4.5232	1812.4793
133	22	1.00	4.1036	729.0639	339	24	0.95	4.5261	1821.2056
133	21	1.00	4.1254	743.6124	351	26	0.95	4.5276	1835.1038
133	20	1.00	4.1454	760.3199	339	23	0.95	4.5294	1850.6942
135	20	0.95	4.1468	782.9590	351	25	0.95	4.5324	1859.7427
141	21	0.95	4.1563	799.4042	351	24	0.95	4.5367	1885.6731
135	19	0.95	4.1627	804.5413	356	25	0.95	4.5367	1886.2348
133	18	1.00	4.1767	804.8805	362	26	0.95	4.5375	1892.6142
133	17	1.00	4.1863	835.1050	365	26	0.95	$4.5\overline{400}$	1908.2988
151	21	0.95	4.1989	856.0995	356	24	0.95	$4.5\overline{408}$	1912.5345
151	20	0.95	$4.2\overline{144}$	875.7541	365	25	0.95	$4.5\overline{443}$	1933.9205
152	20	0.95	4.2181	881.5538	362	24	0.95	$4.5\overline{457}$	$1944.\overline{7682}$
157	21	0.95	4.2219	890.1167	375	26	0.95	$4.5\overline{483}$	$1960.\overline{5810}$
158	21	0.95	4.2255	895.7863	376	26	0.95	$4.5\overline{491}$	1965.8092
157	20	0.95	4.2362	910.5523	375	25	0.95	4.5522	1986.9046
158	20	0.95	4.2396	916.3520	376	25	0.95	4.5530	1992.2030
179	24	1.00	4.2576	949.8984	382	26	0.95	4.5539	1997.1785
179	23	1.00	4.2734	964.6207	375	24	0.95	4.5557	2014.6080
174	21	0.95	4.2783	986.4988	376	24	0.95	4.5564	2019.9802
187	24	1.00	4.2826	992.3519	389	26	0.95	4.5592	2033.7760
179	21	1.00	4.3010	1000.8017	382	24	0.95	4.5608	2052.2140
187	22	1.00	4.3109	1025.0748	398	25	0.90	4.5618	2134.8613
187	21	1.00	4.3227	1045.5303	398	24	0.90	4.5637	2167.2155
187	20	1.00	4.3328	1069.0212	398	23	0.90	4.5647	2203.2373
199	21	0.95	4.3438	1128.2371	400	22	0.90	4.5658	2254.4086

TABLE XVIII: Pareto–Optimal Solutions with D = 4 for σ = 0.1 and q = 0.1

F	M	n	TH	Delay	F	M	n	TH	Delau
33	32	0.95	7 1012	245 3070	179	76	P 1.00	8 0556	1033 4483
41	40	0.95	7.3404	270.1097	179	75	1.00	8.0578	1034.7290
47	34	1.00	7.3949	333.1892	179	70	1.00	8.0675	1042.0235
53	49	0.80	7.4412	338.7860	179	68	1.00	8.0705	1045.3901
59	58	0.85	7.4762	361.2183	179	67	1.00	8.0718	1047.1864
63	61	0.85	7.5030	382.7137	179	65	1.00	8.0739	1051.0750
63	60	0.85	7.5116	383.6504	179	63	1.00	8.0753	1055.2551
63	59	0.85	7.5198	384.6414	179	61	1.00	8.0759	1059.8911
63	58	0.85	7.5279	385.7077	187	70	1.00	8.0816	1088.5944
63	56	0.85	7.5429	387.9479	196	70	1.00	8.0960	1140.9866
66	64	1.00	7.5620	388.2742	213	75	0.95	8.0996	1240.3549
63	48	0.85	7.5866	400.2863	221	86	1.00	8.1058	1262.6918
63	47	0.85	7.5894	402.3536	221	85	1.00	8.1079	1263.8408
63	46	0.85	7.5915	404.5593	221	82	1.00	8.1137	1267.4084
63	44	0.85	7.5928	409.5500	221	76	1.00	8.1235	1275.9334
70	61	1.00	7.6322	414.4820	221	75	1.00	8.1248	1277.5146
66	43	1.00	7.6700	420.8535	221	70	1.00	8.1299	1286.5206
70	48	1.00	7.7016	433.1317	221	68	1.00	8.1311	1290.6772
70	47	1.00	7.7033	435.3956	221	65	1.00	8.1317	1297.6959
77	60	1.00	7.7047	456.9995	229	76	1.00	8.1336	1322.1210
77	56	1.00	7.7274	461.9959	229	70	1.00	8.1392	1333.0915
77	54	1.00	7.7367	464.9136	229	68	1.00	8.1401	1337.3985
77	48	1.00	7.7532	476.4448	229	65	1.00	8.1403	1344.6713
77	47	1.00	7.7537	478.9352	238	77	1.00	8.1430	1372.4190
84	58	0.95	7.7540	505.0006	239	70	1.00	8.1499	1391.3051
88	61	0.95	7.7664	525.1011	239	68	1.00	8.1505	1395.8002
88	47	0.95	7.8008	551.6826	255	83	1.00	8.1541	1460.9271
96	63	0.95	7.8058	570.2683	260	85	1.00	8.1565	1486.8716
96	61	0.95	7.8146	572.8376	264	83	1.00	8.1634	1512.4892
96	60	0.95	7.8186	574.2269	264	79	1.00	8.1680	1518.7843
97	61	0.95	7.8201	578.8046	264	75	1.00	8.1713	1526.0808
97	60	0.95	7.8240	580.2084	266	76	1.00	8.1724	1535.7389
96	55	0.95	7.8345	582.3037	264	70	1.00	8.1732	1536.8391
96	54	0.95	7.8366	584.1936	266	70	1.00	8.1749	1548.4819
97	56	0.95	7.8369	586.5320	281	79	1.00	8.1833	1616.5848
97	54	0.95	7.8414	590.2789	292	86	1.00	8.1856	1668.3530
97	49	0.95	7.8446	602.1189	292	85	1.00	8.1867	1669.8711
105	67	1.00	7.8506	614.2706	292	83	1.00	8.1889	1672.9048
105	65	1.00	7.8595	616.5516	292	82	1.00	8.1898	1674.5848
105	64	1.00	7.8637	617.7090	292	81	1.00	8.1906	1676.3327
105	63	1.00	7.8677	619.0036	292	79	1.00	8.1922	1679.8675
105	61	1.00	7.8751	621.7231	292	77	1.00	8.1933	1683.8082
105	60	1.00	7.8784	623.1812	292	76	1.00	8.1938	1685.8487
105	54	1.00	7.8923	633.9731	292	75	1.00	8.1942	1687.9379
105	49	1.00	7.8924	646.6391	292	70	1.00	8.1946	1699.8372
115	61	0.95	7.9022	686.2116	310	89	1.00	8.1969	1766.6876
119	65	0.95	7.9057	704.0403	310	86	1.00	8.2000	1771.1966
119	64	0.95	7.9089	705.4300	310	85	1.00	8.2010	1772.8084
119	63	0.95	7.9118	706.8951	310	83	1.00	8.2028	1776.0290
119	61	0.95	7.9171	710.0799	310	82	1.00	8.2035	1777.8127
119	57	0.95	7.9246	717.4567	310	81	1.00	8.2042	1779.6682
119	56	0.95	7.9257	719.5607	310	79	1.00	8.2054	1783.4210
119	54	0.95	7.9269	724.1573	310	77	1.00	8.2062	1787.6046
129	65	0.95	7.9411	763.2034	310	76	1.00	8.2065	1789.7709
129	63	0.95	7.9461	766.2989	319	86	1.00	8.2066	1822.6185
129	61	0.95	7.9502	769.7513	319	85	1.00	8.2075	1824.2770
129	57	0.95	7.9555	777.7472	319	83	1.00	8.2091	1827.5912
129	56	0.95	7.9561	780.0280	319	82	1.00	8.2098	1829.4266
129	54	0.95	7.9561	785.0109	319	81	1.00	8.2104	1831.3360
138	63	0.95	7.9727	819.7616	319	76	1.00	8.2123	1841.7319
146	75	1.00	7.9782	843.9677	322	81	1.00	8.2124	1848.5586
146	70	1.00	7.9933	849.9186	322	79	1.00	8.2134	1852.4566
146	68	1.00	1.9985	852.0645	322	76	1.00	8.2142	1859.0523
146	07	1.00	8.0009	854.1297	322	15	1.00	8.2143	1801.3561
140	64	1.00	8.0051	007.3014	332	00	1.00	0.4100	1002 0000
140	62	1.00	8.0070	860 7100	332	02	1.00	0.4183	1903.9800
140	61	1.00	8.0087	864 4000	332	01 76	1.00	0.4188	1016 7000
140	57	1.00	8.0110	004.4922	332	10	1.00	0.2202	1910./808
140	07 62	1.00	8.0139 8.014E	010.4200	344 244	09	1.00	0.2208	1900.4033
155	61	0.95	8.0145 8.0164	920.7408	344 244	00 95	1.00	0.4232	1903.4309
155	56	0.95	8.0166	924.0900	344	82	1.00	8 2251	1907.2400
167	75	0.95	8 0192	931.2429	344	80	1.00	8 2255	1072 7096
167	70	0.90	8 0202	070 / 2027	344	81	1.00	8 2250	1074 9576
167	69	0.90	8 02293	082 6771	344	70	1.00	8 2266	1070 0000
167	08	0.95	8.0328	904.0//1	344 244	19	1.00	0.2200	1979.0220
167	62	0.90	8 0290	900.0242	369	80	1.00	8 2217	2063 0259
167	61	0.90	8 0400	994.0304	360	80	1.00	8 22/15	2003.0332
167	60	0.95	8.0400	990.4998 008.0166	262	04 90	1.00	0.2040 9.225F	2004.0000
172	70	0.90	8 0414	1014 6116	362	81	1.00	0.4000 8 9950	2070.0204
173	68	0.95	8 0446	1017 0820	362	76	1.00	8 2361	2010.1902
173	65	0.95	8 0/82	1023 5221	305	82	0.05	8 2272	2083.5503
173	63	0.95	8 0/00	1027 6722	396	70	1.00	8 2474	2305 2587
170	77	1.00	8 0522	1021.0122	390	10	1.00	0.2414	2303.2301
119		1.00	0.0000	1002.1910					

TABLE XIX: Pareto–Optimal Solutions with D=2 for $\sigma=0.1$ and q=0.9

F	M	p	TH	Delay	F	M	p	TH	Delay
20	19	1.00	4.1950	142.9385	159	39	1.00	4.6884	892.2140
28	26	0.95	4.2882	176.6527	168	46	1.00	4.6915	917.6848
30	28	0.90	4.2901	187.9799	168	45	1.00	4.6922	921.0810
30	26	0.90	4.3060	192.6414	168	42	1.00	4.6940	931.1127
30	25	0.90	4.3124	195.4275	168	40	1.00	4.6943	939.2653
30	24	0.90	4.3176	198.4739	168	39	1.00	4.6947	942.7167
30	23	0.90	4.3214	201.9226	179	49	1.00	4.6970	969.2203
30	22	0.90	4.3234	206.1104	179	46	1.00	4.6996	977.7713
36	35	1.00	4.3263	206.4702	179	45	1.00	4.7001	981.3899
36	34	1.00	4.3359	207.8107	179	43	1.00	4.7011	988.1975
36	33	1.00	4.3451	209.1466	179	42	1.00	4.7014	992.0784
36	32	1.00	4.3540	210.7434	179	39	1.00	4.7016	1004.4422
36	30	1.00	4.3705	214.2174	187	49	1.00	4.7026	1012.5374
36	29	1.00	4.3780	216.1423	187	46	1.00	4.7049	1021.4706
36	28	1.00	4.3849	218.3544	187	45	1.00	4.7053	1025.2509
36	27	1.00	4.3911	220.6340	187	43	1.00	4.7061	1032.3628
36	26	1.00	4.3964	223.4830	187	42	1.00	4.7062	1036.4171
36	24	1.00	4.4039	229.9165	191	46	1.00	4.7074	1043.3203
36	22	1.00	4.4058	238.4012	198	49	1.00	4.7096	1072.0984
43	34	1.00	4.4095	248.2184	198	46	1.00	4.7115	1081.5571
43	33	1.00	4.4165	249.8140	198	45	1.00	4.7117	1085.5597
43	32	1.00	4.4231	251.7213	198	42	1.00	4.7122	1097.3828
43	29	1.00	4.4404	258.1700	219	58	1.00	4.7138	1161.6927
43	28	1.00	4.4450	260.8122	217	52	1.00	4.7182	1165.9556
43	26	1.00	4.4521	266.9380	217	49	1.00	4.7201	1174.9766
43	24	1.00	4.4552	274.6225	217	46	1.00	4.7213	1185.3429
52	36	1.00	4.4640	296.5489	219	46	1.00	4.7223	1196.2677
52	35	1.00	4.4696	298.2347	219	43	1.00	4.7223	1209.0238
52	34	1.00	4.4749	300.1711	224	49	1.00	4.7235	1212.8790
52	33	1.00	4.4800	302.1007	224	46	1.00	4.7245	1223.5798
52	32	1.00	4.4846	304.4072	238	52	1.00	4.7284	1278.7900
52	30	1.00	4.4927	309.4251	238	49	1.00	4.7297	1288.6840
52	29	1.00	4.4960	312.2056	238	46	1.00	4.7304	1300.0535
52	28	1.00	4.4986	315.4008	264	64	1.00	4.7306	1386.8496
52	26	1.00	4.5016	322.8088	264	62	1.00	4.7325	1390.6721
61	31	1.00	4.5311	359.6015	264	61	1.00	4.7331	1393.8399
67	36	1.00	4.5383	382.0919	264	58	1.00	4.7357	1400.3967
64	29	1.00	4.5458	384.2531	264	55	1.00	4.7375	1408.8282
64	28	1.00	4.5466	388.1856	263	53	1.00	4.7379	1410.3125
64	27	1.00	4.5469	392.2382	264	52	1.00	4.7388	1418.4898
67	30	1.00	4.5542	398.6824	264	49	1.00	4.7395	1429.4646
67	29	1.00	4.5554	402.2649	264	46	1.00	4.7395	1442.0762
79	42	1.00	4.5584	437.8447	272	43	1.00	4.7407	1501.6186
79	40	1.00	4.5654	441.6783	294	64	1.00	4.7426	1544.4461
79	36	1.00	4.5774	450.5263	294	62	1.00	4.7442	1548.7030
79	35	1.00	4.5798	453.0874	294	61	1.00	4.7445	1552.2308
79	29	1.00	4.5867	474.3124	294	59	1.00	4.7457	1557.5254
81	30	1.00	4.5911	481.9891	294	58	1.00	4.7465	1559.5326
90	35	1.00	4.6058	516.1755	294	55	1.00	4.7478	1568.9224
100	43	1.00	4.6097	552.0656	296	55	1.00	4.7484	1579.5953
101	34	1.00	4.6267	583.0245	294	52	1.00	4.7485	1579.6818
116	48	1.00	4.6275	630.1263	296	52	1.00	4.7491	1590.4279
116	46	1.00	4.6323	633.6395	296	49	1.00	4.7492	1602.7330
116	45	1.00	4.6343	635.9845	309	44	1.00	4.7507	1699.2107
116	42	1.00	4.6400	642.9112	317	46	1.00	4.7536	1731.5839
116	40	1.00	4.6430	648.5403	340	69	1.00	4.7538	1774.2927
116	39	1.00	4.6447	650.9234	340	64	1.00	4.7569	1786.0941
116	38	1.00	4.6456	654.3937	340	62	1.00	4.7580	1791.0171
118	40	1.00	4.6458	659.7220	340	58	1.00	4.7594	1803.5411
116	36	1.00	4.6471	661.5322	340	55	1.00	4.7600	1814.4000
116	35	1.00	4.6475	665.2929	340	52	1.00	4.7601	1826.8429
116	34	1.00	4.6476	669.6124	345	49	1.00	4.7606	1868.0503
118	36	1.00	4.6496	672.9380	359	64	1.00	4.7617	1885.9053
118	35	1.00	4.6500	676.7634	359	62	1.00	4.7627	1891.1034
124	42	1.00	4.6513	687.2499	359	58	1.00	4.7638	1904.3273
124	40	1.00	4.6537	693.2672	359	55	1.00	4.7642	1915.7929
124	38	1.00	4.6557	699.5243	363	52	1.00	4.7648	1950.4234
124	36	1.00	4.6567	707.1552	376	64	1.00	4.7656	1975.2100
126	38	1.00	4.6581	710.8070	376	62	1.00	4.7665	1980.6542
134	42	1.00	4.6635	742.6732	376	58	1.00	4.7674	1994.5043
134	40	1.00	4.6653	749.1759	376	55	1.00	4.7675	2006.5129
146	43	1.00	4.6750	806.0158	392	64	1.00	4.7690	2059.2615
148	42	1.00	4.6777	820.2660	392	62	1.00	4.7697	2064.9374
148	40	1.00	4.6789	827.4480	392	58	1.00	4.7704	2079.3768
148	39	1.00	4.6796	830.4885	392	55	1.00	4.7704	2091.8965
159	40	1.00	4.6878	888.9475	1				
					•				

TABLE XX: Pareto–Optimal Solutions with D = 4 for σ = 0.1 and q = 0.9

			(T) II	DI				(T) 11	
F	M	p	1 H	Delay	P	M	p	TH	Delay
59	58	1.00	2.1063	370.3544	267	62	1.00	12.1493	2230.7494
93	90	1.00	2.8918	395.9297	267	61	1.00	12.1538	2244.2711
87	81	1.00	3 5163	395 9749	281	69	0.85	12 1607	2288 7751
80	75	0.05	2 7064	200 7555	282	70	0.05	12 1702	2202.0601
02	10	1.00	4.4004	400.0000	200	10	0.55	10.1000	2252.0001
93	82	1.00	4.4961	420.0662	281	68	0.85	12.1883	2295.3987
88	74	0.95	5.0647	434.3924	283	69	0.95	12.2077	2298.3471
96	81	0.95	5.1804	443.8206	283	68	0.95	12.2342	2305.2475
93	75	1.00	5.7674	450.2873	281	66	0.85	12.2368	2310.5158
102	83	1.00	5.8360	459 5633	281	65	0.85	12 2573	2310 1/35
102	80	1.00	6.0050	463.0000	201	66	0.05	12.2015	2010.1400
102	84	1.00	0.0030	403.2229	283	00	0.95	12.2795	2321.1010
96	76	0.95	6.0222	468.5994	283	65	0.95	12.2980	2330.3376
102	81	1.00	6.1459	470.9645	283	64	0.95	12.3132	2340.4481
96	75	0.95	6.1879	473.1560	283	62	0.95	12.3324	2363.9356
93	71	1.00	6.4118	473.6980	283	61	0.95	12.3356	2377.5747
03	70	1.00	6 5682	479 4886	203	66	0.80	12 3550	2414 1383
00	10	1.00	0.0002	413.4000	200	00	0.00	12.3000	2414.1000
93	69	1.00	6.6526	494.9640	294	65	0.95	12.4179	2420.9161
93	68	1.00	6.8012	501.1260	293	61	0.80	12.4188	2467.1767
102	76	1.00	6.8517	504.7822	303	68	0.95	12.4570	2468.1625
96	70	0.95	6.8945	509.2894	303	66	0.95	12.4949	2485.2013
102	75	1.00	7.0022	509,4007	303	65	0.95	12,5095	2495.0258
9/	67	1.00	7.0812	513 1302	303	64	0.05	12 5200	2505 8507
- 74	01	1.00	7.0013	513.1302	303	04	0.93	12.0209	2000.0007
93	66	1.00	7.0839	514.6344	303	62	0.95	12.5323	2530.9982
120	90	1.00	7.2202	520.3065	311	68	0.95	12.5381	2533.3285
93	64	1.00	7.3446	529.9683	309	65	0.95	12.5676	2544.4322
102	71	1.00	7.5711	530.4633	311	66	0.95	12.5732	2550.8172
102	70	1.00	7,7038	536,4886	311	65	0.95	12.5865	2560.9010
102	60	1.00	7 8222	542 8627	211	64	0.05	12.5065	2572.0119
102	09	1.00	1.8323	542.8037	311	04	0.95	12.3903	2572.0118
102	68	1.00	7.9561	549.6221	311	63	0.95	12.6028	2584.2762
120	82	1.00	8.2047	566.1850	311	62	0.95	12.6051	2597.8232
102	62	1.00	8.2763	640.4361	319	68	0.90	12.6056	2601.5668
102	61	1.00	8.3685	649.6459	319	67	0.90	12.6239	2609.9115
154	104	1.00	8 8246	650 2395	319	66	0.90	12 6396	2619 0591
116	60	0.05	8 8406	676 8070	210	65	0.00	12.6525	2620.0041
110	09	0.95	0.0015	070.8070	319	03	0.90	12.0323	2029.0941
119	71	0.95	8.9015	682.6612	319	64	0.90	12.6623	2640.1140
120	71	1.00	9.0176	684.2333	319	63	0.90	12.6687	2652.2337
120	70	1.00	9.1197	690.0403	327	69	0.95	12.6695	2655.6873
120	69	1.00	9.2181	696.2207	327	68	0.95	12.6884	2663.6606
120	68	1.00	9.3126	702.8104	327	66	0.95	12.7185	2682.0489
110	66	0.05	0.2951	714 7679	207	65	0.05	12 7202	2602.6516
110	00	1.00	0.40001	714.1010	027	00	0.55	12.72.02	2052.0010
120	66	1.00	9.4882	/1/.3///	327	64	0.95	12.7366	2704.3340
120	65	1.00	9.5687	725.4454	334	69	1.00	12.7388	2710.1871
120	64	1.00	9.6437	734.1042	334	68	1.00	12.7560	2718.5418
124	67	0.95	9.6816	737.2330	336	68	0.95	12.7666	2736.9723
119	62	0.95	9.6880	749.3706	334	66	1.00	12.7823	2737.9122
120	62	1.00	9 7758	753 4542	334	65	1.00	12 7907	2749 1351
120	61	1.00	0.8217	764 2802	226	66	0.05	12.7501	2745.1501
140	75	1.00	9.0017	104.2093	330	64	0.95	10 7057	2700.0008
140	61	1.00	10.3408	000.1130	334	04	1.00	12.(95)	2101.34/4
179	93	1.00	10.9044	912.5794	336	65	0.95	12.8035	2766.7612
179	90	1.00	11.1564	921.4987	336	64	0.95	12.8095	2778.7652
283	147	0.95	11.3139	1343.3053	336	63	0.95	12.8119	2792.0154
293	150	0.80	11.3432	1418.4865	355	71	0.95	12.8672	2868.0009
310	162	0.90	11 5494	1510 6355	355	70	0.95	12 8865	2875 1990
010	102	1.00	11.0404	1700.0000	055	10	0.55	12.0000	2010.1330
380	195	1.00	11.8208	1788.8234	300	69	0.95	12.9038	2883.0830
248	64	0.80	11.8396	2058.9891	355	68	0.95	12.9188	2891.7416
248	62	0.80	11.8827	2077.6122	355	66	0.95	12.9412	2911.7045
248	61	0.80	11.8992	2088.2587	355	65	0.95	12.9479	2923.2150
248	60	0.80	11.9119	2099.9237	355	64	0.95	12.9514	2935.8977
253	61	0.70	11 9250	2141 7683	362	66	0.95	12 9914	2969 1184
250	61	0.70	11 0280	2150 2229	975	71	1.00	12.0014	2026 6070
204	01	0.70	11.9380	±100.2008	373	11	1.00	10.0200	3020.0079
253	60	0.70	11.9387	2153.0325	375	-70	1.00	13.0425	3034.3547
267	71	1.00	11.9437	2154.9449	375	69	1.00	13.0569	3042.8747
267	70	1.00	11.9772	2160.4605	375	68	1.00	13.0689	3052.2550
267	69	1.00	12.0087	2166.5268	375	66	1.00	13.0846	3074.0032
267	68	1.00	12 0379	2173 2056	375	65	1.00	13 0877	3086 6038
201	66	1.00	12.0019	2170.2000	202	65	1.00	19 1990	2144 2204
207	00	1.00	12.0004	±100.0903	362	00	1.00	13.1320	3144.2204
267	65	1.00	12.1092	2197.6619	389	64	0.80	13.1379	3229.6241
267	64	1.00	12.1265	2207.5843	393	65	1.00	13.1985	3234.7608

TABLE XXI: Pareto–Optimal Solutions with D = 2 for σ = 0.3 and q = 0.1

F	M	2 2	TU	Dolow	F	М		TU	Delaw
г	111	<i>p</i>	1 1	Delay	F	1/1	<i>p</i>	1 H	Delay
34	33	0.90	1.3673	311.6469	146	46	1.00	8.8400	1003.8562
54	51	0.90	1.8711	361.7802	146	45	1.00	8.8671	1016.9040
56	49	0.95	2.6455	376.9664	146	44	1.00	8.8902	1030.9933
36	29	0.85	2 7377	387 2301	170	58	0.95	8 9002	1060 4493
62	54	0.85	2.1011	417 6202	146	42	1.00	8 0227	1062 5056
03	54	0.85	2.8039	417.0203	140	44	1.00	0.9221	1002.3930
70	- 59	0.90	3.0928	439.5373	173	58	0.95	8.9686	1079.1631
70	58	0.90	3.2484	442.5826	173	57	0.95	9.0097	1086.8729
70	57	0.90	3.4027	445.7957	170	54	0.95	9.0603	1093.1592
70	54	0.90	3.8566	456.4441	170	52	0.95	9.1292	1112.3626
44	30	0.80	3.9097	458.9648	173	52	0.95	9.1893	1131.9926
70	50	0.00	4 1506	464 5714	170	40	0.05	0.2152	1145 7497
10	32	0.90	4.1300	404.3714	170	49	0.95	9.2100	1140.7427
63	44	0.85	4.4406	465.9087	173	50	0.95	9.2465	1153.9439
70	49	0.90	4.5761	478.6461	173	49	0.95	9.2713	1165.9617
60	39	0.85	4.7796	481.9291	173	48	0.95	9.2933	1178.7386
74	50	0.90	4.8682	500.7292	173	46	0.95	9.3275	1207.0901
70	45	0.90	5.1062	502.1384	173	45	0.95	9.3395	1222.7307
66	41	0.90	5 2017	502 8503	186	52	0.90	9 3675	1235 9681
66	40	0.00	5.2011	511.8126	186	50	0.00	0.4192	1260.0875
00	40	0.90	5.3200	511.8136	186	50	0.90	9.4123	1260.0875
70	43	0.90	5.3510	516.5293	186	49	0.90	9.4309	1273.2641
74	46	0.90	$5.3\overline{677}$	524.0001	186	48	0.90	9.4465	1287.3358
70	42	0.90	5.4672	524.5982	186	46	0.90	9.4687	1318.2854
74	45	0.90	5.4851	530.8320	186	45	0.90	9.4745	1335.3950
69	40	0.85	5 5557	543 9651	216	63	0.85	9.4770	1345 8400
00	40	0.00	5.0001	544 5991	102	40	0.00	0.4910	1259 2705
80	48	0.95	5.7001	544.5331	193	48	0.85	9.4819	1358.3725
70	39	0.90	5.7853	553.1735	224	64	0.85	9.5679	1387.6379
74	42	0.90	5.8141	554.5753	230	65	0.90	9.6841	1395.2227
74	40	0.90	6.0102	573.8516	230	64	0.90	9.7141	1402.8300
74	39	0.90	6.0998	584.7834	230	63	0.90	9.7430	1410.7551
88	50	0.95	6 1094	586 3202	230	62	0.90	9 7707	1419 0987
00	40	0.05	6 2102	502.4600	2200	61	0.00	0.7075	1427 7210
00	49	0.95	0.2102	592.4000	230	50	0.90	9.1913	1427.7210
88	48	0.95	6.3084	598.9864	230	58	0.90	9.8695	1456.3539
88	46	0.95	6.4959	613.4244	230	57	0.90	9.8907	1466.8442
88	45	0.95	6.5847	621.4098	230	54	0.90	9.9441	1501.7264
85	42	0.90	6.5975	637.5124	230	52	0.90	9.9700	1528.3477
88	43	0.95	6.7480	639.8316	252	64	0.90	9.9974	1537.0137
88	42	0.95	6 8244	649 8497	255	61	0.85	10 0345	1608 2307
00	40	0.05	6.0619	672 5208	200	82	1.00	10.0621	1611 7002
100	40	0.95	0.9018	072.3298	292	04	1.00	10.0021	1011.7093
100	48	0.95	7.0354	681.3518	298	82	1.00	10.1307	1644.8266
88	37	0.95	7.1200	715.1902	292	75	1.00	10.2632	1649.5250
91	39	0.90	7.1259	719.5900	292	73	1.00	10.3159	1662.0702
109	52	0.90	7.1427	724.3039	298	75	1.00	10.3253	1683.4193
109	50	0.90	7.2903	738.4384	298	73	1.00	10.3762	1696.2224
109	49	0.90	7 3604	746 1601	298	70	1.00	10 4475	1717 3317
103	10	0.00	7 4107	749 7177	200	65	1.00	10.4982	1723 0556
100	40	0.00	7.4107	743.1111	202	00	1.00	10.4302	1720.0000
109	48	0.90	1.4277	754.4065	298	67	1.00	10.5125	1740.8813
119	54	0.95	7.5058	765.2114	292	63	1.00	10.5352	1741.6114
109	46	0.90	7.5536	772.5436	292	62	1.00	10.5518	1751.6434
121	54	0.95	7.5915	$7\overline{78.0721}$	292	61	1.00	10.5675	1761.9951
119	52	0.95	7.6430	778.6539	298	63	1.00	10.5863	1777.3979
119	51	0.95	7.7083	785,9880	298	62	1.00	10.6020	1787.6361
121	52	0.95	7 7248	791 7405	292	58	1.00	10.6068	1796 3109
110	52	0.55	7 7714	702 7522	294	61	1.00	10.0008	1708 2004
119	50	0.95	1.1114	193.1033	298	01	1.00	10.0108	1798.2004
119	49	0.95	7.8319	802.0199	298	58	1.00	10.6532	1833.2214
121	50	0.95	7.8495	807.0937	298	57	1.00	10.6622	1846.2234
119	48	0.95	7.8898	810.8086	298	54	1.00	10.6797	1889.2279
121	49	0.95	7.9081	815.4992	298	52	1.00	10.6815	1922.1129
121	48	0.95	7.9641	824,4357	343	65	0.90	10.7724	2080.7017
110	46	0.05	7 9960	830 3106	334	58	0.05	10.8368	2083 4709
110	45	0.05	9 0441	841 0601	224	57	0.00	10.8404	2000.1109
119	40	0.95	0.0441	044.0091	334	57	0.95	10.0404	2098.3007 0100 0505
121	46	0.95	8.0665	844.2654	340	57	0.95	10.8751	2136.0507
119	42	0.95	8.1631	878.7741	383	75	0.95	10.9444	2190.8333
121	42	0.95	8.2259	893.5434	383	73	0.95	10.9747	2207.7073
146	58	1.00	8.2979	898.1554	383	65	0.95	11.0657	2290.3113
146	57	1.00	8.3540	904.5256	383	63	0.95	11.0796	2315,4323
146	54	1.00	8 5130	925 5949	383	62	0.05	11.0850	2328 7701
140	59	1.00	8,6007	041 7062	200	61	0.55	11.0800	2020.1191
140	52	1.00	8.6097	941.7063	383	01	0.95	11.0890	2342.8882
146	50	1.00	8.6975	959.8511	383	58	0.95	11.0936	2389.1298
146	48	1.00	8 7748	980 4055	398	61	0.90	11 0941	2470 5781

TABLE XXII: Pareto–Optimal Solutions with D = 4 for σ = 0.3 and q = 0.1

F	M	p	TH	Delay	F	M	p	TH	Delay
12	12	0.15	3.5861	546.3375	167	74	0.85	8.2252	3101.4186
18	17	0.15	5.1677	546.8462	167	70	0.85	8.2309	3108.5015
22	20	0.15	5 7844	588 8639	167	68	0.85	8 2326	3112 5065
40	20	0.10	7.0025	818 4041	174	65	0.85	8.2467	3250 1819
40	31	0.20	7.2233	818.4041	174	0.5	0.85	0.2407	3230.1812
44	43	0.25	7.4066	866.6762	179	75	1.00	8.2495	3322.5040
59	55	0.85	7.6948	1115.2087	179	74	1.00	8.2505	3324.3987
72	70	0.85	7.7558	1340.1914	179	70	1.00	8.2524	3333.1606
72	68	0.85	7.7715	1341.9181	181	75	0.85	8.2533	3359.7380
72	66	0.85	7.7863	1343.8637	181	74	0.85	8.2547	3361.4177
72	65	0.85	7.7934	1344.9492	181	70	0.85	8.2587	3369.0944
72	61	0.85	7.8178	1349.9078	181	68	0.85	8.2596	3373,4352
72	60	0.85	7 8228	1351 3605	193	83	0.85	8 2621	3570 4078
72	50	0.85	7 9272	1252.0766	102	75	0.85	8 9754	2592 4921
72	59	0.85	7.0212	1054 5150	193	73	0.85	0.2704	3582.4851
72	58	0.85	7.8311	1354.7173	193	74	0.85	8.2766	3584.2741
72	57	0.85	7.8342	1356.6164	193	70	0.85	8.2794	3592.4598
72	55	0.85	7.8376	1360.9327	193	68	0.85	8.2797	3597.0884
72	54	0.85	7.8377	1363.4563	211	75	0.60	8.2873	3926.4487
75	61	0.85	7.8467	1406.1540	211	74	0.60	8.2886	3928.0996
76	47	0.75	7.8526	1461.2977	211	70	0.60	8.2930	3935.1506
82	68	0.55	7.8537	1532.3326	211	68	0.60	8.2943	3939.1654
82	67	0.55	7 8608	1533 1597	211	65	0.60	8 20/0	3946.0566
82	66	0.55	7 8679	1534 0174	211	66	0.00	8 2040	30/3 6/01
04	65	0.00	1.0010	1504.01/4	211	00	0.00	0.2949	3343.0401
82	05	0.55	1.8745	1034.8956	215	82	0.85	8.3016	3978.8397
82	61	0.55	7.8992	1539.0160	215	75	0.85	8.3097	3990.8490
82	60	0.55	7.9047	1540.2262	215	74	0.85	8.3103	3992.8443
82	58	0.55	7.9147	1542.8547	215	70	0.85	8.3112	4001.9630
82	55	0.55	7.9264	1547.5694	222	70	0.65	8.3121	4137.2120
82	54	0.55	7.9293	1549.4039	222	68	0.65	8.3127	4141.6381
86	56	0.85	7.9440	1622.8717	224	83	0.85	8.3134	4143.8930
94	58	0.85	7 9916	1768 6587	224	82	0.85	8 31/0	4145 3958
07	60	0.85	8.0061	1920 5920	224	75	0.85	8 2217	4157 0078
100	00	0.85	8.0001	1017 0100	224	73	0.85	0.0217	4157.9078
103	70	0.85	8.0071	1917.2182	224	74	0.85	8.3222	4159.9866
103	68	0.85	8.0155	1919.6885	224	70	0.85	8.3225	4169.4870
103	66	0.85	8.0228	1922.4717	225	75	0.85	8.3230	4176.4699
103	65	0.85	8.0261	1924.0246	225	74	0.85	8.3235	4178.5579
103	64	0.85	8.0290	1925.6067	225	70	0.85	8.3237	4188.1008
103	61	0.85	8.0356	1931.1181	236	82	0.80	8.3287	4368.9233
103	58	0.85	8.0375	1937.9984	236	74	0.80	8.3354	4383.6492
105	61	0.60	8.0433	1969.1950	236	70	0.80	8.3356	4393,1992
105	59	0.60	8.0488	1972 5033	238	83	1.00	8 3359	4400 4692
105	59	0.60	8.0500	1074 2211	2200	74	1.00	0.0000	4420 1502
105	50	0.00	8.0505	1076 2506	238	14	1.00	8.3381	4420.1302
105	37	0.00	8.0327	1970.2390	243	02	0.85	8.3390	4497.0142
105	55	0.60	8.0545	1980.6412	243	75	0.85	8.3443	4510.5875
105	54	0.60	8.0546	1983.1211	243	74	0.85	8.3445	4512.8426
111	65	0.85	8.0650	2073.4634	248	74	0.80	8.3485	4606.5466
119	70	0.55	8.0665	2221.5635	254	85	0.85	8.3492	4695.4470
119	66	0.55	8.0819	2226.1961	260	75	0.65	8.3505	4834.1725
122	53	0.85	8.0917	2315.1104	260	74	0.65	8.3509	4836.3146
131	70	0.85	8.1319	2438.4039	260	70	0.65	8.3516	4845.3834
131	59	0.85	8 1/19	2461 6671	260	66	0.85	8 35/15	4852 8441
135	65	0.85	8 15/2	2521 6022	265	83	0.85	8 3620	4002.3734
120	69	0.00	8 1560	2573 2517	265	82	0.00	8 3697	4904 1519
190	66	0.70	9 1602	2576 4769	200	75	0.00	0.0007	4019 0595
138	00	0.70	0.1003	2010.4103	200	61	0.85	0.3003	4910.9030
138	65	0.70	8.1622	2578.2161	272	86	0.85	8.3673	5026.5765
138	61	0.70	8.1668	2586.1470	275	83	0.80	8.3704	5089.0919
138	59	0.70	8.1669	2591.0254	275	82	0.80	8.3712	5090.9063
146	75	1.00	8.1680	2709.9736	275	75	0.80	8.3737	5105.7237
146	74	1.00	8.1701	2711.5190	275	74	0.80	8.3737	5108.0658
146	72	1.00	8.1737	2714.8753	289	82	0.75	8.3805	5352.6773
146	70	1.00	8.1764	2718.6673	298	96	0.85	8.3811	5491.4676
146	68	1.00	8,1781	2722.8803	298	75	1.00	8.3936	5531,3195
146	66	1.00	8 1786	2727 5646	301	83	0.85	8 3952	5568 3562
150	60	1.00	9 1001	2022 0401	201	00	0.00	0.0000	5570 2750
102	00	0.85	0.1901	2032.9401	301	04	0.85	0.3907	5000.0055
153	- 28	0.75	8.2004	2870.1001	319	93	0.90	8.4051	3880.6255
158	74	0.85	8.2035	2934.2762	319	91	0.90	8.4068	5883.8741
158	70	0.85	8.2104	2940.9774	319	89	0.90	8.4081	5887.5163
158	68	0.85	8.2127	2944.7666	319	83	0.90	$8.4\overline{106}$	5899.6129
160	68	0.70	8.2141	2983.4802	319	82	0.90	8.4107	5901.8547
160	66	0.70	8.2167	2987.2189	344	93	0.95	8.4256	6339.5227
160	65	0.70	8.2176	2989.2361	344	91	0.95	8,4267	6343.2073
160	61	0.70	8 2187	2998 4313	358	91	0.85	8 4311	6605 7926
161	61	0.75	8 2200	3017 1944	304	82	0.85	8 / 51 /	7288 0110
169	60	0.15	8.2209	2027 0555	334	00	0.85	0.4014	1200.0110
103	08	0.80	0.4240	3037.99999	1				

TABLE XXIII: Pareto–Optimal Solutions with D = 2 for σ = 0.3 and q = 0.9

F	М		77.11	D -1	F	М	-	TH	Delesi
F	M	p	1 H	Delay	F	M	p	TH	Delay
29	28	0.90	6.2569	566.8349	153	75	1.00	7.9481	2233.2192
41	39	0.90	7.0068	676.2686	155	77	1.00	7.9523	2257.8913
45	42	0.90	7.1211	725.8764	155	75	1.00	7.9534	2262.4116
46	44	0.90	7.1576	733.0485	155	74	1.00	7.9536	2264.8660
48	42	0.90	7.1669	774.2682	158	82	1.00	7.9550	2291.5198
51	44	0.90	7.2319	812.7277	158	79	1.00	7.9586	2297.4021
54	51	0.90	7.3082	834.2926	158	77	1.00	7,9602	2301.5924
57	51	0.00	7 2482	880.6422	159	76	1.00	7.0607	2202.0405
60	E0	0.00	7.3808	008.6201	150	75	1.00	7.0611	2306.3430
00	00	0.90	7.3808	908.0391	158	73	1.00	7.9011	2300.2002
63	61	0.90	7.4092	947.9864	158	74	1.00	7.9611	2308.7021
63	60	0.90	7.4128	949.9002	172	83	0.95	7.9675	2503.9047
63	58	0.90	7.4184	954.0710	172	82	0.95	7.9685	2505.8595
63	56	0.90	7.4218	958.7782	172	79	0.95	7.9706	2512.2362
64	53	0.90	7.4320	982.2631	172	77	0.95	7.9711	2517.0146
66	64	0.90	7.4334	987.6190	176	85	0.95	7.9747	2558.1539
66	63	0.90	7.4378	989.3630	176	83	0.95	7.9767	2562.1350
66	62	0.90	7.4416	991.1537	176	82	0.95	7.9776	2564.1353
66	61	0.90	7 4453	993 1286	176	81	0.95	7 9783	2566 2918
66	60	0.00	7 4492	005 1225	170	09	1.00	7.0702	2570 2082
00	50	0.90	7.4403	990.1000	175	50	1.00	1.9192	2570.3582
66	38	0.90	7.4526	999.5030	170	79	0.95	7.9793	2570.6603
66	57	0.90	7.4539	1001.8760	179	96	1.00	7.9838	2572.9970
68	56	0.90	7.4751	1034.8717	179	93	1.00	7.9902	2577.1130
71	66	0.90	7.4815	1058.9385	179	91	1.00	7.9940	2580.1204
73	63	0.90	7.5130	1094.2954	179	85	1.00	8.0032	2590.0586
75	55	0.90	7.5361	1144.4699	179	83	1.00	8.0052	2594.0675
76	56	1.00	7.5938	1144.8285	179	82	1.00	8.0061	2596.0889
80	71	1.00	7.5949	1172.9996	179	81	1.00	8.0068	2598.1710
80	69	1.00	7.6038	1176.0771	179	79	1.00	8,0077	2602,7530
80	64	1.00	7.6205	1184.9753	179	77	1.00	8.0081	2607.5002
80	62	1.00	7 6226	1187 0144	180	81	1.00	8 0121	2641 7159
80	03	1.00	7.0220	1101.5010	102	01	1.00	8.0131	2041.7138
80	61	1.00	7.6258	1191.5313	199	84	1.00	8.0438	2881.7215
80	60	1.00	7.6266	1193.9218	209	77	1.00	8.0597	3044.5114
90	58	1.00	7.6927	1349.0562	229	106	1.00	8.0676	3276.8281
96	71	0.95	7.6962	1414.3063	229	105	1.00	8.0693	3278.3783
96	69	0.95	7.7011	1417.9353	229	98	1.00	8.0801	3288.3865
96	65	0.95	7.7075	1426.4422	229	96	1.00	8.0826	3291.7112
96	64	0.95	7.7082	1428.7395	229	93	1.00	8.0858	3296.9770
96	63	0.95	7.7085	1431.3329	229	83	1.00	8.0902	3318.6674
105	76	0.90	7.7114	1546.0900	232	91	1.00	8.0918	3344.0667
105	75	0.90	7.7144	1547.8077	236	96	1.00	8.0930	3392.3312
105	74	0.90	7.7171	1549.4569	238	98	1.00	8.0937	3417.6244
105	71	0.90	7 7238	1554 9436	238	93	1.00	8 0987	3426 5525
105	66	0.00	7 7208	1566 0259	250	105	1.00	8 1018	2570.0156
105	64	0.90	7.7298	1500.0338	250	105	1.00	8.1018	3579.0150
100	04	0.90	7.7298	1071.2121	200	90	1.00	8.1104	3589.9410
108	67	0.90	7.7438	1608.2930	250	96	1.00	8.1123	3593.5712
111	83	1.00	7.7668	1608.6117	250	81	1.00	8.1146	3628.7305
111	82	1.00	7.7706	1609.8652	277	114	1.00	8.1248	3952.6794
111	79	1.00	7.7812	1613.9977	277	113	1.00	8.1263	3953.9326
111	77	1.00	7.7875	1616.9415	277	106	1.00	8.1355	3963.6742
111	75	1.00	7.7930	1620.1786	277	105	1.00	8.1364	3965.5493
111	74	1.00	7.7955	1621.9363	277	98	1.00	8.1427	3977.6553
111	73	1.00	7.7977	1623.6915	277	96	1.00	8.1438	3981.6769
111	71	1.00	7.8015	1627.5370	277	93	1.00	8.1450	3988.0464
111	69	1.00	7.8042	1631.8070	292	111	1.00	8.1466	4170.7147
111	64	1.00	7.8055	1644.1532	292	106	1.00	8.1521	4178.3136
118	82	1.00	7 8074	1711 3882	292	105	1.00	8 1529	4180 2902
118	77	1.00	7 8210	1718 9109	202	08	1.00	8 1580	4193 0519
110	76	1.00	7.8242	1720.6712	292	30	1.00	0.1000	4107 2012
110	70	1.00	1.8243	1720.0712	292	90	1.00	8.1388	4197.2912
118	74	1.00	(.8285	1/24.2206	292	93	1.00	8.1596	4204.0056
118	64	1.00	7.8339	1747.8385	292	91	1.00	8.1596	4208.9115
143	93	0.90	7.8360	2077.8511	350	143	1.00	8.1613	4959.8613
146	106	1.00	7.8449	2089.1568	350	133	1.00	8.1761	4969.3807
146	105	1.00	7.8489	2090.1451	343	81	1.00	8.1883	4978.6182
143	83	0.90	7.8614	2092.2729	350	119	1.00	8.1930	4986.6821
143	82	0.90	7.8633	2093.9008	350	118	1.00	8.1939	4988.2202
146	100	1.00	7.8677	2094.4486	350	114	1.00	8.1975	4994.3603
146	98	1.00	7.8748	2096.5259	350	113	1.00	8.1984	4995,9437
146	96	1.00	7.8816	2098.6456	350	106	1.00	8.2030	5008.2526
146	93	1.00	7 8012	2102 0028	350	105	1.00	8 2033	5010 6219
1/6	80	1.00	7 0020	2102.0020	350	101	1.00	8 2046	5018 0711
140	09	1.00	7.0170	2100.0791	250	101	1.00	0.2040 9 2050	5025 0102
140	03	1.00	1.91/2	2110.8310	300	98	1.00	0.2000	5120.4001
146	82	1.00	7.9192	2117.4804	359	105	1.00	8.2096	0139.4664
146	79	1.00	7.9242	2122.9159	359	98	1.00	8.2109	5155.1562
146	77	1.00	7.9267	2126.7879	364	98	1.00	8.2140	5226.9550
146	76	1.00	7.9276	2128.9660	379	98	1.00	8.2230	5442.3515
146	75	1.00	7.9284	2131.0457	387	109	1.00	8.2263	5531.9175
146	74	1.00	7.9290	2133.3577	389	106	1.00	8.2287	5566.3150
146	73	1.00	7.9294	2135.6663	I				

TABLE XXIV: Pareto–Optimal Solutions with D=4 for $\sigma=0.3$ and q=0.9

E	M		7711	Deless	F	14		7711	Deless
10	1/1	P	1 11	Delay FEC 1000	1	111	<i>P</i>	10,1400	Delay
43	42	0.30	1.6945	556.4200	270	64	0.55	12.1439	3138.0416
44	42	0.40	1.9839	566.3662	274	66	0.75	12.1719	3160.8198
46	44	0.30	2.0173	573.1780	270	61	0.55	12.1835	3170.9931
48	46	0.30	2.0570	577.6958	288	65	0.45	12.2638	3358.7122
45	42	0.30	2.2419	582.3000	290	65	0.90	12.3041	3376.2918
54	51	0.55	2.4682	584.3526	288	58	0.45	12.3195	3444.0699
68	66	0.90	2.5116	594.1586	308	75	0.90	12.3359	3488.5127
44	39	0.30	2.6756	606.6104	309	75	0.80	12.3521	3498.2727
71	66	0.80	3 2703	612 8076	309	73	0.80	12 /112	3508 6465
95	79	0.00	2.0628	622 6218	200	71	0.80	12.4112	2521 4570
85	10	0.90	3.9028	033.0218	309	71	0.80	12.4023	3521.4579
96	88	0.95	4.3198	649.8116	309	70	0.80	12.4843	3528.9593
82	72	0.55	4.4209	668.7963	309	69	0.80	12.5035	3537.3030
82	71	0.55	4.6129	675.4179	309	68	0.80	12.5196	3546.5906
82	70	0.55	4.7990	682.5016	309	67	0.80	12.5323	3556.9294
73	60	0.55	4.8711	682.7800	309	66	0.80	12.5413	3568.4441
82	69	0.55	4.9832	689.3468	309	65	0.80	12.5461	3581.2693
82	68	0.55	5.1565	697.4123	309	64	0.80	12.5463	3595.5581
82	67	0.55	5.3309	704.7924	328	75	0.80	12.5521	3713.3769
82	66	0.55	5 4999	712 4999	328	72	0.80	12 6291	3730 8286
110	105	0.05	5.5705	720.0621	228	71	0.80	12.6505	2727 0877
107	01	0.00	5.9016	722.6116	220	70	0.00	12.0000	2745 0502
107	76	0.00	6.9996	728 1401	320	10	0.80	10.6950	3743.9303
95	70	0.90	0.2236	728.1491	328	69	0.80	12.0806	3/34.80/0
107	88	0.80	6.2866	741.7578	328	68	0.80	12.6987	3764.6657
107	86	0.80	6.6137	752.4452	328	67	0.80	12.7084	3775.6403
104	82	0.90	6.7303	758.7731	328	66	0.80	12.7142	3787.8630
119	97	0.95	6.8484	767.0926	328	65	0.80	12.7158	3801.4767
96	72	0.95	6.8802	778.9473	337	71	0.80	12.7323	3840.5544
107	82	0.80	7.1620	784.4557	337	70	0.80	12.7499	3848.7356
119	94	0.95	7.2076	795.8840	337	69	0.80	12.7648	3857.8353
119	91	0.95	7.6550	810.6303	337	68	0.80	12.7765	3867.9645
129	99	0.90	7 8561	843 7765	337	67	0.80	12 7848	3879 2402
120	97	0.00	8 1/29	852 2048	337	66	0.80	12 7893	3801 7082
105	70	0.50	0.1420	886 2182	227	65	0.80	12.7000	2005 7856
105	10	0.00	0.1005	880.2183	337	03	0.80	12.7893	3903.7830
119	83	0.95	8.4487	890.0121	337	64	0.55	12.7987	3916.7408
119	82	0.95	8.5680	896.4239	337	61	0.55	12.8018	3957.8692
129	86	0.90	9.2194	947.3741	352	72	0.95	12.8164	4012.4344
146	99	1.00	9.4959	1003.7471	352	71	0.95	12.8287	4022.1635
158	106	0.90	9.7807	1069.4030	352	70	0.95	12.8376	4033.0821
129	71	0.90	9.8320	1152.2513	352	69	0.95	12.8426	4045.3356
129	70	0.90	9.8967	1161.7738	352	68	0.95	12.8433	4059.0850
129	69	0.90	9.9553	1172.0130	358	72	0.70	12.8874	4072.8371
129	68	0.90	10.0072	1183.0291	358	71	0.70	12.9070	4079.8697
129	67	0.90	10.0520	1194.8884	358	70	0.70	12.9245	4087.6294
129	66	0.90	10.0894	1207.6636	358	69	0.70	12.9397	4096.1936
129	65	0.90	10.1189	1221.4370	358	68	0.70	12.9523	4105.6540
146	82	1.00	10 1727	1224 8247	358	67	0.70	12 9620	4116 1075
146	77	1.00	10.5696	1256.6696	358	66	0.70	12.9685	4127.6678
146	75	1.00	10.6072	1272.0074	259	65	0.70	12.0000	4140.4549
140	10	1.00	10.0973	1212.9914	300	71	0.70	12.9710	4140.4048
158	83	0.90	10.8842	1319.9918	368	/1	0.85	12.9769	4196.1210
158	82	0.90	10.9654	1325.0752	368	70	0.85	12.9887	4205.7301
158	80	0.90	11.1184	1336.3175	368	69	0.85	12.9973	4216.4556
178	89	0.90	11.5383	1459.6192	368	68	0.85	13.0025	4228.4293
205	105	0.90	11.5662	1637.4053	368	67	0.85	13.0038	4241.8019
209	105	0.95	11.7683	1667.2308	376	70	0.90	13.0332	4301.7931
260	130	0.65	11.8491	2067.0196	377	70	0.90	13.0401	4313.2340
298	150	1.00	11.9145	2338.8295	381	72	0.90	13.0485	4338.5490
260	68	0.65	11.9418	2982.8238	381	71	0.90	13.0596	4348,1980
260	67	0.65	11,9699	2990.0376	381	70	0.90	13.0676	4358,9978
260	66	0.65	11 9953	2997 9817	382	70	0.90	13 0744	4370 4387
260	65	0.65	12 0177	3006 7222	392	69	0.55	13 0947	1304 1060
200	64	0.00	12.0111	2016 2802	202	66	0.33	19.1960	4415 0122
200	04	0.00	12.0307	3010.3808	383	00	0.70	10.1309	4410.9128
260	61	0.65	12.0704	3051.7311	394	71	0.90	13.1464	4496.5618
267	65	0.70	12.1080	3087.9928	394	70	0.90	13.1530	4507.7300
267	64	0.70	12.1232	3098.5462	394	69	0.90	13.1561	4520.2314
270	65	0.55	12.1242	3128.8859	392	65	0.55	13.1679	4542.6787
267	61	0.70	12.1424	3137.5299					

TABLE XXV: Pareto–Optimal Solutions with D=2 for $\sigma=0.6$ and q=0.1

F	М	20	TH	Delau	F	M	n	TH	Delay
24	222	P	1 4916	E14.0647	146	50	P 1.00	10.0705	1204 2075
34	33	0.85	1.4210	500 5051	140	59	1.00	10.9703	1304.2973
30	34	0.60	1.7352	526.5051	140	38	1.00	10.9879	1317.9969
46	44	0.60	1.9166	545.2758	167	76	0.95	11.1268	1326.9692
48	46	0.60	1.9421	551.6055	167	75	0.95	11.1814	1334.4123
45	42	0.60	2.1434	551.8316	179	85	1.00	11.2423	1346.1325
37	33	0.60	2.2281	556.5068	167	73	0.95	11.2838	1350.1546
54	51	0.60	2.2360	580.5064	179	83	1.00	11.3657	1358.0098
38	32	0.60	2.6662	588.8827	179	81	1.00	11.4825	1370.6911
54	49	0.60	2.6785	595.2342	179	79	1.00	11.5923	1384.2479
48	41	0.60	3.0516	599.4393	179	76	1.00	11.7421	1406.4834
49	40	0.90	3.5575	600.1779	179	75	1.00	11.7878	1414.4449
54	43	0.60	3.8499	650.7778	179	73	1.00	11.8723	1431.3049
60	49	0.60	3.8717	661.3730	179	71	1.00	11.9469	1449.5298
51	39	0.60	3.9826	662.4269	179	70	1.00	11.9802	1459.1964
60	48	0.60	4.0471	670.2267	179	69	1.00	12.0107	1469.2728
55	41	0.60	4 3428	686 8730	179	68	1.00	12 0382	1479 7743
58	13	0.60	4 5214	699.0014	170	67	1.00	12.0625	1490 7464
95	70	0.00	4.7204	701 7200	170	66	1.00	12.0020	1502 1056
00	60	0.90	4.1394	706.6527	175	62	1.00	12.0837	1502.1930
00	69	0.90	4.9072	710.0337	179	50	1.00	12.1201	1539.8031
80	67	0.90	5.2339	717.1723	179	59	1.00	12.1265	1599.1044
85	66	0.90	5.3929	722.7366	219	85	0.95	12.6663	1666.0603
81	61	0.85	5.5325	727.5087	238	97	1.00	12.8389	1712.8771
88	68	0.95	5.5662	728.2892	219	77	0.95	12.9344	1730.7570
85	63	0.90	5.8486	741.0920	238	92	1.00	13.0618	1741.7238
85	61	0.90	6.1348	754.6183	238	91	1.00	13.1030	1748.0006
76	47	0.75	6.5449	827.1522	238	88	1.00	13.2189	1767.9611
74	44	0.80	6.6342	839.7195	238	85	1.00	13.3223	1789.8298
107	76	0.80	6.6519	875.2443	238	83	1.00	13.3837	1805.6220
107	75	0.80	6.7779	880.2251	238	81	1.00	13.4383	1822.4832
107	73	0.80	7.0235	890.7210	238	80	1.00	13.4630	1831.3485
107	71	0.80	7.2523	903.2512	238	79	1.00	13.4859	1840.5084
107	70	0.80	7.3671	909.1713	238	76	1.00	13.5423	1870.0730
107	69	0.80	7.4793	915.3168	238	75	1.00	13.5569	1880.6585
107	68	0.80	7.5888	921.7102	238	73	1.00	13.5790	1903.0758
107	67	0.80	7 6955	928.3600	238	71	1.00	13 5911	1927 3078
107	66	0.80	7 7993	035 2836	238	70	1.00	13 5031	1940 1606
107	65	0.80	7 9002	942 4848	200	92	0.90	13 7096	2046 7010
107	64	0.80	7.0078	050.0058	210	114	1.00	12 7204	2040.1010
107	62	0.80	8.0021	930.0038	230	01	1.00	13.7304	2051.0702
107	60	0.80	8.0921	957.8403	273	91	0.90	13.7362	2034.0220
107	62	0.80	0.1030	900.0370	213	00	0.90	13.8108	2077.2800
107	59	0.80	8.4333	992.9325	273	85	0.90	13.8834	2102.7212
107	58	0.80	8.5087	1002.7651	298	102	1.00	14.1825	2113.1506
107	57	0.80	8.5797	1013.0775	298	97	1.00	14.3364	2144.6949
107	54	0.80	8.7645	1047.3238	298	92	1.00	14.4649	2180.8138
146	91	1.00	8.8521	1058.9123	298	91	1.00	14.4871	2188.6731
146	89	1.00	9.0488	1067.2062	298	88	1.00	14.5463	2213.6656
146	88	1.00	9.1452	1071.5482	298	85	1.00	14.5929	2241.0474
146	85	1.00	9.4255	1085.3893	298	83	1.00	14.6163	2260.8208
146	83	1.00	9.6046	1095.3777	298	82	1.00	14.6255	2271.2025
146	81	1.00	9.7769	1106.0260	298	81	1.00	14.6330	2281.9327
146	79	1.00	9.9420	1117.4055	298	79	1.00	14.6426	2304.5021
146	76	1.00	10.1745	1136.0482	350	115	1.00	14.7705	2404.3906
146	75	1.00	10.2477	1142.7240	350	114	1.00	14.8015	2409.5623
146	73	1.00	10.3869	1156.8429	350	111	1.00	14.8908	2425.7935
146	71	1.00	10.4478	1182.2981	350	97	1.00	15.2190	2518.9369
146	70	1.00	10.5096	1190.1826	350	92	1.00	15.2918	2561.3585
146	69	1.00	10.5685	1198,4013	350	91	1.00	15,3029	2570,5892
146	67	1.00	10.6775	1215.9161	350	88	1.00	15.3285	2599.9428
146	66	1.00	10 7272	1225 2545	350	85	1.00	15 3417	2632 1026
146	64	1.00	10.8162	1245 2332	350	83	1.00	15 3429	2655 3264
170	02	1.00	10.8657	1293 3781	378	01	0.90	15 3737	2844 0312
170	94 01	1.00	10.0007	1209 2555	310	31	0.90	10.0101	2344.0313
119	91	1.00	10.9372	1290.2000	1			1	1 1

TABLE XXVI: Pareto–Optimal Solutions with D=4 for $\sigma=0.6$ and q=0.1

THDelas M $\frac{p}{0.85}$ 17 0.15 5.1943 677.9470 200 80 8.2829 4369.3791 20 24 0.15 26 0.15 $6.3690 \\ 6.5685$ 75 75 $0.85 \\ 0.70$ 8.2871 8.2932 26 28 706.4151 200 4379.0715 736.0641 204 4466.8225 29 28 0.15 6.7033 743.0282 204 68 0.708.29614482.035240 37 0.207.2943 941.9469 214 82 0.858.3034 4671.6492 21453 51 0.85 7.55991196.5166224 88 0.858.3107 4880.1638 55 0.25 67 0.90 224 7.6093 8.3149 4884.83 85 0.85 1302.5578 1496.9358 2244886.450468 7.722484 0.85 8.31614889.9506 7.7804 7.8287 $\frac{1532.5876}{1643.6447}$ 224 224 82 81 58 0.85 58 0.85 $0.85 \\ 0.85$ 8.3182 8.3191 69 74 4891.8280 80 75 82 68 0.557.86491802.9216 224 0.858.3199 4893.704682 66 0.55 7.8783 1804.7541 2240.85 8.3217 4904.5601 82 65 0.55 7.8847 7.8909 1805.7568230 74 0.908.32715039.759082 64 0.55 1806.7762 234 85 0.90 8.3291 5102.757 82 62 0.55 7.90241809.0732 23484 0.90 8.33005104.585882 58 0.557.9213 1814.5766234 83 0.90 8.3308 5106.427453 0.55 1824.2790 5108.3918 7.9333 23482 8.3315 0.90 88 65 0.70 7.93411937.0619 23480 0.90 8.33245112.655564 0.70 62 0.70 7.9386 7.9465 234 239 8.3324 8.3388 5124.5646 5224.0960 1938.4304 75 79 0.90 88 88 1941.4039 88
 59
 0.70

 56
 0.70
 7.95501946.7797 1953.5747 242 242 85 82 $0.85 \\ 0.85$ 8.3393 8.3417 5277.3690 5282.8930 7.9578 88 96 65 0.957.9675 2118.6615242 80 0.858.3428 5286.948796 62 0.95 7.9686 2125.8633 24275 0.85 8.3432 5298.6766 10577 0.60 75 0.60 0.60 7.97882298.9690247 85 84 0.90 8.34565386.2442105 7.9898 2300.5876 247 0.90 8.3463 5388.1739 105 74 0.60 7.99512301.4619 24783 0.90 8.34695390.1179105 68 0.60 8.0241 2307.6132247 82 0.90 8.3474 5392.1914105 105 67 0.60 8.0283 8.0361 2308.8115 80 0.90 8.3479 8.3503 5396.691965 0.60 2311.461624875 0.80 5429.5861251 105 64 0.60 8.0396 2312.8672 2315.9792 84 0.85 8.3510 5475.4422 5477.3298 251 8.3517 105 62 0.60 8.0457 83 0.8510! $251 \\ 251$ 82 81 $0.85 \\ 0.85$ 5479 3643 59 0.60 8 0522 2321105 58 0.60 8.0535 2323.5155 8.3526 5481.4679 105 $\frac{56}{65}$ 0.60 8.0543 2328.254525180 75 $0.85 \\ 0.85$ 8.35308.35375483.5708 5517.6301 115 8.0742 2534.2636 252 117 65 0.90 8.0774 2580.017925475 0.708.35555561.6319119 58 0.55 8.1088 2633.3502 260 75 0.65 8.3594 5694.4639 126 68 0.85 8.11372770.2611263 84 0.858.36415737.216367 126 0.858.1150 2772.2763263 81 0.90 8.3650 5743.8216 2776.6715 5800.744512665 0.85 8.1164 26685 0.85 8.3666 144 80 0.60 8.13943149.7662266 84 0.858.3673 5802.65990.85 1.00 14682 8.1470 3188.1705 266 83 8.3678 5804.6602 79 1.00 5806.8163146 8.1540 3192.6242 266 82 0.858.3681
 77
 1.00
 8.1579
 3195.8998

 75
 1.00
 8.1610
 3199.5161
 81 80 0.85 5809.0457 5811.2742 146 146 266 266 8.3683 8.3685 147 146 79 68 0.85 8.1612 8.1635 3212.8265 3215.6246 276 276 88 85 0.90 8.37548.37696012.6248 6018.6373 75 0.85 75 0.90 8.1707 8.1721 276 282 0.90 8.3775 8.3823 6025.2827 6168.7003 147 3218.6158 82 77 148 3241.1758 75 148 68 0.90 8.1789 3255.4467287 0.708.3848 6284.20628.1839 153 77 0.75 3346.8969 289 82 0.758.3876 6310.2447152 153 65 0.85 68 0.75 8.1919 3349.6370291750.85 8.3881 8.3922 6371.54918.1999 3361.9060 293 81 6399.01041530.75 8.2007 3363.9963 299 0.85 8.3971 6520.385 299 153 65 0.75 8.2012 3368.6732 82 0.858.39756527.21083471.6448 6710.0263 8.212330888 1.00 8.4036158 67 0.65 8.2134 3473.5767 0.856753.7982310 88 8.40506760.2661 6762.4983 3477.7798 3484.9573 8.4058 8.4060 158 158 65 62 0.65 8.2149 8.2151 310 310 85 84 0.85 173 85 0.90 8.21843772.5516310 83 85 0.85 8.4060 6764.8296173 84 8.2206 8.2228 3773.9033 312 0.85 8.4074 6803.8807 17383 0.90 377 5.2647318 85 0.85 8.4118 6934.7246 173 82 0.90 8.22483776.7170 318 84 0.858.4119 6937.014417380 0.90 8.22843779.869232885 0.858.41887152.7970.70173 79 0.90 8.23013781.4586340 85 8.42197419.0439 173 173 77 0.90 75 0.90 8.2329 8.2351 340 340 0.70 7421.06477425.84563784.921684 8.42223788.6738 82 8.4222 173 68 0.90 8.2358 3805 3533 349 0.85 8.4314 7618,7176 82 7803.3899 3908.7866 359 179 82 1.00 8.236396 0.90 8.4375179 180 1.00 8.2425 8.2520 3922.6965 3940.7869 359 367 85 96 0.90 8.43848.44127828.58987978.616075 75 183 183 0.85 0.85 0.90 8.44508.445075 8.25714006.8505 371 371 96 8064.2274 8090.2697 68 8.25784023.4765 85 8.2612 4073.3718 37 8186.3012 186 0.90 82 0.85 8.445 196 75 1.00 8.27384295.2431392 85 0.708 4505 8553 7212 397 20085 0.85 82 0.85 8.27554361.462096 0.858.45838630.8189 8.2803 4366.0273 200

TABLE XXVII: Pareto–Optimal Solutions with D = 2 for σ = 0.6 and q = 0.9

THTH0.05 1.3427 671.7824 146 95 1.00 8.0256 3012.2217 0.55 6.0748 0.95 6.2403 93 89 1.00 8.0331 3014.0237 8.0472 3018.0662 26761.5336 146 2831 30 814.7712 146 33 32 0.80 6.5914 816.1951 146 87 1.00 8.0536 3020.3783 37 34 0.956.7351899.1289 146 85 1.00 8.0597 3022.675251 49 0.95 7.4204 1106.5099146 81 1.00 8.0702 3028.22567.4299 7.5299 8.0725 3029.6612 8.0809 3038.5602 56 46 14680 0.80 1234.2463 1380.5150 1.00 63 47 0.85146 1.00 0.80 7.6003 0.80 7.6062 1494.7662 1496.1068 146 146 74 70 1.00 8.0821 3040.3956 8.0837 3049.7202 70 $\frac{71}{71}$ 69 7168 0.807.61191497.5212 166 81 0.858.0901 3460.850967 0.80 7.6171 1498.9445 166 $\frac{1}{76}$ 0.85 8.0950 3470.9141 66 7.62201500.5253176 96 0.958.1080 3635.2117710.8071 65 0.80 7.6265 1502.1638 176 92 0.95 8.1188 3639.6273 71 64 0.80 7.6305 1503.8537 17689 0.95 8.12603643.3084 71 63 0.80 7.6341 1505.6735176 85 0.958.1341 3649.1331 1507.635462 7.6373 176 0.95 0.80 80 8.1415 71 60 0.80 7.64181511.8223176 76 0.958.1444 3666.0849
 0.80
 7.6438
 1516.5809

 0.95
 7.6892
 1625.7271
 176 179 0.95 8.1447 3668.3073 8.1515 3705.8827 75 85 58 75 78
 8.1575
 3712.6875

 8.1588
 3714.4476
 78 70
 0.95
 7.7183
 1631.7317

 0.95
 7.7234
 1633.1942
 179 179 81 1.00 69 80 7878 68 0.957.72791634.6080179 76 1.008.1614 3722.955378 67 0.95 7.7322 1636.2248 179 75 1.00 8.1616 3725.3580 78 66 0.957.7360 1637.8374194 89 $0.95 \\ 0.95$ 8.1662 4015.9195 8.1724 4022.3399 78 65 0.95 7.7395 1639.6100 194 85 7864 0.957.7426 1641.5353 194 80 0.95 8.1775 4031.6733 78 63 0.957.7450 1643.5272194 75 0.958.1783 4043.4751 78 61 0.957.7484 7.7491 1647.90151980.95 8.1850 8.1857 4126.84 4126.8458
4300.2009 78 60 0.951650.2750208 93 84 63 7.7492 1781.3602 208 208 89 0.95 8.1926 4305.7281 89 71 0.80 7.7648 1872.232585 0.95 8.1976 4312.6119 0.95 89 70 7.7684 208 4320 6645 1873 721081 89 69 0.80 7.7719 1875.4015 208 80 0.95 8.2012 4322.6188 0.80 89 $\frac{68}{67}$ 7.7749 1877.1744 238 238 1.004890.3772 114 8.2027 8.2188 89 1878.9586 107 1.00 4896.6556 89 66 0.807.7800 1880.9401 238 106 1.00 8.2212 4897.3054 4898.5349 89 65 0.80 7.7819 1882.9940 238 105 1.00 8.2231 89 60 0.80 7.78451895.1012 238104 1.00 8.22524899.6469 0.80 4909.1041 91 67 7.7915 1921.1824 238 96 1.00 8.2399 8.2444 4913.2715 96 83 0.957.80191992.216323893 1.00 96 76 0.957.83821999.6826 238 89 1.00 8.24914919.8613 0.95 8.2523 75 96 7.8426 2000.8949 238 85 1.00 4927.3747 748.2534 4936.4225 2002.2370 238 96 0.957.846881 1.0096 96 80 89 1.00 8.2534 4938.7628 8.2601 5278.6571 72 71 238 255 70 69 0.95 7.8610 7.8639 2008.28522010.0852255 286 85 80 0.95 8.2620 8.2632 5287.0963 5965.9746 96 96 96 96 68 67 0.95 7.8663 7.8685 2011.8253 2013.8151 292 292 114 107 1.00 8.2790 5999.9586 8.2903 6007.6614 96 66 0.957.8702 2015.7999 292 106 1.00 8.29216008.4587 96 65 0.957.8715 2017.9816292 105 1.00 8.2933 6009.9672 96 64 62 0.957.8723 7.8724 2020.3512 2025.3530 29296 1.008.3039 6022.9345 8.3056 6026.3610 292 96 0.9594 1.00
 7.8780
 2250.8862

 7.8800
 2252.6759
 292 292 107 0.80 93 1.00 8.3064 6028.0473 70 107 0.8089 1.008.3084 6036.1324 6045.350 292 311 10' 69 85 1.00 93 107 0.95 8.3126 6429.6273 68 7.88427.88482258.9727 2261.3550 8.3191 8.3195 107 67 66 0.80 319 333 85 107 0.95 6614.0538 6860.0816 107 65 0.80 7.88512263.8243 333 106 0.95 8.3206 6861.4376 112 69 0.95 7.9509 2345.0994 333 105 0.95 8.3218 6862.6680 2444.6034 6877 7.9519 117 740.90 333 96 0.95 8.3286 .98 117 73 0.90 7.95422446.2270333 93 0.958.3295 6884.4562117 710.90 7.9579 7.9594 2449.9849333 89 0.958.3301 8.3371 6893.3051 117 70 0.90 2452.0870344 93 0.957111.8707 7.9605 350 350 117 117 2454.2291 2456.3459 1.00 7200.9640 7201.9197 690.90 107 8.342668 8.3438 0.90 106 117 67 0.90 7.9617 2458.822 350 10 1.00 8.3446 7203 7278 7.9617 2461.2168 350 8.3507 7219.2708 11766 1.00 0.90 - 96 118 119 68 70 $0.95 \\ 0.95$ $7.9782 \\ 7.9806$ 2472.86862489.4368 $350 \\ 380$ 93 107 1.00 8.3517 8.3537 7225.3992 7828.3213
 0.95
 8.0128
 2661.4772

 0.85
 8.0199
 2960.4869
 0.95 8.35448.3553127 68 81 380 380 106 7829.8687 105 7831 2727 3011.4672 380 7848.7525 146 96 1.00 8.0217 96 0.95 8.3592

TABLE XXVIII: Pareto–Optimal Solutions with D = 4 for σ = 0.6 and q = 0.9

F	М		ΤU	Delaw	F	M	~	TU	Delaw
1.	101	P	1 11	COO DOOT	1.	111	<i>p</i>	10.0150	Deluy
44	43	0.25	1.7017	600.8897	260	65	0.65	12.0159	3223.8894
57	56	0.55	2.0544	614.0245	260	64	0.65	12.0324	3234.2510
60	59	0.55	2.1288	618.2430	260	63	0.65	12.0448	3245.7228
40	36	0.30	2.3483	627.2699	260	61	0.65	12.0558	3272.4985
59	54	0.30	2.9577	673.7504	267	63	0.65	12.1329	3333.1076
91	89	0.95	2.9873	684.2659	276	68	0.65	12.1588	3395.2317
97	95	0.95	3.0863	696.7224	279	68	0.65	12,1961	3432.1364
96	03	0.95	3 2905	699 6015	280	68	0.65	12 2083	3444 4380
80	75	0.55	2 8645	700 4152	200	65	0.65	12.2000	2450 4912
01	15	0.35	3.8043	709.4132	219	03	0.05	12.2000	3439.4813
91	84	0.95	4.0488	713.2210	279	04	0.65	12.2030	3470.0001
96	86	0.95	4.7126	741.3697	279	63	0.65	12.2736	3482.9102
82	70	0.55	4.8434	743.5710	280	63	0.65	12.2848	3495.3938
96	85	0.95	4.8959	748.5847	288	65	0.45	12.2982	3588.2408
96	84	0.95	5.0777	755.5158	288	64	0.45	12.3150	3597.7771
82	67	0.55	5.3678	767.5174	288	63	0.45	12.3290	3608.1371
96	82	0.95	5.4126	772.3125	288	58	0.45	12.3474	3675.4129
102	87	0.95	5 6738	784 4173	304	71	0.55	12 3880	3724 0508
102	65	0.55	5.6799	786 6272	204	70	0.55	12.0005	2720.2511
02	05	0.35	5.0788	780.0372	304	10	0.55	12.4100	3730.2311
90	80	0.95	5.7418	181.9804	304	08	0.55	12.4626	3744.4304
110	94	0.95	5.9247	802.4320	304	65	0.55	12.5152	3771.2317
110	93	0.95	6.0951	807.9929	304	64	0.55	12.5269	3781.9350
96	75	0.95	6.4178	840.1570	304	63	0.55	12.5352	3793.6869
82	58	0.55	6.5882	863.6424	311	65	0.55	12.5823	3858.0693
110	86	0.95	7.0674	867.5393	311	64	0.55	12.5928	3869.0190
107	82	0.80	7.1944	869.4495	311	63	0.55	12.5999	3881.0415
110	84	0.95	7 3467	881 4777	324	71	0.65	12 6134	3962 1920
110	82	0.05	7.4028	022.0120	224	70	0.65	12.6254	2060.2646
110	80	0.95	7.4028	923.0120	324	10	0.05	12.0334	3909.2040
110	80	0.95	7.0578	937.4323	324	00	0.65	12.0721	3985.7008
117	86	0.95	7.8110	955.4556	326	68	0.55	12.6746	4015.4303
105	70	0.60	8.2309	968.0403	324	65	0.65	12.7050	4017.4622
113	78	0.65	8.2870	976.4386	324	64	0.65	12.7088	4030.3743
117	82	0.95	8.3057	981.7492	326	65	0.55	12.7164	4044.1498
120	84	0.65	8.3735	1000.4928	326	64	0.55	12.7245	4055.6276
120	82	0.65	8.6229	1011.5636	326	63	0.55	12.7292	4068.2300
120	80	0.65	8.8588	1023.6668	331	68	0.65	12.7345	4071.8178
123	82	0.65	8.9589	1036.8527	333	68	0.65	12.7518	4096.4209
144	100	0.65	9.0117	1126 4429	331	65	0.65	12 7642	4104 2592
120	71	0.65	0.1272	1167 0522	221	64	0.65	12.7660	4117 4502
120	71	0.05	9.1372	1107.9000	222	04	0.05	12.7009	4117.4505
120	70	0.05	9.2280	1175.2921	333	05	0.65	12.7800	4129.0384
158	111	0.90	9.2531	1176.7974	333	64	0.65	12.7831	4142.3292
119	68	0.55	9.2896	1184.8956	341	70	0.65	12.7874	4177.5285
120	68	0.65	9.3970	1191.4604	345	70	0.55	12.8012	4233.3442
123	70	0.65	9.4774	1204.6744	345	68	0.55	12.8359	4249.4585
119	65	0.55	9.5287	1210.3456	345	65	0.55	12.8696	4279.8518
119	64	0.55	9.5980	1219.9356	345	64	0.55	12.8749	4291.9986
120	65	0.65	9.6090	1220.0482	345	63	0.55	12.8768	4305.3354
123	68	0.65	9.6356	1221.2469	352	70	0.65	12.8780	4312.2875
119	63	0.55	9.6615	1230.1494	351	68	0.65	12,8991	4317.8491
120	64	0.65	9.6676	1230 9135	352	68	0.65	12 9068	4330 1506
162	100	0.65	9.6941	1238 6966	350	67	0.65	12.0000	4340 5191
102	109	0.05	9.0341	1238.0800	352	07	0.05	12.9170	4340.3131
120	03	0.65	9.7195	1242.5390	301	00	0.65	12.9203	4352.2507
123	65	0.65	9.8319	1250.5494	352	65	0.65	12.9277	4364.6503
123	64	0.65	9.8852	1261.6864	363	71	0.65	12.9463	4439.1225
130	71	0.65	9.9377	1265.2827	363	70	0.65	12.9630	4447.0465
130	70	0.65	10.0132	1273.2331	363	68	0.65	12.9891	4465.4678
130	68	0.65	10.1494	1290.7488	363	65	0.65	13.0057	4501.0456
130	65	0.65	10.3121	1321.7189	368	68	0.65	13.0249	4526.9757
142	75	0.95	10.3989	1361.8485	368	65	0.65	13.0397	4563.0435
144	75	0.65	10.5999	1371.4073	382	71	0.90	13.0418	4687,1731
146	75	1.00	10.6147	1406 0819	382	70	0.00	13 0452	4699 6649
140	10	0.05	10.0147	1491 5140	200	75	0.50	12 0562	4720 2406
100	0Z	0.95	10.7620	1431.3148	389	10	0.05	10.1010	4730.3406
152	76	0.65	11.0231	1440.8067	389	71	0.65	13.1312	4757.0762
160	82	0.70	11.0631	1478.3410	389	70	0.65	13.1450	4765.5677
197	99	0.65	11.6124	1759.8632	389	68	0.65	13.1652	4785.3085
219	111	0.95	11.7534	1917.1502	389	65	0.65	13.1728	4823.4346
230	115	0.95	11.9104	2009.2016	399	63	0.65	13.2151	4980.9361
363	182	0.65	11.9459	3153.5321					

TABLE XXIX: Pareto–Optimal Solutions with D = 2 for σ = 0.8 and q = 0.1

F	M	n	TH	Delay	F	M	n	TH	Delay
-		P	1 11	Derag	-		P	1 11	Detag
28	26	0.55	1.4831	592.3037	205	85	0.95	13.0779	1760.1407
E 4	E 1	0.75	9 2048	622 4622	205	80	0.05	12 0520	1802 0625
34	31	0.75	2.3948	022.4023	205	80	0.95	13.2032	1802.0625
53	49	0.75	2.6137	628.0454	205	79	0.95	13.2816	1811.3291
4.1	0.5	0.75	0.7500	647 0691	0.05		0.05	10.0007	1051 0049
41	35	0.75	2.7582	647.8631	205	75	0.95	13.3697	1851.8843
48	41	0.75	3 1639	653 6783	226	96	0.95	13 3785	1860 9366
10		0.10	0.1000	500.0100	220	50	0.00	10.0100	1000.0000
60	49	0.75	4.1245	710.9943	205	74	0.95	13.3849	1862.9950
69	40	0.75	4 6600	746 5570	207	75	0.05	19 4991	1860 0514
03	49	0.75	4.0092	740.5570	207	75	0.95	15.4551	1809.9314
77	63	0.95	4.8990	751.7379	226	94	0.95	13.4695	1873.5628
77	60	0.05	F 4000	774 0010	000	0.0	0.05	10 5100	1000 1407
77	60	0.95	5.4033	774.3313	226	93	0.95	13.5128	1880.1487
88	69	0.95	5 72/13	816 9058	238	104	1.00	13 5450	1894 1442
00	05	0.50	0.1240	010.5000	200	104	1.00	10.0400	1054.1442
77	54	0.95	6.2567	830.8322	226	90	0.95	13.6337	1901.0776
05	70	0.05	6 3053	869.0291	226	80	0.05	12 6708	1008 4725
95	12	0.95	0.3033	802.9521	220	- 69	0.95	13.0708	1908.4725
95	70	0.95	6.5928	875.7549	226	86	0.95	13.7715	1932.0813
		0.00					0.00		
88	58	0.95	7.2075	905.4007	226	85	0.95	13.8014	1940.4478
05	62	0.05	7 4702	020 1747	226	02	0.05	12 9552	1058 0222
90	03	0.95	1.4194	929.1141	220	83	0.93	13.8002	1938.0223
95	58	0.95	7.9819	977.4213	226	82	0.95	13.8790	1967.2461
100	0.0	0.05	0.0000	1011 5505	000	0.0	0.05	19.0100	1000 0040
122	04	0.95	0.2022	1044.7505	220	80	0.95	13.9199	1980.0040
122	79	0.95	8.5780	1064.7536	226	79	0.95	13.9369	1996.8799
		0.00					0.00		
122	75	0.95	8.9943	1089.8792	237	89	0.95	14.0192	2001.3627
122	73	0.95	0 1853	1103 8672	237	85	0.95	1/ 1202	2034 8944
122	10	0.00	0.1000	1100.0012	201	00	0.00	17.1202	2004.0044
139	85	0.95	9.4995	1176.8557	257	96	0.95	14.3772	2116.1978
140	OF	0.05	0 5896	1105 2002	957	0.4	0.05	14 4415	9120 FFF0
140	00	0.95	9.0820	1100.3223	201	94	0.95	14.4410	∠130.3339
140	84	0.95	9.6774	1190.9345	257	93	0.95	14,4716	2138.0452
100	0.0	0.00	0.0000	1100.0550	057	000	0.07	14 5501	0101 0110
122	63	0.95	9.9296	1193.2559	257	90	0.95	14.5524	2161.8449
139	80	0.95	9 9586	1206 5658	257	89	0.95	14 5761	2170 2541
105		0.90	0.0000	1200.0000	201		0.90	14.0701	2110.2041
139	79	0.95	10.0435	1213.1209	257	88	0.95	14.5981	2178.9350
140	90	1.00	10.0564	1010 0000	957	90	0.05	14 6967	9107 1019
140	00	1.00	10.0304	1410.3083	401	00	0.95	14.0307	4191.1013
140	79	0.95	10.1186	1221.8484	257	85	0.95	14.6533	2206.6155
100		0.00	10.2525	1041 5452	057	00	0.07	14.0005	0007 0000
139	75	0.95	10.3567	1241.7476	257	82	0.95	14.6907	2237.0896
146	82	1.00	10/4022	1242 1694	257	79	0.95	14 7085	2270 7882
140	02	1.00	10.4022	1242.1034	201	10	0.50	14.1000	2210.1002
140	75	0.95	10.4266	1250.6810	267	85	0.95	14.8859	2292.4760
100	77.0	0.05	10,1009	1057 0040	0.07	0.4	0.05	14.0000	0000 0050
139	13	0.95	10.4963	1257.0848	267	84	0.95	14.8968	2302.6859
146	79	1.00	10 6374	1262 2411	296	107	0.95	15 0343	2360 5990
110	10	1.00	10.0011	1202.2111	200	101	0.00	10.0010	2000.0000
144	75	0.95	10.6962	1286.4148	296	100	0.95	15.2431	2406.8641
146	75	1.00	10.0141	1202 5080	206	06	0.05	15 2266	9497 9998
140	15	1.00	10.9141	1292.3080	290	90	0.93	10.000	2431.3328
146	74	1.00	10.9760	1300.7959	296	94	0.95	15.3753	2453.8698
1.4.0	77.0	1.00	11.09.49	1000 1007	2000	0.0	0.05	15 0005	0460 4055
140	13	1.00	11.0348	1309.4027	296	93	0.95	15.3925	2462.4957
146	71	1.00	11.0402	1341.2956	296	90	0.95	15.4348	2489.9070
4.4.0		4.00	44.004.8	1050.0000	200	0.0	0.00		2100.0010
146	70	1.00	11.0915	1350.6393	296	89	0.95	15.4457	2499.5922
144	64	0.95	11 1442	1406 5761	316	108	0.95	15 4644	2513 7287
111	01	0.00	11.1112	1100.0101	010	100	0.00	10.1011	2010.1201
172	93	0.95	11.1766	1408.0888	316	107	0.95	15.4931	2520.0989
146	64	1.00	11 2107	1415 0757	916	106	0.05	15 5908	2526 6276
140	04	1.00	11.3197	1415.8757	310	100	0.95	15.5208	2520.0570
172	90	0.95	11.3975	1424.8373	323	111	0.95	15.5268	2550.7311
170	0.0	0.05	11 1070	1490 7415	010	0.0	0.05	15 (001	0550 (101
112	- 69	0.95	11.4078	1430.7415	310	90	0.95	15.0221	2002.0121
179	96	1.00	11.4786	1434 4314	310	94	0.95	15.6532	2569 9312
110	00	1.00	11.1100	1101.1011	010	01	0.00	10.0002	2000.0012
172	88	0.95	11.5363	1436.8343	310	93	0.95	15.6665	2578.9651
179	94	1.00	11.6260	1444 9506	316	96	0.95	15,7367	2602 0175
110	01	1.00	11.0200	11110000	010	00	0.00	10.1001	2002.0110
172	86	0.95	11.6676	1449.5863	316	94	0.95	15.7647	2619.6718
170	0.2	1.00	11 6079	1450 4454	916	0.2	0.05	15 7765	3638 880F
179	93	1.00	11.0972	1430.4434	310	93	0.95	15.7705	2028.8803
179	90	1.00	11.9013	1467.8828	316	90	0.95	15.8029	2658.1439
170	00	1.00	11.0000	1515 0515	910	80	0.05	15 0004	0669 4000
179	80	1.00	11.9893	1010.8010	310	89	0.95	10.8084	∠008.4836
179	85	1.00	12.0483	1522.4868	316	88	0.95	15.8122	2679.1575
170	0.4	1.00	10 1050	1500.0500	2000	0.0	0.05	15 0101	0004.0500
179	84	1.00	12.1052	1929.3569	326	96	0.95	15.9184	2084.3598
179	83	1.00	12.1601	1536,4503	326	94	0.95	15.9415	2702.5729
1 70	0.0	1.00	10.0100	1540 5500	0.10	1.07	0.05	10.0255	0705 1000
179	82	1.00	12.2128	1543.7798	343	107	0.95	16.0277	2735.4238
179	80	1.00	12.3114	1559.2258	349	111	0.95	16.0448	2756 0532
1.0		1.00	10.0114	1500.2200	010	4.6-	0.00	10.0110	2700.0002
179	79	1.00	12.3571	1567.3602	349	107	0.95	16.1352	2783.2738
170	75	1.00	12 51/1	1602 0802	3/10	106	0.95	16 1555	2700 /052
119	10	1.00	12.0141	1002.9093	345	100	0.95	10.1000	2120.4200
179	74	1.00	12.5463	1612.7660	345	100	0.95	16.1889	2805.2977
170	79	1.00	19 5755	1622.0150	250	106	0.05	16 2242	2022 4701
119	10	1.00	12.0700	1022.9100	303	100	0.95	10.2243	2022.4101
179	72	1.00	12.6015	1633.4845	349	100	0.95	16.2544	2837.8229
100		0.05	10.0450	1001 4105	9.40		0.05	10.0002	0050 5450
189	80	0.95	12.6458	1661.4137	349	96	0.95	16.2966	2873.7472
189	79	0.95	12.6845	1669.9571	349	94	0.95	16.3097	2893.2452
100		0.00	12.0010	1000.0011	545		0.00	10.0001	2000.2402
191	80	0.95	12.7273	1678.9948	349	93	0.95	16.3140	2903.4155
102	80	0.05	12 7992	1670 0022	350	02	0.05	16 2227	2011 7247
190	04	0.90	12.1200	1019.9999	330	53	0.90	10.3201	4911.1341
191	79	0.95	12.7646	1687.6286	369	107	0.95	16.4685	2942.7737
109	00	0.05	19 9071	1606 5750	204	110	0.05	16 5911	2008 7110
193	0U	0.95	14.00/1	1090.9198	384	110	0.95	10.0311	2990./110
189	75	0.95	12.8141	1707.3469	384	113	0.95	16.5937	3018.4873
100		0.00	10.0007	1818 5005	001	10	0.00	10.0057	0000 0005
189	74	0.95	12.8397	1717.5905	384	107	0.95	16.6957	3062.3987
205	90	0.95	12.8536	1724 4988	384	106	0.95	16 7094	3070 3444
200	20	0.90	12.0000	1127.4200	004	100	0.90	10.1034	0010.0444
191	75	0.95	12.8886	1725.4141	399	116	0.95	16.7632	3115.8488
0.05	00	0.05	10.0000	1791 1905	204	100	0.05	16 7000	9100 4100
205	89	0.95	12.9020	1/31.1365	384	100	0.95	10.7692	3122.4183
191	74	0.95	12,9128	1735.7661	384	96	0.95	16.7854	3161 9453
101		0.00	12.0120	1100.1001	004		0.00	10.1004	0101.0100
205	88	0.95	12.9487	1738.0610	399	107	0.95	16.9058	3182.0236
102	75	0.05	12 0616	17/3 /019	300	106	0.05	16 0170	3100 2707
190	10	0.90	14.9010	1140.4010	399	100	0.95	10.9170	3130.2191
205	86	0.95	13.0367	1752.5517	399	96	0.95	16.9686	3285.4588

TABLE XXX: Pareto–Optimal Solutions with D=4 for $\sigma=0.8$ and q=0.1

THDela Mp 0.95 TH20 0.15 5.3964 664.5433 176 75 8.2370 4003.2917 18 0.15 6.6434 0.15 6.7201 $0.95 \\ 1.00$ 8.2372 4005.6578 8.2394 4071.0091 27747.6567 176 74 2829 28 765.2599 179 76 36 34 0.157.0618 905.2943 179751.00 8.2396 4073.2941 40 37 0.207.3080 973.4298 180 82 0.80 8.2408 4079.5380 43 7.466481 8.2504 59 54 0.15 7.4677 1406.0278180 76 0.80 4089.1666 528.2516 4090.9850 8.2524 4093.0505 1409.5849 180 0.80 0.1559 51 0.157.48061411.5584180 74 0.80 0.15 7.4836 0.15 7.4872 1413.64761418.2790 70 76
 8.2542
 4101.8341

 8.2591
 4227.0327
 59 50180 0.80 0.90 186 59 48 59 47 0.157.48781420.8607 191 82 0.808.26354328.843161 54 0.15 7.4923 1453.6898 193 82 0.85 8.2673 4374.1135 61 527.50051457.3674193 0.858.2688 4375.70450.1581 61 51 0.15 7.5038 1459.4079 193 76 0.85 8.2738 4385.1256 61 48 0.157.5090 1466.3563 193 74 0.858.27464389.4975 63 52 0.857.6817 1473.3629206 83 0.658.2839 4670.0944 8.2882 4686.41 7.7678 1797.7916 0.85 47 0.7585 82 78 0.557.79121863.6665207 82 0.858.2921 4691.4067 76 75
 0.55
 7.8073
 1864.8762

 0.55
 7.8152
 1865.5293
 207 207 81 76 0.85 8.2933 4693.1132 8.2967 4703.2176 82 82 74 70
 0.55
 7.8230
 1866.2081

 0.55
 7.8527
 1869.1900
 207 74 0.85 8.2970 4707.9066 8.3079 4918.0447 4707 9066 217 82 82 82 67 0.557.8734 1871.7928 219 82 0.80 8.3108 4963.4379 82 65 0.55 7.8862 1873.7696 219 81 0.80 8.3119 4965.1306 8.3152 8.3154 82 62 $0.55 \\ 0.55$ 7.90341877.1343219 76 $0.80 \\ 0.80$ 4975.152682 59 7.9177 1881.2530 219 74 4979.8781 82 580.557.9217 1882.8535 22482 0.858.3181 5076.6913 82 56 0.557.9279 1886.3770 224 81 0.858.3189 5078.5379224 228 82 $\frac{54}{52}$ $0.55 \\ 0.55$ 1890.5226760.858.3207 5089.4721 82 7.93171895.533082 0.80 8.3236 5167.4148 96 74 70 0.95 7.9360 2184.9031 228 228 81 0.80 8.3245 5169.1771 96 0.957.9513 2190.6620 76 0.80 8.3270 5179.6110 96 229 0 220 68 7 9569 2194 0694 76 0.95 7.9591 2195.9599 96 67 231 76 0.80 8.3307 5247.7637 96 65 $0.95 \\ 0.80$ 7.96202200.1892 $236 \\ 243$ 0.80 8.33678.34045363.7359 7597 62 7.9915 2223.8903 85 5501.7137 10575 0.607.99152387.6223 24382 0.808.34285507.3763 105 74 0.60 7.9968 2388.4497 243 81 0.80 8.3435 5509.2545 105 70 0.60 8.0164 2392.4961 24376 0.80 8.34475520.37480.60 8.0252 5614.9177 105 68 2394.7789248 85 0.80 8.3465 2396.0495105 67 0.608.0292 24882 0.80 8.34865620.6968 105 65 0.608.0368 2398.706924881 0.80 8.3493 5622.61370.60 8.0528 8.3502 105 582411.2470 248 76 0.80 5633.9628 255 8.35650.80 8.0618 2602.9643 5779.3455 113 5882 0.80 74 70 255 258 76 85 0.80 119 119 8.3574 5792.9860 8.3580 5841.3257 119 119 68 67 $0.55 \\ 0.55$ 8.0878 8.0912 2715.0759 2716.3824 258 258 0.80 8.3597 8.3604 5847.3378 5861.1387 82 76 119 119 65 62 $\frac{260}{262}$ 0.65 8.3606 8.3639 76 5907.8372 75 5954.6560 119 26785 0.708.36446047.3935 58 0.80 129 75 8.1097 2931.871126876 0.80 8.3699 6088.3146 12974 70
 0.80
 8.1126
 2933.3513

 0.80
 8.1221
 2939.6463
 27677 0.808.3773 6267.4063 8.3831 6407.3456 85 129 2830.80 2945.2916 2949.7176 283 283 129 67 0.80 8.1267 0.80 8.3839 6413.9402 129 65 0.80 8.1281 81 0.80 8.3841 6416.1277 8.3849 6452.6272 8.3857 6459.2684 285 285 131 85 65 82 131 0.803054.65743061.01908.3859 8.3884 134 134 70 67 0.85 0.85 8.1368 8.1394 285 289 81 82 0.80 6461.4714 6550.4506 $144 \\ 144$ 81 0.858.14553264.7725 302 91 0.80 8.3962 6826.0297 75 0.85 8.1605 3273.4292 302 82 0.80 8.3997 6844.5581 3287.057 7138.8415 14468 0.858.1690 316 93 0.80 8.406415685 0.858.1722 3531.7909 328 75 0.80 8.41357454.6838 15682 0.85 8.1803 3535.5509 0.85 8.1829 3536.8369 333 85 0.808.42217539.38547652.5894 15681 338 85 0.80 8.42547771.3970 7788.4342 156 156 76 74 3544.4538 3547.9876 $\frac{344}{344}$ 8.4272 0.858.1933 93 0.80 8.4292 0.858.196485 0.80 70 75 8.2000 156 0.85 3556.1701 354 93 0.80 8.4338 7997 3097 0.65 8.2003 3591.5855 358 8.4363 8087.6748 15893 0.80 3592.95033597.6463 $158 \\ 158$ $0.65 \\ 0.65$ 8.2026 8.2085 $358 \\ 358$ 0.80 8.43708.43758091.7835 8105.4054 91 85 $74 \\ 71$ 0.85 0.85 158 158 70 0.658.21013599.3805 368 368 93 8.44388312.2292 67 8.2136 8.2149 0.653605 1435 91 8.4443 8316.4121 378 8.4459 158 65 0.653609.4091 104 0.90 8515.8260 176 85 0.958.22463985.1157 378 93 0.90 8.4504 8537.2505 8.4504 8541.9813 8.4556 8945.7620 17682 0.958.2299 3989.8655 8.2314 3991.4920 378 397 910.90 176 81 0.95104 176760.958.2365 4001.1297 397 93 0.85 8.4598 8967.2690

TABLE XXXI: Pareto–Optimal Solutions with D = 2 for σ = 0.8 and q = 0.9

F	M	p	TH	Delay	F	M	p	TH	Delay
11	11	0.15	3.2561	597.1464	186	82	1.00	8.1882	4156.9028
15	13	0.15	3.8510	696.4835	186	81	1.00	8.1895	4158.5300
16	14	0.15	4.0429	706.2196	186	76	1.00	8.1927	4169.0692
22	20	0.15	4 8789	707 8320	208	08	1.00	8 2020	4625.0178
22	20	0.10	4.0103	910 6549	200	05	1.00	8.2020	4628.4422
20	20	0.55	0.0374	810.0348	208	95	1.00	0.2000	4028.4422
40	39	0.75	7.0602	982.6642	208	89	1.00	8.2198	4636.4889
54	44	1.00	7.3929	1287.8192	208	85	1.00	8.2253	4642.9824
63	57	0.85	7.5976	1445.4107	208	82	1.00	8.2281	4648.5795
67	65	1.00	7.6505	1514.6468	208	81	1.00	8.2290	4650.3991
69	68	1.00	7.6585	1555.3764	208	76	1.00	8.2296	4662.1850
71	62	0.80	7 6627	1620 3219	209	76	1.00	8 2311	4684 5993
72	60	0.05	7.6701	1622.4425	216	95	1.00	0.2011	4921 5596
72	09	0.93	7.0791	1023.4433	210	80	1.00	8.2383	4821.3380
74	60	0.80	7.6959	1693.2097	216	82	1.00	8.2406	4827.3710
82	79	1.00	7.7306	1835.1225	216	81	1.00	8.2413	4829.2606
82	75	1.00	7.7562	1839.0999	223	82	0.95	8.2419	4989.4742
83	64	0.80	7.7656	1889.7732	223	81	0.95	8.2422	4991.7341
85	63	1.00	7.8276	1925.8063	229	89	0.95	8.2447	5110.2484
92	76	1.00	7.8361	2062.1203	229	85	0.95	8.2486	5117.3761
92	75	1.00	7 8410	2063 3804	229	82	0.95	8 2501	5123 7202
02	72	1.00	7 8501	2005.0001	220	91	0.05	8 2502	5126.0400
92	73	1.00	7.8501	2003.9404	229	104	0.90	8.2303	5120.0409
92	72	1.00	(.8542	2067.3002	247	104	1.00	8.2551	0480.2201
92	70	1.00	7.8617	2070.4072	247	98	1.00	8.2660	5492.2086
92	69	1.00	7.8649	2072.1080	247	96	1.00	8.2691	5494.9644
92	68	1.00	7.8677	2073.8352	247	95	1.00	8.2706	5496.2751
92	65	1.00	7.8738	2079.8135	247	91	1.00	8.2758	5502.3463
92	62	1.00	7.8752	2087.0339	247	89	1.00	8.2778	5505.8305
06	71	0.05	7 8767	2161 2759	247	85	1.00	8 2906	5513 5416
90	70	0.95	7.0707	2101.2700	241	00	1.00	0.4000	5510.1000
96	70	0.95	1.8798	2102.8727	247	82	1.00	8.2814	0020.1882
96	68	0.95	7.8852	2166.5408	247	81	1.00	8.2816	5522.3489
96	62	0.95	7.8906	2180.0784	251	89	1.00	8.2827	5594.9938
108	85	1.00	7.9009	2410.7793	251	87	1.00	8.2842	5598.7834
108	82	1.00	7.9156	2413.6855	251	85	1.00	8.2853	5602.8297
108	81	1.00	7,9202	2414.6303	251	82	1.00	8.2860	5609.5840
108	76	1.00	7.9406	2420 7499	251	81	1.00	8 2861	5611 7797
108	70	1.00	7.9400	2420.7499	231	01	1.00	8.2801	5011.1191
108	75	1.00	7.9441	2422.2292	255	85	1.00	8.2898	5692.1178
108	73	1.00	7.9503	2425.2344	278	104	1.00	8.2956	6173.6485
108	72	1.00	7.9531	2426.8306	278	98	1.00	8.3041	6181.5142
108	70	1.00	7.9576	2430.4780	278	95	1.00	8.3075	6186.0910
108	68	1.00	7.9608	2434.5022	278	91	1.00	8.3111	6192.9242
108	67	1.00	7.9618	2436.6122	278	89	1.00	8.3122	6196.8457
116	66	1.00	7 9981	2619 6635	278	87	1.00	8 3131	6201.0430
110	70	1.00	7.0007	2613.0600	270	01	1.00	0.0101	6201.0430
119	10	0.93	1.9991	2081.0009	218	80	1.00	8.3133	0203.3243
119	68	0.95	8.0013	2685.6079	286	76	1.00	8.3148	6410.5043
119	67	0.95	8.0016	2687.8877	292	98	1.00	8.3186	6492.8135
132	85	0.95	8.0149	2949.7539	292	96	1.00	8.3206	6496.0713
132	81	0.95	8.0281	2954.7484	292	95	1.00	8.3216	6497.6207
132	76	0.95	8.0410	2962.0994	292	93	1.00	8.3233	6500.9784
132	75	0.95	8.0429	2963,8298	292	91	1.00	8.3245	6504 7980
122	70	0.05	8 0/20	2073 0400	202	00	1.00	8 3951	6506 7429
102	10	0.95	0.0409	2010.9499	292	30	1.00	0.0201	6509.0170
132	08	0.95	8.0490	2978.9936	292	89	1.00	8.3254	0308.9170
146	93	1.00	8.0495	3250.4892	292	87	1.00	8.3259	6513.3257
146	90	1.00	8.0603	3253.3719	292	85	1.00	8.3260	6518.0330
146	85	1.00	8.0765	3259.0165	315	104	1.00	8.3334	6995.3211
146	82	1.00	8.0848	3262.9452	315	98	1.00	8.3397	7004.2337
146	81	1.00	8.0873	3264.2224	315	95	1.00	8.3420	7009.4196
146	76	1.00	8.0971	3272,4952	315	87	1.00	8.3446	7026.3617
146	75	1.00	8 0984	3274 4950	321	85	1.00	8 3486	7165 3718
146	79	1.00	8 1010	2220 7155	227	97	1.00	9 2522	7204 0226
140	12	1.00	0.1010	3260./100	321	01	1.00	0.3033	1294.0320
146	70	1.00	8.1011	3285.6462	335	95	1.00	8.3575	(454.4622
162	75	0.95	8.1327	3637.4275	335	89	1.00	8.3590	7467.4220
164	82	1.00	8.1376	3665.2262	340	98	1.00	8.3594	7560.1253
164	70	1.00	8.1459	3690.7259	340	95	1.00	8.3611	7565.7228
167	73	1.00	8.1539	3750.1310	340	91	1.00	8.3623	7574.0799
171	70	1.00	8.1608	3848.2569	340	89	1.00	8.3624	7578.8760
173	81	1.00	8 1615	3867 8800	352	95	1.00	8 3692	7832 7482
170	70	1.00	0.1010	3077.0000	0.75	100	1.00	0.0000	0004.1400
1/3	76	1.00	8.1665	3811.6827	3/5	108	1.00	8.3756	8321.7776
173	75	1.00	8.1668	3880.0523	378	82	1.00	8.3800	8447.8993
175	79	1.00	8.1684	3916.4199	383	89	1.00	8.3876	8537.3809
178	76	1.00	8.1770	3989.7544	391	98	1.00	8.3917	8694.1440
179	76	1.00	8.1791	4012.1688	391	95	1.00	8.3924	8700.5812
179	75	1.00	8.1792	4014.6206	398	104	1.00	8.3928	8838.5328
180	75	1.00	8 1919	4037 0497	300	05	1.00	8 3061	8856 2461
100	10	1.00	0.1012	4037.0487	390	90	1.00	0.0901	0000.0401
186	85	1.00	8.1838	4151.8977					1

TABLE XXXII: Pareto–Optimal Solutions with D = 4 for σ = 0.8 and q = 0.9